

BRIDGEWATER CROSSING DERWENT RIVER, BRIDGEWATER ARCHIVAL RECORD

PREPARED FOR DEPARTMENT OF STATE GROWTH

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ARCHIVAL RECORD

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INTRODUCTION

BACKGROUND

This Archival Record of Bridgewater Crossing in Bridgewater, Tasmania has been prepared for the Department of State Growth. The recording is intended to capture the context and setting of the Bridgewater Crossing, inclusive of the bridge, causeway and associated features, prior to the construction of the new Bridgewater Bridge. The causeway, bridge, and associated features that form the Bridgewater Crossing are currently included on the Tasmania Heritage Register (THR) and due to their heritage significance, this Archival Record has been prepared prior to the proposed works. This report aims to document Bridgewater Crossing in accordance with the guidelines for Archival Recordings specified by the NSW Heritage Office, having been identified as a best practice guide.

Hanna Morgan, Heritage Specialist of Purcell prepared this report with overview by Lucy Burke-Smith, Associate and Tracey Skovronek, Regional Partner. The photographs that form this Archival Record were taken by Martin Passingham on Monday 22nd March, 2021. The historic drawings included at Appendix 5 were sourced from the Department of State Growth and Point Cloud model was prepared by JACOBS. Sample views of the Point Cloud Model and included in this report only; a copy of the model is held with the Department of State Growth and can be viewed with 3D Viewer freeware.

METHODOLOGY

This report has been prepared in accordance with the guidelines for Archival Recordings specified by the NSW Heritage Office, including methodology and report format.

Each photograph has been allocated a unique name/number, refer Appendix 3. The name/numbers are then cross referenced to the Plan and Catalogue Sheets, refer Appendices I and 2. Markers are used on the Plan Sheet to indicate the location in which the photographs were taken. The Catalogue Sheets record the project details, date, photographer's name, camera type and lenses used, photographic data, direction and brief description of each photograph.

This Archival Record captures close-up and overall views of the Bridgewater Crossing, limited to the bridge and causeway only, as well as the immediate context. The photographic documentation follows a clockwise order starting at Location 1 and finishing at Location 8 depicted on the aerial site map (refer plan at Appendix 1). Limitations include suitable vantage points to capture all angles of the bridge structure, causeway, and associated infrastructure features.

REFERENCES

The following references inform this report:

- Guidelines for how to prepare Archival Records of Heritage Items, NSW Heritage Office, 1998.
- Guidelines for the Photographic Recording of Heritage Items using Film or Digital Capture, NSW Heritage Office, 2006.
- Purcell, "Bridgewater Bridge Replacement, Preliminary Heritage Impact Assessment". Prepared for Department of State Growth, 25 March 2021.
- Purcell, "Memorandum: Review of assessment of significance against state criteria/threshold". Prepared for Department of State Growth, 12 October 2020
- GHD, "Bridgewater Bridge Replacement Planning Study, Historic Heritage Investigations". Prepared for DIER, August 2010.
- Austral (Tas), "Draft Bridgewater Causeway and Bridge Historic Heritage Assessment and Archaeological Zoning Plan". 27 August 2020.

UNDERSTANDING THE SITE

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LOCATION

Bridgewater Crossing comprises the causeway and bridge which crosses the Derwent River, in Bridgewater Tasmania, located within the Brighton Municipal Council Local Government Area (LGA). The broader cultural landscape of the Bridgewater crossing has been considered in some detail by GHD and is summarised as follows¹:

The place connects Granton on the southern shore of the Derwent with Bridgewater on the north. It consists of the causeway, historic bridge infrastructure and the extant road and rail bridge. The crossing at this point of the Derwent is some 1.08 kilometres. The lower foothills of Snake Mount form the background on the southern shore, characterised by native vegetation on the upper slopes and low density residential development on the lower slopes. The immediate foreground of the causeway is the convict quarry from which the material used in its construction was obtained. Remnant historic buildings of these works include the Watch House and the Commandant's Cottage. The causeway itself is a low linear feature, approximately 785 metres long, as measured from the Brooker, Midland and Lyell Highway roundabout. Vegetated embankments rise on either side rise slightly above the roadway. The causeway has some visual prominence when viewed obliquely from surrounding road networks.

The Bridgewater Bridge is a prominent element in the landscape, notable for its truss form and in particular the two towers and lifting mechanism. Although visible from the Brooker Highway, its dark colouring does not make the bridge a distinctive element on its southern approach until in close proximity to the causeway. Conversely, the bridge stands out distinctly against the sky when viewed from the Lyell Highway, Boyer Road and Woods Point at Bridgewater.



Location map showing extent of the Bridgewater Crossing (causeway and bridge) shaded in yellow (Source: Google Maps modified by Purcell, boundary information supplied by Austral Tasmania). Note: north to top of page.

https://purcellukcom.sharepoint.com/sites/AsiaPacific/Shared Documents/Projects/240780/30 Reports, Specifications & Schedules/Archival Record/00 Report/Bridgewater Crossing Archival Record 20210818.docx

¹ GHD, Bridgewater Bridge Replacement Planning Study. Historic Heritage Investigations, report prepared for DIER, August 2010

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HISTORICAL SUMMARY

The following Historical Summary draws from the Draft Bridgewater Causeway and Bridge Historic Heritage Assessment and Archaeological Zoning Plan, prepared by Austral (Tas) 27 August 2020:

Introduction

The study area forms part of a rich historic cultural heritage landscape which demonstrates the evolution of transport over a period of more than two hundred years. The European history of the place has witnessed these changes from ferries, a causeway, numerous road and rail bridges, and the current structure built in the 1940s. Each phase has left evidence in the landscape, which is discussed in the following sections. It is drawn principally from previous detailed assessments of the place. Original references are provided.²

Arranged chronologically, this historical overview addresses the following key phases of use and development:

- The Aboriginal People of the Area and Contact History;
- Early European settlement of Hobart;
- The Black Snake Inn and Early Development of the Area;
- The Bridgewater Causeway and Convict Road Station;
- Earlier Bridge Crossings of the Derwent at Bridgewater:
 - The 1849 Timber Bridge;
 - The 1874 Tasmanian Main Line Railway Bridge;
 - The 1893 Road and Rail Bridge;
 - 1908 Conversion of the 1874 Rail Bridge to Road Uses;
- The Current Bridgewater Bridge;
 - The Designer of the Bridge AW Knight;
 - Welding Technologies used in the Bridge; and
- Later Modifications to the Bridgewater Bridge.

The Aboriginal People of the Area and Contact History

Before European settlement, Ryan has described Tasmanian Aboriginal society as consisting of nine nations, each containing multiple social units or bands. Boundaries between groups could vary between well-defined borders based on geographical features, to broader transitional zones existing between two friendly tribes.

The Derwent formed the boundary between two such nations. The western shore of the Derwent was part of the lands of the South East nation. Their territory covered an area of approximately 3,100 square kilometres to encompass the western shore of the Derwent north to New Norfolk, the D'Entrecasteaux Channel and Bruny Island, and south to South Cape, extending west to the Huon Valley. Ryan writes that prior to European contact, the area probably contained seven bands, each with about 70 to 80 people. The Hobart area was home to the Muwinina band. They knew the area as Nibberloone or Linghe.

The eastern shore is part of the country of the Oyster Bay people. Located on the east coast of Tasmania, their lands covered some 7,800 square kilometres, including 515 kilometres of coastline. Their country extended from St Patricks Head in the north, to the east bank of the Derwent. Inland, it reached St Peters Pass in the Midlands, before following the Eastern Tiers to the Break O'Day River, where it returned to the coast at St Patricks Head.

Prior to European settlement, Ryan proposes that ten bands formed part of the Oyster Bay nation with a population of between 700-800 people, the largest group in Tasmania. The Risdon and Pitt Water areas were the home of the Moomairremener band.³

Contact between Europeans and Aboriginal people occurred on both sides of the Derwent. With the establishment of Hobart Town in 1804 the Reverend Robert Knopwood made brief notes in his diary on contact between the two groups. An entry in March 1804 records his observations on encountering 'a great many native hutts [sic] and the fires they made' on the western shore of the Derwent, north of Hobart. Two days later he noted many Aboriginal people were around the camp at Sullivans Cove, but could not be persuaded to enter. On numerous occasions, Knopwood wrote of the fires lit by the Aboriginal people for both land management and hunting.⁴

Initial contact between the Muwinina and Europeans was positive. Although not visiting the settlement, the Aboriginal people were friendly with small groups of Europeans they met at more isolated areas. Such relations were not to last, as by 1806, violence had already began to emerge. Conflict over food resources was one of the triggers in the deteriorating relationship. By necessity, the European settlers sought to augment their meagre stores with fresh caught game, mainly kangaroos, thereby placing them in direct competition with the Aboriginal people. So insatiable was the European demand for kangaroos, that by late 1808 this food resource had largely been exhausted from the immediate surrounds of Hobart, with hunting parties having to venture further afield.⁵

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² See: GHD, Bridgewater Bridge Replacement Planning Study. Historic Heritage Investigations, report prepared for DIER, August 2010; GHD, Tasmania's Truss Bridges. Comparative Heritage Assessment, prepared for DIER, October 2009; Austral Archaeology, National Highway Approach to Hobart – Bridgewater Planning Study Heritage Assessment: Stage I – Volume 2, 1997; Austral Archaeology, Midland Highway Black Snake Lane to East Derwent Highway Historical Archaeological Survey Report, prepared for Road & Environmental Planning Group, 1996; Whitlam, L, 'The Bridges, Road and Rails of Bridgewater', Tasmanian Historical Research Association and Proceedings, Vol. 36, No.2, 1989

³ Ryan, L, The Aboriginal Tasmanians, St Leonards: Allen & Unwin, 1996, p.12

⁴ Nicholls, Mary (ed.), The Diary of the Reverend Robert Knopwood 1803-1808. First Chaplain of Tasmania, Tasmanian Historical Research Association: Hobart, 1977, p.46; Brown, S, Aboriginal Archaeological Resources in South East Tasmania. An Overview of the Nature and Management of Aboriginal Sites, National Parks & Wildlife Service Tasmania, Occasional Paper No. 12, April 1986, pp. 171-172

⁵ Ryan, op. cit., pp.76-78

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On the eastern shore of the Derwent, contact between Europeans and Aboriginal people began during the late-eighteenth century. In 1798 Bass and Flinders explored the Derwent venturing as far as what is now Bridgewater, and reaching an inlet of the river, which they named Herdsman's Cove. From here, Flinders travelled two miles inland up the Jordan River. It was in the vicinity of Herdsman's Cove that an encounter took place with Aboriginal people. Finding two women and a man carrying three spears, Bass and Flinders attempted to communicate with the group by offering them a black swan. The two women left, but the man remained.⁶

Following a failed attempt to follow him to his hut, Bass and Flinders left the man - their only encounter with Aboriginal people in Van Diemen's Land.⁷ A few years later in 1802, Peron found some huts, smouldering fires and remains of food in the vicinity of Herdsman's Cove, but no Aboriginal people were seen.⁸

In September the following year, Lieutenant John Bowen arrived at Risdon Cove, establishing the first permanent European settlement in Van Diemen's Land. Uneasy contact between the Aboriginal people and settlers descended into conflict in May 1804.⁹

The period 1804 to 1824 has been described as one of 'uneasy coexistence' between Aboriginal people and Europeans. Certainly, there were outbreaks of hostilities, but by comparison with what occurred post-1824, the first two decades since the coming of the Europeans were relatively calm.¹⁰

Such relative peace was not to last. During the 1820s, the European population grew rapidly, accompanied by an explosion in the issuing of land grants over the most valuable grass plains. These actions created disputes over access to native game, hunting grounds and the connection of Aboriginal people with their traditional tribal lands. What followed was unprecedented violence.¹¹

Early European settlement of Hobart

The first decade of European settlement in Hobart was marked by the close relationship between development and the waterfront. After the failure of the settlement at Risdon Cove and the relocation to Sullivans Cove on the western shore in February 1804, the early occupants of Hobart Town spent their first decade in a struggle for survival, building upon the camp clustered on the western boundary of the cove.¹²

In 1806 Lieutenant Governor Collins wrote of his reliance on the small amounts of wheat and barley which were grown at the government farm at New Town. This was supplemented by locally procured game. The lack of food was not the only problem faced by the young settlement, with the physical condition and morale of the general population being a cause of concern. Collins described them as having been scantily clad and badly fed for a year, and by mid-1806 they were largely destitute of clothing. To supply goods and food he requested that ships be sent to Hobart first instead of Sydney.¹³

Merchant ships were not permitted to enter the Derwent until 1813. After this time and most notably when the embargo on whaling was lifted, port activity gradually increased. Despite these impediments it was not long before settlement spread out along the shores of the Derwent, albeit on a limited scale. By the late 1820s the numbers and size of ships using the port had increased markedly, coinciding also with the beginning of urbanisation. At this time the population of the town had reached 6,000. The rapid increase in demand for port facilities was not solely due to the importation of goods as had previously been the case, but also the beginning of trade in export commodities.¹⁴

The Black Snake Inn and Early Development of the Area

Travellers were some of the first Europeans to visit the Granton area, or Black Snake as it was originally known. In 1811, Governor Macquarie during his first visit to Van Diemen's Land wrote in his diary about a trip to New Norfolk, where he and his party had breakfast at Black Snake Point. Knopwood's diary also mentions frequent visits to the Black Snake Inn between 1819 and 1825.¹⁵

The first Black Snake Inn was probably constructed between 1817 and 1821 by which time a ferry crossing the Derwent was in operation from the location. This also corresponds with the period when travel became more frequent with the completion of the road constructed by McCarty between Hobart and New Norfolk in 1819, Tasmania's first formed road. A population centre had emerged at Black Snake. In 1824, 23 children were attending school in the area.¹⁶

During the late 1820s or early 1830s the current gothic inspired building was constructed, presumably on the same site as the first inn.¹⁷ The Black Snake Inn was one crossing place of the Derwent used by ferries. A number of flat bottomed punts and clinker type craft crossed the river back and forth from select locations. There were two well known crossing points on this part of the Derwent; one from Roseneath

Environmental Planning Group, 1996, p.4: Solomon, RJ, Urbanisation. The Evolution of an Australian Capital, Angus & Robertson, Sydney, p.27 ¹⁴ Austral Archaeology, 1996, pp.4-5: Solomon, op. cit., p.75

⁶ Flinders, M, A voyage to Terra Australis: undertaken for the purpose of completing the discovery of that vast country, and prosecuted in the years 1801, 1802, and 1803, in His Majesty's ship the Investigator ..., London: G and W Nicol, 1814, pp.135-136
⁷ Ibid, p.136

⁸ Alexander, A, Brighton and Surrounds. A history of Bagdad, Bridgewater, Brighton, Broadmarsh, Dromedary, Elderslie, Mangalore, Old Beach, Pontville and Tea Tree, Gagebrook: Brighton Council, 2006, p.3

⁹ Ryan, op. cit., pp.73-75

¹⁰ Boyce, J, Van Diemen's Land, Black Inc.: Melbourne, 2008, pp. 67-68, 105-106; McFarlane, I, 'Frontier Conflict', in Alexander, A, (ed.), The Companion to Tasmanian History, Centre for Tasmanian Historical Studies, University of Tasmania: Hobart, 2005

¹¹ Boyce, op. cit., pp.140-146

¹² Walker, JB, 'The English at the Derwent and the Risdon Settlement', Early Tasmania: Papers Read before the Royal Society of Tasmania during the Years 1888 to 1899, John Vail Government Printer, Hobart, p.59

¹³ Austral Archaeology, Midland Highway Black Snake Lane to East Derwent Highway Historical Archaeological Survey Report, prepared for Road &

¹⁵ Austral Archaeology, 1996, p.5: Macquarie, L, Governor of New South Wales, Journals of his Tours in New South Wales and Van Diemen's Land 1811-1822, Library of Australian History, pp.58-59

¹⁶ Austral Archaeology 1996, p.5: Rait BE, Historic Buildings, City of Glenorchy, unpublished document; Robson, LL, A History of Van Diemen's Land Volume 1, Oxford University Press, 1983, p.130

¹⁷ Austral Archaeology 1996, pp.5-6: Brand I, The Convict Probation System: Van Diemen's Land 1839-1854, Blubber Head Press, 1990, p.20 Bridgewater Crossing – Archival Record [Revision 02, 18th June 2021]

(Austin's Ferry) to Herdsman's Cove and Old Beach, and the second from Black Snake to Herdsman's Cove and Green Point. Travel by ferry could be dangerous and was often inconvenient, being dependant on the current, wind and availability of the service.¹⁸

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By this time, the inn had diversified and offered both ferry and coach transport to travellers. Throughout its life the inn has functioned as a public house, shop and currently is a private residence.¹⁹

The Bridgewater Causeway and Convict Road Station

In 1826 the Land Commissioners investigated the best location for crossing the Derwent. After some deliberation a site at Black Snake was decided on. There was plentiful timber at nearby Mount Dromedary, while stone was available from quarrying away at the hill behind the intended causeway, at what is now Granton. The river at this point also included a sand and mud bar which ran most of the way over the Derwent, and at a shallow depth.²⁰ This was seen as a desirable attribute in constructing a causeway, but one that was later to cause considerable issues. In 1830 the convict station at Bridgewater (which later became known as Granton) was opened and works began on constructing the causeway.²¹ Works were to prove a very slow affair. To hasten progress, John Lee Archer, civil engineer recommended the construction of a timber railway with trucks to be pulled by bullocks.²²

Ross's almanac for 1831 wrote:

An establishment has been formed at Bridgewater for a Chain Gang, which is employed in constructing that great work, the causeway over the Derwent. A gaol or barracks for the reception and safe keeping of the prisoners after their hours of labor, was among the first works completed; It is capable, of containing 160 men. A commodious barracks for the military has also been constructed, as well as a store, solitary cells for such convicts as misconduct themselves, &c, &c. On a commanding eminence stands a neat building for the Officers quarters.

A very excellent quarry on the road side gives employment to one part of the gang, while the others are busily engaged in wheeling the stone out into the water. The bed of the river over the flats at this place is composed of soft mud, which the heavy mass of stone thus thrown upon it soon displaces, and in this manner a good foundation is obtained on which to raise the subsequent work. Five and twenty small abutments will then be built and covered with timber. From the piers to the edge of the deep channel a solid road of stone will be formed with a small basin at the end to haul the punt into. As the distance across is very trifling no delay can occur, because the punt instead of being towed by a boat will be made to swing backwards and forwards.²³

This was perhaps the last positive account of the works, which were not trifling by any measure. The causeway was constructed at an oblique angle, which was not the shortest point of crossing, although planned that way to contend with the wind and currents at this stretch of the Derwent. Early attempts at constructing piers in the sand and mud were found to be a failure due the failure to find a solid bottom.²⁴ The work was beset by controversy and labelled a 'folly' when the tons of stone dumped into the river were continually submerged in the mud and silt, without a trace. This perhaps simplifies the construction of the causeway to little more than dumping rock in the river. There was however engineering to the structure, as referred to by Ross and the construction of 25 abutments. Other contemporary accounts provide a few more clues.

A curious description of the causeway was given, midway during construction. It noted a structure quite different to the one we know:

The work at this station [Bridgewater], was the construction of a massive bridge across the Derwent, which is here three-fourths of a mile in breadth. It had been a long time since it was commenced, and was not yet completed when I finally left the island. It is composed almost entirely of stone. From either shore two solid stone abutments extends to some distance into the river. Other abutments are placed at regular distances, also filled with stone. Arches of stone span the spaces, at a sufficient height to permit the passage of small steam boats. Before its final completion the bridge somewhat resembles a shallow aqueduct, but instead of water is filled with pounded stone, thus making a way over the water in all respects like the road itself.²⁵

Other than its description as being composed of stone and the presence of abutments, it is difficult to reconcile this description with what was actually constructed. Abutments only extended from the southern shore of the Derwent, and while arches were constructed, it seems unlikely that they could accommodate small steam boats. As a description made part way through construction works, the writer's interpretation may have been inaccurate.²⁶

By 1833 the causeway extended for some 365 metres. It was 28 metres wide at its base and 16 metres wide at the top. Roderic O'Connor made an urgent request for 250 planks required to complete the 'bridge', used in some form in the construction of the causeway.²⁷ By the following year the causeway had reached a length of some 708 metres, reaching nearly its ultimate length. The causeway committee investigated the works in July 1834, finding that the portion immediately beyond the arches (towards its southern end) had already been sinking into the mud for some time. The obvious solution was to support the structure with piles, but the costs of such works were unacceptable. Instead, they favoured the use of vegetation rafts on which the stone would be supported, and disappointed that such a method had not been adopted from the start. They also recommended the removal of the arches at the southern end, where the current

²⁶ Austral Archaeology 1996, p.8

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¹⁸ Austral Archaeology 1996, p.7; Newitt, L, Convicts & carriageways: Tasmanian road development until 1880, Hobart : Dept. of Main Roads, Tasmania, 1988, pp.35-37, 108-111

Austral Archaeology 1996, p.7

²⁰ TAHO, CSO1/285/6777, Correspondence 6 October 1831

²¹ TAHO, CSO1/285/6777, Land Commissioners to Survey Office, 6 November 1826; Austral Archaeology 1996, p.7; Newitt, op. cit., p.55

²² TAHO, CSO1/284/6777, John Lee Archer to Colonial Secretary, 19 June 1831

²³ Launceston Advertiser, Monday 17 January 1831, p.24

²⁴ TAHO, CSO1/285/6777, Committee on the Causeway across the Derwent to Colonial Secretary's Office, 14 October 1831

²⁵ Austral Archaeology 1996, p.8: Gates, W, Recollections of Life in Van Diemen's Land, in Australian Historical Monographs, XL, Part 1

²⁷ TAHO, CSO1/543/11623, Roderic O'Connor to Colonial Secretary, 12 September 1833

risked undermining the causeway.²⁸ A plan was prepared, recommending the proposed point of connection with the northern shore of the Derwent

It was to take a further two years however before it was finished, likely because of the continual subsidence into the mud. Works to date included the construction of six piers, upon which planks were laid, allowing carts to travel across the short distance. When finally the causeway formation did appear above the water line, it was prone to subsidence and had to be continually built up. The continued dumping of rock displaced large volumes of mud, creating banks on either side of the causeway. There was no shortage of opinion on how to deal with the problem and perhaps the original concept was modified over time. Nevertheless, the majority sources, including artwork, depict the causeway as an unbroken formation of stone.²⁹

Structural problems continued into 1835. A report was prepared which supported the use of vegetation rafts as the best solution, but questioning the integrity of the embankments on either side of the causeway. It recommended that the walling on either side be at least 1.2 metres thick and battered. Those already constructed were found to be badly placed and did not have a sufficient hold on the bank.³⁰

As it neared completion in 1835, more positive accounts began to be published on the 'magnificent work' that would address the dangers and difficulties of crossing the Derwent, which was cut to only a 3 minute punt ride connecting from the end of the causeway to the northern shore.³¹ One very detailed report noted how the overseers had addressed the fruitless problem of stone being swallowed up by the mud. The Hobart Town Courier wrote:

This stupendous undertaking is situated about 11 miles from Hobart town, It consists of a mound or roadway carried out over an extensive bank, near a mile in extent to the edge of deep water and the stream, so as to reach within a short distance of the opposite bank, the earth and stone for the purpose being dug from a hill contiguous with the river. Much of the stone and materials originally carried out of course subsided in the mud, until it became sufficiently solid, and in one part the mud thus pushed out has risen on each side and formed small islands, now rapidly covering with verdure.

By adopting the expedient of laying a compact bottom of logs and dead timber on the mud so as better to prevent the earth and stone from subsiding, the work is proceeding with great rapidity and about three-quarters of a mile of the mound are now finished on a firm basis, so as to admit of carriages of any weight or description freely to pass.

. . . .

It is a curious fact and one which serves to declare the stability of the work that in times of heavy rains, when the flow of fresh water is strong down the river, that the level is invariably some inches higher on the lower side of the embankment, than on the upper. caused doubtless from the meeting of the tide with the freshwater. For these reasons, Lieut. Wrixon, with the advice of the Inspector has very judiciously shut up the arches that were originally left open at the south extremity as a sort of safety valve in case of any accumulated force of the stream pressing with injury on either side. The stones which composed these arches being removed, have been applied to the purpose of erecting a large and lofty room or hall, used as a church and school room.³²

The ingenuity of constructing rafts of timber and vegetation to support the weight of the stones appears to have been the solution to the never ending problem of the mud. The article also describes arches on the southern end of the causeway, which is again consistent with the earlier description given above, but that these arches had been removed by 1835 and the stone used elsewhere. However, whether these arches were high enough to allow small steam boats to pass beneath seems somewhat dubious. The success of the raft system was however already in doubt, an acerbic article from as early as 1836 describing the causeway as 'floating on a foundation of brushwood faggots, which will continue at intervals to sink in various places with its super incumbent weighty until it has displaced the soft mud.'³³ This subsidence was already occurring as early as 1836. Wrixon had commanded the laying of the road metal along the course of the causeway, only to be ordered to raise the causeway in height by another 1.2 metres.³⁴

The grand opening of the causeway was made in October 1836 by Lieutenant-Governor Arthur with a guard of honour and the band and colours of the Scotch Fusiliers. It was approximately 730 metres long, 20 metres wide and contained 400,000 cubic metres of fill. At the time, its cost of £45,000 was enormous. From its northern end was a gap approximately 340 metres across the Derwent to the northern shore. Between 1836 and 1849 a 'flying bridge' or ferry winched on cables connected the causeway with the shore.³⁵

In 1863 the causeway was widened and raised by some 76 centimetres in attempt to avoid overtopping by the water. Low stone walls were constructed on both sides of the causeway to bind the new fill. It was again widened on the downstream side in 1874 to accommodate the Tasmanian Main Line Railway, and later in 1893 when the bridge was converted to combine both road and rail uses.³⁶

The 1849 Timber Bridge

Parliament authorised the construction of the first bridge to span the gap of 340 metres in 1846. The contract for its construction was awarded to Messrs. Thomas and Blackburn in early 1847. Convicts from the Mount Dromedary probation station spent the remainder of the year cutting and stockpiling timber for the bridge. The Illustrated London News wrote in 1851 how roads first had to be cut into the gullies

³⁰ TAHO, CSO1/285/6777, report made on the works carried on by Government at Bridgewater Van Diemen's Land June 11 1835

³¹ The Tasmanian, Friday 3 April 1835, p.7

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²⁸ TAHO, CSO1/285/6777, Report of the Committee on the Causeway, 28 July 1834

²⁹ Austral Archaeology, National Highway Approach to Hobart – Bridgewater Planning Study Heritage Assessment: Stage 1 – Volume 2, 1997, p.6; The Sydney Gazette and New South Wales Advertiser, Thursday 17 October 1833, p.3; Austral Archaeology 1996, pp.7-8: Brand, op. cit., pp.108-109

³² The Hobart Town Courier, Friday 12 June 1835, p.2

³³ The True Colonist Van Diemen's Land Political Despatch, and Agricultural and Commercial, Friday 8 January 1836, p.7

³⁴ The True Colonist Van Diemen's Land Political Despatch, and Agricultural and Commercial, Friday 15 January 1836, p.14

³⁵ Austral Archaeology 1996, p.8: Whitlam, L, 'The Bridges, Road and Rails of Bridgewater', Tasmanian Historical Research Association and Proceedings, Vol. 36, No.2, 1989, p.57; Fowler, A, 'River Derwent, Tasmania – Bridgewater Bridges – Past and Present', 16th Engineering Heritage Australia Conference Hobart November 2011, p.2; The True Colonist Van Diemen's Land Political Despatch, and Agricultural and Commercial, Friday 21 October 1836, p.4 ³⁶ Austral Archaeology, Stage 1 – Volume 2, 1997, pp.7-8

on the steep mountain sides to facilitate removal of the timber. Two of these gullies were lined with timber, forming a chute down which the logs were moved. The process was intensive. First the timber was loaded into a chute and propelled downward by its own momentum to a benched landing where it was manoeuvred to another chute which conveyed it to the base of the mountain. There, the terrain was of sufficient grade to allow the logs to be carried by wagons to the water's edge. From here, it was towed by boats to the work site.³⁷

Construction of the timber bridge works began in January 1848, starting at the northern end of the causeway. The bridge was not built as a straight extension of the causeway, rather its alignment diverged ten degrees eastwards to the nearest point of the river bank, and the same location used for the ferry wharf. The wharf was demolished and a temporary wharf constructed nearby.³⁸

The spans of the bridge were supported by over 360 timber piles. To allow for river navigation upstream to New Norfolk, the bridge (and all subsequent structures) included moving spans. Originally a swing span was proposed for Bridgewater, but this was substituted with a rolling span modelled on a prototype bridge over the Arun River, England.³⁹

The bridge was opened to traffic on 26 April 1849 with a roadway 7.3 metres wide. A series of landing or fender piles were installed in the river both up and down stream for some 55 metres to assist shipping in negotiating the opening. Tolls were collected until 1880, and a toll keepers house was located near the bridge approach. A new house for the toll keepers was built c.1870 to replace the old one, but was located so close to the river that water entered its basement at high tide. The causeway was also raised around c. 1860 to avoid 'overtopping' by water. Following the abolition of tolls the toll keeper became known as the bridge keeper and the old toll house survived until about 1947.40

The 1874 Tasmanian Main Line Railway Bridge

Works to construct a rail line between Hobart and Launceston began in 1872, with the Derwent being a key challenge to the project. In response, in 1874 the Tasmanian Main Line Railway Company constructed a separate timber rail bridge on the downstream side of the causeway. The bridge keyed into the causeway on a curve, approximately 30 metres before its end, before running parallel to the 1849 road bridge for 350 metres to the northern bank of the river. The 1874 bridge also required a moving span and a lattice girder iron bridge was installed which pivoted on a turntable. The railway was intended primarily for the transport of goods between Hobart and Launceston, but from 1875 passenger carriages were attached on weekdays with coach transfers.⁴¹

The moving bridge span was supported by timber piles, and this construction method caused problems with subsidence. As a precaution, measures were put in place to ensure that the span was locked in place before every train crossing. However, the Rail Engineer in Chief was never truly satisfied with these measures, nor the signalling equipment at the Bridgewater end. These fears came to be when disaster struck in 1886. The swing span had shifted slightly resulting in the Launceston express engine being derailed and overturned. One rail worker and one passenger died in the accident.42

Infrastructure changes in Bridgewater to accommodate the railway included the construction of a small stockyard and passenger station in the vicinity of the existing War Memorial Reserve, and gated crossings on all secondary roads. The junction between the railway and the Main Road was monitored from a small two storeyed signal box just north of the station.⁴³

The 1893 Road and Rail Bridge

By 1888, the 1849 road bridge was declared unsafe. However, without other options, it continued to be used. In 1891 a contract was awarded for the construction of a new road bridge. Like all previous, it included a swing span, which was fabricated in England and completed in 1893. The new bridge was upstream, or to the west of the 1849 bridge. Its completion resulted in the strange scenario of three bridges extending from the northern end of the causeway.⁴⁴

The design of the 1893 bridge allowed for its later conversion to a rail bridge. It was largely constructed from timber with the exception of the pier or caisson on which the plate girder swing span turned. This bridge extended straight out from the causeway and landed on the northern bank. The northern abutment adopted a dog-leg design to enable it to accommodate the heavy railway traffic straight ahead and a lighter roadway that would curve eastward. The bridge was over 360 metres long with a road width of 6.5 metres that narrowed to five metres over the swing span. The navigable channel was 13 metres wide. The 1849 road bridge was retained in anticipation that it would be required as a temporary detour while the new bridge was converted to rail use. However, this was not to happen until 1906-07 by which time the former had become a danger to the 1874 rail bridge. The 1849 was eventually demolished in 1899.⁴⁵

The old 1874 Tasmanian Main Line Railway Bridge coupled with the advent of heavier locomotives, made the transfer to the 1893 bridge urgent. In 1906-07 the conversion works began. These works required the widening of the full length of the causeway on the upstream, western side, substantial filling in behind the northern abutment and land acquisition at Bridgewater. The rail line was transferred from the eastern to the western side of the causeway, where it remains to this day. In response, a new station was constructed adjacent to the bridge abutments on the Bridgewater side. Shared use by road and rail of the 1893 bridge began in January 1908. However, community disquiet about the length of delays in road traffic and compromised safety conditions, led to a reversal of positions and the conversion of the 1874 rail bridge to a road bridge.46

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³⁷ Austral Archaeology 1996, p.9: The Illustrated London News, 12 April 1851

³⁸ Austral Archaeology 1996, p.9: Whitlam, *op. cit.*, p.57

³⁹ Austral Archaeology 1996, p.9: Whitlam, op. cit., p.58

⁴⁰ Austral Archaeology 1996, pp.9-10: The Illustrated London News, 12 April 1851; Whitlam, op. cit., p.59

⁴¹ Austral Archaeology 1996, p.10: Whitlam, *op. cit.*, pp.62-63

⁴² Austral Archaeology 1996, p.10: Whitlam, op. cit., p.63

⁴³ Austral Archaeology 1996, p.10: Whitlam, op. cit., pp.63

⁴⁴ Austral Archaeology 1996, p.10: Whitlam, *op. cit.*, pp.65-66

⁴⁵ Austral Archaeology 1996, p.10: Whitlam, op. cit., pp.66-67

⁴⁶ Austral Archaeology 1996, p.10: Whitlam, op. cit., p.67

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1908 Conversion of the 1874 Rail Bridge to Road Uses

In 1908 the 1874 railway bridge was converted to road uses. This required the bridge to be re-piled and the deck converted to accommodate a two lane roadway. It was opened in 1908. The new approaches to the bridge resulted in demolition of the 1876 and 1887 railway station platforms at Bridgewater.47

Joint use of both rail and road of the 1893 bridge was short lived, lasting just ten months before reverting solely to rail. It was temporarily jointly used again in 1911, 1912, 1924-25 and 1926-27 while repairs were being carried out to the road bridge. Heavy vehicles were also regularly redirected over the 1893 bridge.

In 1916 the road bridge was rigged with timber gantries to carry power from the new Waddamana hydro-electric power station to Hobart. This was a temporary measure due to a war time delay in shipping of three special towers from England. On arrival, the towers were erected as planned. This included a backstay and 50 metre high tower on the north bank and another straddling the road at the end of the causeway. The towers were replaced with a submarine cable in 1987.48

When the Second World War broke out a number of strategic sites were declared, among them the Bridgewater Bridge. It was guarded by a small number of sentries located in temporary buildings off Nielsen Esplanade. By 1941 the road bridge was so rickety that a single lane system with coloured signal lights was brought into operation by the army.⁴⁹

The Current Bridgewater Bridge

Whitlam notes the importance of the development of the Derwent Valley Paper Company in promoting the need for a new bridge at Bridgwater. Indeed, he suggests that had it not been for the Boyer paper operation, the road and rail bridges may never have been combined.50

Discussions between the government and the Paper Company began in 1933. To allow for shipping access, the company initially requested a clear opening in the bridge some 18 metres wide. The Public Works Department investigated, and found that modifying the existing bridges for such a width would be very difficult. Further, the existing road bridge had been constructed as the rail bridge in 1874, and although not dangerous, had reached the end of its life. The best solution would be for a new combined road and rail bridge. To maintain the essential transport connections, the new bridge would need to be built between the existing road and rail bridges. With such a constraint and the narrow distance between the two existing bridges, it would not be possible to construct a swing bridge. Initially the department favoured a bascule type of lifting span, but later came to favour a lift span.⁵¹

Preparatory geotechnical works were carried out in 1933. Boring of the riverbed found a solid rock bottom from 7.3 to 28 metres below the water level. The overlying strata of the bed was largely mud, but clay was also found over the northern half. A basalt base was found on the northern bank of the Derwent, but was underlaid by mud, which would require foundations to descend to a deeper level.

Department engineer and key designer of the bridge Allan Knight and director of Public Works George Balsille toured New South Wales in 1936 visiting a number of different types of moving bridges. Balsille also visited the combined road and rail bridge at Paringa, South Australia. Following the review of how other states had addressed similar problems, the department shifted its position to a lift span structure rather than a bascule arrangement.

A meeting was held with the Hobart Marine Board in April 1936 to determine the required width for the opening of a new structure at Bridgewater. Conflicting advice was given on the tonnage of shipping that would need to pass through the bridge, although it did confirm that a bascule bridge was not suitable. As a result, the preliminary concept was for a lift span bridge to be constructed with a horizontal clearance of 36 metres, and a vertical clearance above the high water mark of 30 metres.⁵²

Further geotechnical work was required to determine costs for the piles supporting the lift span as no information was available on the likely behaviour of the mud should bridge cylinders be sunk. Testing was carried out on timber and concrete piles to determine if a satisfactory pile foundation could be constructed. Although timber piles were acceptable from a load point of view, they rapidly deteriorated about the mud line resulting in expensive and frequent renewal.

Initial costings for the new bridge were estimated at £100,000. A further £25,000 was needed when the lift span was widened, whilst the needs of other government departments added a £10,000 to the project. Offsets and savings in the pile testing reduced the final estimate of works to £123,000.

The Parliamentary Standing Committee on public works investigated the project in 1937. The Railways Department estimated that the existing rail bridge had an estimated lifespan of at least 15 years. However, if the road bridge was to be renewed, it was sensible to also replace the rail bridge at the same time. The Paper Company and the Marine Board were in support of an opening at least 30 metres wide, which would provide safe navigation of vessel up to 2,000 tons. They estimated that on establishment of the factory, the mill would be served by 60 to 80 ships.53

Public Works submitted plans for a steel and concrete lift bridge with a horizontal opening of 30 metres. The Department was satisfied that the proposed opening would be sufficient for the largest vessels that would need to reach Boyer. The cost of this opening was estimated at \pm 19,800. Cost comparisons were also made on the use of different materials. A new timber bridge was estimated at \pm 70,000 while a bridge in permanent materials would cost £103,500, excluding additional costs for the bridge approaches and incidental works.

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⁴⁷ Austral Archaeology 1996, p.10: Whitlam, op. cit., p.69

⁴⁸ Austral Archaeology 1996, p.10: Whitlam, *op. cit.*, pp.72, 82

⁴⁹ Austral Archaeology 1996, p.11: Whitlam, op. cit., p.82

⁵⁰ GHD, Tasmania's Truss Bridges. Comparative Heritage Assessment, prepared for DIER, October 2009, p.195: Whitlam, op. cit., pp.67-73

⁵¹ GHD 2009, p.195: Whitlam, op. cit., pp.67-73

⁵² GHD, 2009, p.196; Memorandum 1/37, Removal of Bridgewater Bridge, Parliamentary Standing Committee on Public Works, 1937, pp.1-2

⁵³ GHD, 2009, p.196

The Committee was hesitant to support a project that would result in the demolition of a rail bridge which still had at least a 15 year lifespan left. As a result, the Department were asked to investigate further. They considered the construction of a new road bridge to the east of the existing, while a new rail bridge would be built at the end of its life. It was noted however that having two different bridges with two opening spans would make navigating between the bridges a difficult exercise. Balsille recommended the Department's preferred option of a new combined road and rail bridge, but noted that construction could be postponed until the old rail bridge had reached the end of its life.54

The Committee made three key recommendations:

- 1 Approval of the substructure of a bridge which combined road and rail uses and approval for the superstructure of the road portion including the lift and flanking truss spans. A cost estimate of $\pm 103,000$ was given for this part of the works.
- 2. A decision on the superstructure of the rail portion of the bridge (with the exception of the lift and flanking spans) should be deferred until the Paper Company or other industries established that they needed sea going vessels to navigate above Bridgewater, or that the existing rail bridge required replacement; and
- That before committing addition funds for the construction of the opening span, it was necessary to dredge the Derwent near its 3 junction with the Jordan River.⁵⁵

Construction began in 1937 with preliminary site work, and in January the following year, the acquisition of properties on the bridge approaches. On the Bridgewater side this included demolition of the Railway Hotel, stables and bazaar to make way for the steel fabrication yard and workshop. A nearby 1925 fruit drying factory was rented to provide extra space for the Public Works Department.⁵⁶

It was originally planned that the road bridge would be completed by late 1940. However, the outbreak of the Second World War resulted in the loss of workers and materials, and resources, were instead transferred to completing the Hobart floating bridge. As a result, the Department had difficulties to get tenders for the hoisting material, and the bridge was constructed in a piecemeal manner.⁵⁷

The bridge opened to road traffic in March 1942 once the lift span had been installed, although it was to take several years before the lift span came into operation. It was not until 1951 that the last of the piles from the redundant bridges were removed. The massive concrete filled steel caisson on which the 1893 swing span rotated was left in situ, along with the 1893 abutments on the Bridgewater side of the river.⁵⁸

By 1944, demand had grown for newsprint and the government submitted plans for a revised railway station at Bridgewater to supply Boyer. The factory was also examining its transport needs, favouring river transport, but noting that as a temporary measure, a rail siding was also required. In response, the government continued the upgrade of the Bridgewater Station and brought the bridge lift span into operation. The old 1874 rail bridge was retained while these works occurred, allowing for traffic to be diverted to the old structure while completing the lift span towers in 1943-44. In mysterious circumstances, the old rail bridge caught fire in October 1945. The fire brigade were advised to let it burn, reducing demolition costs, but in the end only three spans were destroyed.⁵⁹

Completion of the bridge towers and lifting mechanism were delayed by the Second World War, with the lifting span coming into operation in 1946. On completion, three bridges existed at the crossing: the new steel bridge combining road and rail traffic, and the old separate rail and road bridges. As a result, shipping had to zig-zag between them to navigate up stream.⁶⁰

The new bridge started carrying rail in October 1946, in combination with a new station layout at Bridgewater. On completion, the old rail bridge was progressively demolished. The full width of the opening span was not available until 20 February 1946. It was take four more years before the old piles were removed from the River, the key survivor being the massive steel and concrete caisson which supported the swing span of the 1893 bridge.⁶¹

The extra costs of the lift span proved a wise investment. By 1946, the Paper Company favoured barging newsprint from Boyer to Hobart. Increased production at the factory resulted in growth in river traffic. In 1947-48, less than 400 vessels made the crossing at Bridgewater, but growing to just over a 1,000 in 1956 and 1,300 by 1969-70. The largest number of openings on a single day was 26 for the New Norfolk Regatta. The only vessels that ever needed the full height of the lifting span were a few of the Sydney-Hobart maxi yachts which ventured this far upstream. River transport to and from Boyer was progressively dropped, ceasing completing in 1986. As a result the number of bridge openings declined markedly. In 1987-88, the bridge opened less than one hundred times.⁶²

The combination of road and rail on the bridge required extra safety precautions to be installed to prevent trains crossing the bridge whilst it was lifted. The solution was the interlocking of the power supply for the lifting mechanism and the signal station at the rail station, and human operation of the switches and signals. All physical systems for safe operation of the lift span were replaced with telephone rail orders in the 1980s.63

Like all structures, the Bridgewater Bridge has undergone a series of modifications since construction.

In 1951, the renewed Bridgewater railway station and its signalling equipment was destroyed by a fire. At first, the bridge rail locks which lowered and raised the opening span were operated by hand, which could be slow, particularly during high winds. These were later replaced with hydraulic cylinders to operate the locks from the machinery house located above the lift span.

⁵⁶ GHD, 2009, p.197

- 59 GHD, 2009, p.199
- ⁶⁰ GHD, 2009, p.199

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⁵⁴ GHD, 2009, p.197

⁵⁵ GHD, 2009, p.197: Parliamentary Standing Committee on Public Works, 1937, pp.1-4

⁵⁷ GHD, 2009, p.197

⁵⁸ GHD, 2009, p.198: Whitlam, pp.73-74; Austral Archaeology 1996, p.12

⁶¹ GHD, 2009, pp.199-200

⁶² GHD, 2009, p.200

⁶³ GHD, 2009, p.200

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Changing rail demands also led to changes to the Bridge. During the 1960s, railway infrastructure was modified to cope with the heavy loads required for the Gordon Power Development project. At Bridgewater, this required the lowering of the rail tracks by 44.45 cm.⁶⁴

Extra steel plates were welded to the under deck girders between 1987-1989 to increase the load limit of the bridge to its maximum limit. The transmission line towers and cables which ran alongside the bridge and causeway were also removed during this time.

The lift span was also subject to structural changes in the 1980s to increase its load capacity. The works included strengthening of the welded plate girders by the addition of plates to the top and bottom flanges and strengthening of piers by the application of transverse steel beams encased in concrete.

The addition of plates to the top and bottom flanges of the girders had the unintended effect of significantly distorting the girders so that they separated from the bridge deck, and in time causing corrosion. The issue was addressed by the addition of grout into the voids. Additional steel cleats were also added to the deck to provide full lateral restraint of the girders.⁶⁵

In 1992 the southern end of the bridge and the causeway was raised and reconstructed, including some vertical realignment of the causeway over a distance of some 150 metres.⁶⁶

The continued settlement of the causeway has resulted in horizontal displacement of sediments, which in turn apply horizontal loads to the piles. Since construction in 1942, settlement in the order of 60 cm has occurred and continues to be an ongoing issue. 67

Some of the most significant refurbishment took place during the early 2000s. Substantial deterioration had been identified in 2006 in some of the bridges counterweight ropes, at their connections with the 170 tonne counterweights. Addressing the risk of rope failure, the bridge was closed for a two week period to allow for close inspection and the design of an alternative counterweight suspension system. This alternative system remained in place until 2010 when it was removed as part of the last major refurbishment project. The closure of the lift span temporarily stranded larger vessels upstream.⁶⁸

The temporary support arrangement for the lift span was not a permanent measure. It also made it more difficult to maintain the ropes and other components. Refurbishment of the bridge and restoration of the operation of the opening span was identified as the appropriate response. Works carried out as part of this major refurbishment were extensive, replacing certain equipment, and making repairs and enhancements. Repairs were generally like-for-like to maintain the heritage values of the bridge. It included:

- Full containment, grit blasting and repainting all plate girder approach spans to safely remove the lead-based paint, rectify steel corrosion and apply a new protective coating;
- The installation of new cathodic protection⁶⁹ systems for the concrete piers. On opening the piers for the repair and installation of 2. the protection system, it was found that not only was there insufficient concrete cover for the installation of a new system, but that the original anodes had damaged the pier reinforcement. The installation of new cathodic protection was therefore abandoned, and work instead focussed on repairing damaged reinforcement and concrete.
- Structural repair of areas of the steel superstructure and concrete piers, with inclusion of cleats to the plate girders of the approach 3 spans to provide them with full lateral restraint. Additional steel repairs were required including reattachment of a large number of braces to the steel plate girders.
- 4. Works were proposed to investigate or stabilise settlement of the causeway, although more urgent works were carried out instead.
- Restoration of the opening lift span and upgrading the electrical and mechanical systems to meet current standards. This included 5 replacement of the motors, a programmable logic control, electro-hydraulic brakes and improved guarding to reduce reliance on manually operated brakes and improve safety.⁷⁰

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⁶⁴ GHD, 2009, p.200

⁶⁵ Fowler, ob. cit., p.8

⁶⁶ Department of Transport, Materials & Research, Derwent River Crossing at Bridgewater. Office Study Geotechnical Report, File No. 2.0082, Report No. 2508/1, 24 June 1996

⁶⁷ Fowler, op. cit., p.6

⁶⁸ Fowler, *op. cit.*, p.6

⁶⁹ i.e., a technique used to control the corrosion of a metal surface by making it the cathode of an electrochemical cell.

⁷⁰ Fowler, *op. cit.*, pp.9-10



HERITAGE LISTING

The Bridgewater Crossing including causeway and bridge has been assessed as having State level significance, recognised in its inclusion on the Tasmanian Heritage Register (THR) ID 618. The site is therefore subject to the Historic Cultural Heritage Act 1995 (HCHA 1995).

The Crossing is also included in Table E13.1 of the Heritage Code of the Brighton Interim Planning Scheme 2015 (BIPS 2015) as "Bridgewater Bridge (CT134751/4)".

ASSESSED HISTORIC CULTURAL HERITAGE SIGNIFICANCE

The following assessment of the Bridgewater Crossing including Statement of Significance has been extracted from the Memorandum: Review of assessment of significance against state criteria/threshold, prepared by Purcell, dated 12 October 2020:

The Bridgewater Causeway and Bridge forms part of a broader and significant cultural landscape which has historical importance with regard to the evolution of transport, and which concentrates at this point of the Derwent. Serviced first by ferries, then later the causeway, road and rail traffic, the place is arguably the focus of Tasmania's most historically important transport route.

The Bridgewater crossing as a major piece of civil infrastructure forms part of a suite of places including roads, bridges, dams and water supply systems. It is important as one of the largest items of civil infrastructure constructed in Van Diemen's Land using convict labour. The Bridgewater Causeway has the potential to enhance an understanding of early civil engineering construction from the early nineteenth century generally and more specifically a greater understanding of the construction methods employed to address the very difficult geological conditions encountered throughout its history.

The Bridgewater Bridge is rare as Tasmania's only surviving lift span bridge and is the largest surviving lift span bridge in Australia. The steel truss approach and lift spans demonstrate the early use of all welded connections in steel truss bridges and the early adoption in Tasmania of design details specifically to address the issue of fatigue. The Bridgewater Bridge is important in demonstrating the key characteristics of a lift span metal truss rail and road bridge. The extensive archive of construction documentation and engineering studies and has the potential to yield information as to historical advances made in welding details, and their long term performance.

The Bridgewater Causeway has a special association with the work of convict labour in the construction of major civil engineering projects during the first half of the nineteenth century. It is also important for its association with Governor Arthur. The Bridgewater Bridge is an important example of the work of engineer Sir Allan Knight. The place has special associations to Engineers Australia who have recognised its technical significance with an Engineering Heritage National Marker in 2018.

"The place is important to the course or pattern of Tasmania's history" a)

The Bridgewater Causeway and Bridge forms part of a broader and significant cultural landscape which has historical importance with regard to the evolution of transport, and which concentrates at this point of the Derwent.

Serviced first by ferries, then later the causeway, road and rail traffic, the place is arguably the focus of Tasmania's most historically important transport route.

The causeway was one of the largest items of civil infrastructure constructed in Van Diemen's Land using convict labour. It demonstrates the scale of public works that could be carried out by convict labour, which was the key workforce available during the first half of the nineteenth century. The length of time to construct the causeway, and the methods used to address the very difficult geological conditions are a testament to the work carried out by the convict workers.

Following completion, the causeway formed the point of construction for all future bridges. Evidence of the 1874 and 1893 bridges exists on the causeway and northern bank of the Derwent. Subsurface evidence of the 1849 bridge abutments may also exist on the northern bank. The current Bridgewater Bridge is of historical importance in demonstrating the development of civil infrastructure by the Public Works Department, during a period of great innovation and technical advancement in the 1930s.

The bridge is also historically significant with its association with a major phase of industrialisation in Tasmania, and in particular the development of the paper industry in the Derwent Valley. The bridge was specifically designed to help facilitate this industry through the provision of both rail and river navigation capabilities.

"The place possesses uncommon or rare aspects of Tasmania's history" b)

The causeway is a rare place. It is one of only two causeways constructed in the state during the early nineteenth century using convict labour. It is considerably larger in length and volume than the Hunter Island causeway, being the other convict built causeway.

The Bridgewater Bridge was Tasmania's second, and the only surviving lift span bridge. It is also the largest surviving lift span bridge in Australia. It is the largest and one of relatively few metal truss road bridges in Tasmania, and is a relatively early example of an all welded bridge.

"The place has the potential to yield information that will contribute to an understanding of Tasmania's history" c)

The Bridgewater Causeway has archaeological research potential. Detailed documentary evidence of its construction methods is limited. It offers opportunities to understand civil engineering construction from the early nineteenth century and methods to address the very difficult geological conditions over an extended period.

The Bridgewater Bridge has research potential to provide new information on bridge design and construction, and in particular, advances made in welding details, and their long term performance.

"The place is important in demonstrating the principal characteristics of a class of place in Tasmania's history" d)

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The Bridgewater Causeway is an important example of large scale civil infrastructure that was built during the first half of the nineteenth century using convict labour. It forms part of a suite of places including roads, bridges, dams and water supply systems.

The Bridgewater Bridge is important in demonstrating the key characteristics of a lift span metal truss road bridge. It is a 'Pratt' type of truss in a half-through configuration. The truss consists of vertical diagonals that slope down towards the centre. Constructed from welded steel, the bridge demonstrates the essential truss form of light weight construction with a hollow skeletal structure formed from vertical, horizontal and diagonal chords creating the essential triangular section of the truss bridge type.

e) "The place is important in demonstrating a high degree of creative or technical achievement"

The Bridgewater Bridge is important in demonstrating a high degree of technical achievement. The steel truss approach spans and the lift span demonstrate the early use of all welded connections in steel truss bridges and the early adoption of design details specifically to address the issue of fatigue. It was designed and constructed some ten years after the world's first all welded bridge, and within a number of years of Tasmania's entry into this technology. Recent investigations have shown that some of the details originally incorporated to reduce susceptibility to metal fatigue are now considered susceptible to fatigue.

Innovative research was carried out and the weld details were designed to address problems with fatigue and brittle fracture.

f) "The place has a strong or special association with a particular community or cultural group for social or spiritual reasons"

No social values assessment has been carried out for this project. The following provides an indicative statement of values which may exist at the place.

The Bridgewater Causeway and Bridge are prominent landmarks and mark the northern entrance to Hobart. It has been the key crossing point of the Derwent since the 1830s.

The causeway and bridge may have strong or special associations with engineers as a group. Engineers Australia has recognised the Bridge with an Engineering Heritage National Marker in 2018.

g) "The place has a special association with the life or works of a person, or group of persons, of importance in Tasmania's history"

The Bridgewater Causeway has a special association with the work of convict labour in the construction of major civil engineering projects during the first half of the nineteenth century. It is among the largest items of infrastructure in Tasmania which demonstrates this association. The causeway is also important for its association with Governor Arthur and various government engineers and officials who designed and oversaw its construction. This includes Inspector of Roads and bridges Roderic O'Connor, and architect and engineer John Lee Archer. The Bridgewater Bridge is an important example of the work of engineer Sir Allan Knight. Knight enjoyed a highly successful career with the Public Works Department and later the Hydro Electric Commission.

He was the designer of a number of technologically advanced bridges including at Vincents Rivulet and the Leven River, and was closely involved with the three bridges across the Derwent – the floating bridge at Hobart, Bridgewater Bridge and the Tasman Bridge. Knight received many awards and honours during his career and was made a Knight Bachelor in 1970.

h) "The place is important in exhibiting particular aesthetic characteristics"

The Bridgewater Bridge is the dominant visual landmark in an aesthetically important cultural landscape, strongly associated with the evolution of transport. This evidence is layered in the landscape, and includes large and small elements.

The bridge with its high towers and distinctive truss forms are landmarks of the area, with important views to the structure available from surrounding road networks.

The still waters of the Derwent at this location and frequent presence of large flocks of Black Swans contribute to the setting of the place.

PHOTOGRAPHIC DOCUMENTATION

CAMERA AND LENS SPECIFICATIONS

The photographs that form this Archival Record were taken with a 50mm camera digital equivalent, meeting the requirements of the NSW Heritage Office Guidelines for Photographic Recordings. The camera and lens specifications are as follows:

Camera Canon 7D Digital SLR (18 Megapixel)

Lens Canon 70-200mm, 50mm

IMAGE FORMAT

The photographs were taken at 18 megapixels in RAW format and converted to high resolution TIF format (approx. 3MB to 6MB each), in accordance with the NSW Heritage Office Guidelines for Archival and Photographic Recordings. The digital copies of this Archival Record comprise each photograph in both RAW, TIF and JPEG format, as well as thumbnail sheets with reference numbers.

PHOTOGRAPHIC CATALOGUE

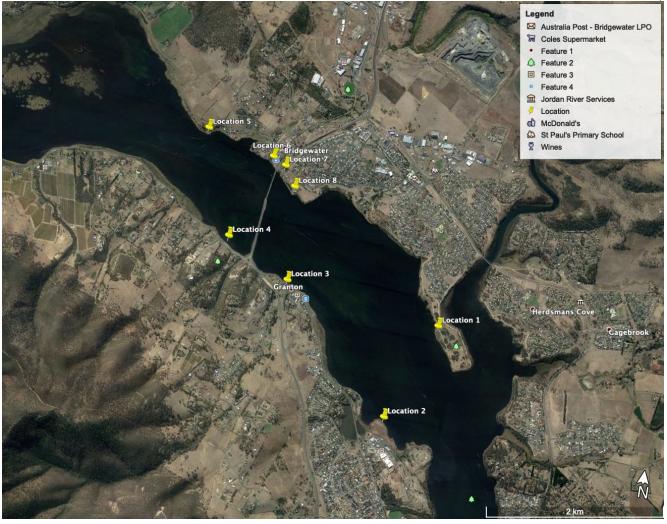
This Archival Record comprises the following sections, consistent with the NSW Heritage Office Guidelines:

- Plan Sheets documenting the location of each photograph using markers (Appendix I);
- Catalogue Sheets comprising detailed descriptions of each photograph, orientation of photographs and cross-references to both plan sheets and thumbnail images (Appendix 2);
- Thumbnail Sheets comprising a thumbnail of each photograph and reference numbers (Appendix 3);
- Selection of Photographs comprising a selection of photographs that capture the Crossing and setting (Appendix 4);
- Historic Photographs & Drawings a selection of historic photographs sourced from Libraries Tasmania and original and early drawings of the bridge sourced from the Department of State Growth comprising survey, plan, elevation, section and detail drawings (Appendix 5), and;
- Point Cloud Survey, Sample Views prepared by JACOBS and comprising sample views of the model (Appendix 6).

DISTRIBUTION

Digital copies of this Archival Record are to be distributed to the Department of State Growth, Heritage Tasmania and the Tasmania Heritage and Archive Office.

APPENDICES APPENDIX I - PLAN SHEET



			Project	Bridgewater	Crossing Archival Red	cord
h, all			Camera	0	U	non 70-200mm, 16-35mm, 50mm
PURCELL			Date Taken	22/03/21	Photographer	Martin Passingham
Image No.	View	Description	Dute Fullen	22/05/21	i notogi upitel	
-		Reference: 100]				
BWC_01	NW	IMGL4860 22/03/21 4.34pm Wide	angle 70-200 f/LL Vie	wed from Locatio	on L East elevation	
BWC_02	NW	IMGL4861 22/03/21 4.35pm Mediu	0			
BWC_03	NW	IMGL4958 21/05/21 8.45am Wide	0			
BWC_04	NW		0			
BWC 05	NW	IMGL4960 21/05/21 8.45am Medium angle 70-200 f/6.3. Viewed from Location 2, East elevation. IMGL4961 21/05/21 8.45am Wide angle 70-200 f/9. Viewed from Location 2, East elevation.				
BWC_06	NW	IMGL4962 21/05/21 8.45am Wide	0			
BWC_07	NTH	IMGL4939 22/03/21 5.49pm Mediu	-			
BWC_08	NTH	IMGL4940 22/03/21 5.49pm Mediu	-			
BWC_09	NTH	IMGL4949 21/05/21 8.34am Mediu	-			
BWC_0	NTH					
BWC_11	NTH	IMGL4950 21/05/21 8.34am Medium angle 70-200 f/5.6.Viewed from Location 3, East elevation. IMGL4954 21/05/21 8.35am Wide angle 70-200 f/8.Viewed from Location 3, East elevation.				
BWC_12	NE	IMGL4912 22/03/21 5.31pm Wide	0			
BWC_12 BWC_13	NE	IMGL4913 22/03/21 5.31pm Mediu	-			
BWC_14	NE		0			
BWC_14 BWC_15	NE	IMGL4914 22/03/21 5.31pm Mediu IMGL4917 22/03/21 5.31pm Wide	0			
BWC 16	NE	IMGL4918 22/03/21 5.32pm Mediu	0			
BWC_17	NE	IMGL4919 22/03/21 5.32pm Mediu	-			
BWC_18	NE	IMGL4923 22/03/21 5.33pm Mediu	0			
BWC_18 BWC 19	NE	IMGL4923 22/03/21 5.33pm Mediu	0			
BWC_20	NE					
BWC_21	SE	IMGL4926 22/03/21 5.40pm Medium angle 70-200 f/4.5. Viewed from Location 4, South Elevation IMGL4877 22/03/21 5.06pm Wide anglw 16-35 f/8. Viewed from Location 5, West elevation				
BWC_22	SE	INGL4677 22/03/21 5.06pm Wide angle 70-200 f/6.3. Viewed from Location 5, West elevation.				
BWC_23	SE					
BWC_24	SE	IMGL4879 22/03/21 5.07pm Medium angle 70-200 f/5.6. Viewed from Location 5, West elevation.				
BWC_25	SE	IMGL4880 22/03/21 5.08pm Medium angle 70-200 f/6.3. Viewed from Location 5, West elevation. IMGL4881 22/03/21 5.08pm Medium angle 70-200 f/5. Viewed from Location 5, West elevation.				
BWC_26	SE	INGL4884 22/03/21 5.09pm Wide angle 50mm f/7.1. Viewed from Location 5, West elevation. IMGL4884 22/03/21 5.09pm Wide angle 50mm f/7.1. Viewed from Location 5, West elevation.				
BWC_27	STH	INGL4664 22/03/21 5.05pm Wide angle Somm 17.1. Viewed from Location 6, North elevation. IMGL4885 22/03/21 5.14pm Medium angle 16-35 f/7.1. Viewed from Location 6, North elevation.				
BWC_28	STH	IMGL4886 22/03/21 5.14pm Medium angle 16-35 f/7.1. Viewed from Location 6, North elevation.				
BWC_29	STH	INGL4666 22/03/21 5.14pin Heddin angle 16-35 ///1. Viewed from Location 6, North elevation.				
BWC_30	STH	IMGL4892 22/03/21 5.16pm Mediu				
BWC_31	STH	IMGL4896 22/03/21 5.17pm Mediu	-			
BWC_32	STH	IMGL4905 22/03/21 5.1 9pm Medium angle 16-35 f/8. Viewed from Location 6, North elevation.				
BWC_33	STH	IMGL4097 22/03/21 5.20pm Mediu				
BWC_34	SW	IMGL4991 21/05/21 9.23am Mediu	m angle 16-35 f/14. Vie	wed from Location	on 7, North East elevation	
BWC_35	SW	IMGL4995 21/05/21 9.25am Mediu	n angle 16-35 f/11. Vie	wed from Location	on 7, North East elevation	
BWC_36	SW	IMGL4997 21/05/21 9.26am Close angle 16-35 f/13. Viewed from Location 7, North East elevation.				
BWC_37	SW	IMGL4998 21/05/21 9.26am Mediu	m angle 16-35 f/14. Vie	wed from Location	on 7,North East elevation.	
BWC_38	W	IMGL4970 21/05/21 9.03am Close angle 16-35 f/14. Viewed from Location 8, East elevation.				
BWC_39	W	IMGL4973 21/05/21 9.08am Wide	angle 16-35 f/13. Viewe	ed from Location	8, East elevation.	
BWC_40	W	IMGL4975 21/05/21 9.09am Wide	0			
BWC_41	W	IMGL4978 21/05/21 9.13am Wide				
BWC_42	W	IMGL4981 21/05/21 9.17am Wide angle 16-35 f/13. Viewed from Location 8, East elevation.				
BWC_43	W	IMGL4982 21/05/21 9.18am Wide				
BWC_44	w w	IMGL4984 21/05/21 9.19am Mediu	0			
BWC_45	W	IMGL4987 21/05/21 9.20am Mediu	ě			
BWC_46	٧V	IMGL4990 21/05/21 9.21am Mediu	n angle 16-35 1/13. Vie	wed from Location	on o, east elevation.	



BWC_01

BWC_02

BWC_03



BWC_04

BWC_05

BWC_06



BWC_07



BWC_08



BWC_09



BWC_10

BWC_11



BWC_13

BWC_14

BWC_15



BWC_16

BWC_17

BWC_18







BWC_23



BWC_25

BWC_26

BWC_27



BWC_28

BWC_29

BWC_30



BWC_33



BWC_34

BWC_35



BWC_37

BWC_39



BWC_41

BWC_42



BWC_43



BWC_44



BWC_45



BWC_46

APPENDIX 4 – SELECTION OF PHOTOGRAPHS

Bridgewater Crossing Archival Record - Selection of Photographs



BWC_01



Bridgewater Crossing Archival Record - Selection of Photographs





BWC_20



BWC_31

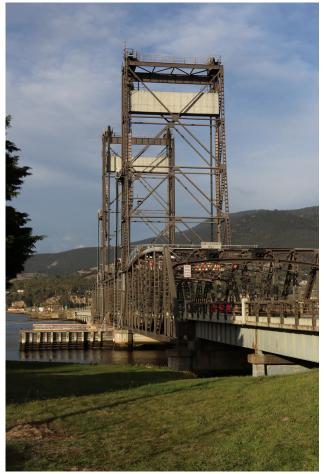


BWC_34

Bridgewater Crossing Archival Record - Selection of Photographs



BWC_38



BWC_44

APPENDIX 5 – HISTORIC PHOTOGRAPHS & DRAWINGS



Elevator Bridge, Bridgewater in 1956 Source: Libraries Tasmania | Item no. AB7 13/1/5677



Tugboat with barges from APPM Boyer passing under the Bridgewater Elevator Bridge in 1957 Source: Libraries Tasmania | Item no. AB7 13/1/5575



Bridgewater Bridge, looking towards Bridgewater in 1962 Source: Libraries Tasmania | Item no. AB7 13/1/8196



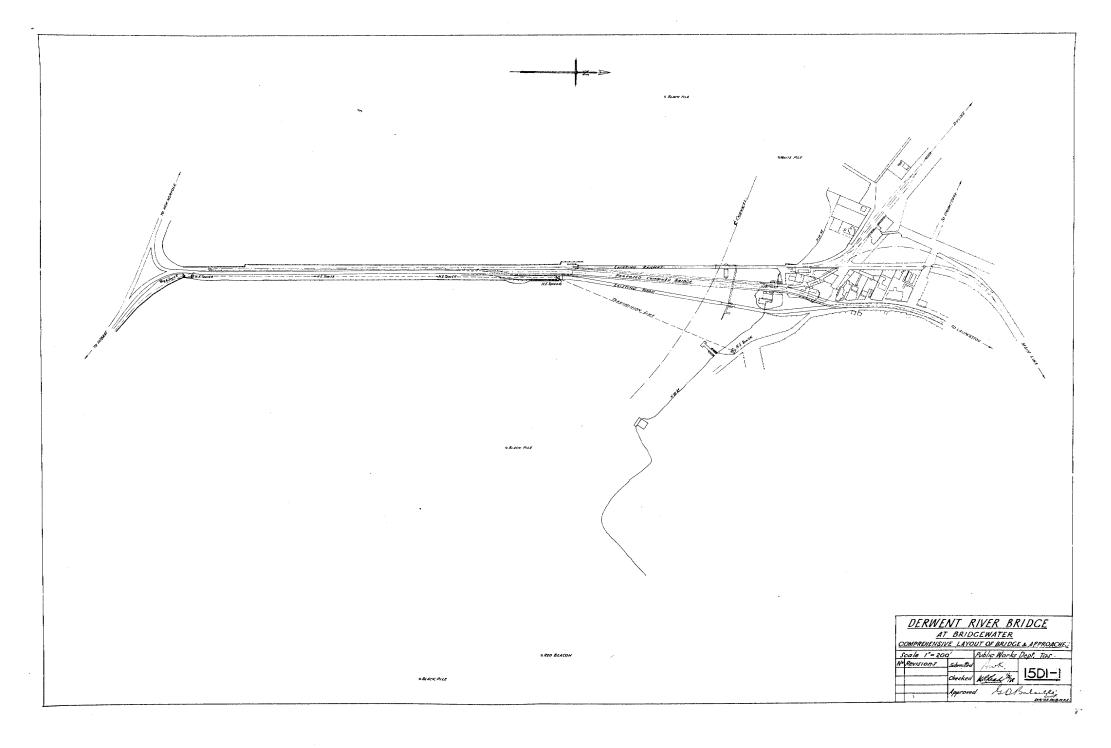
Aerial photograph of the Bridgwater Crossing and Derwent River in the 1970s Source: Libraries Tasmania | Item no. AB7 13/1/11238

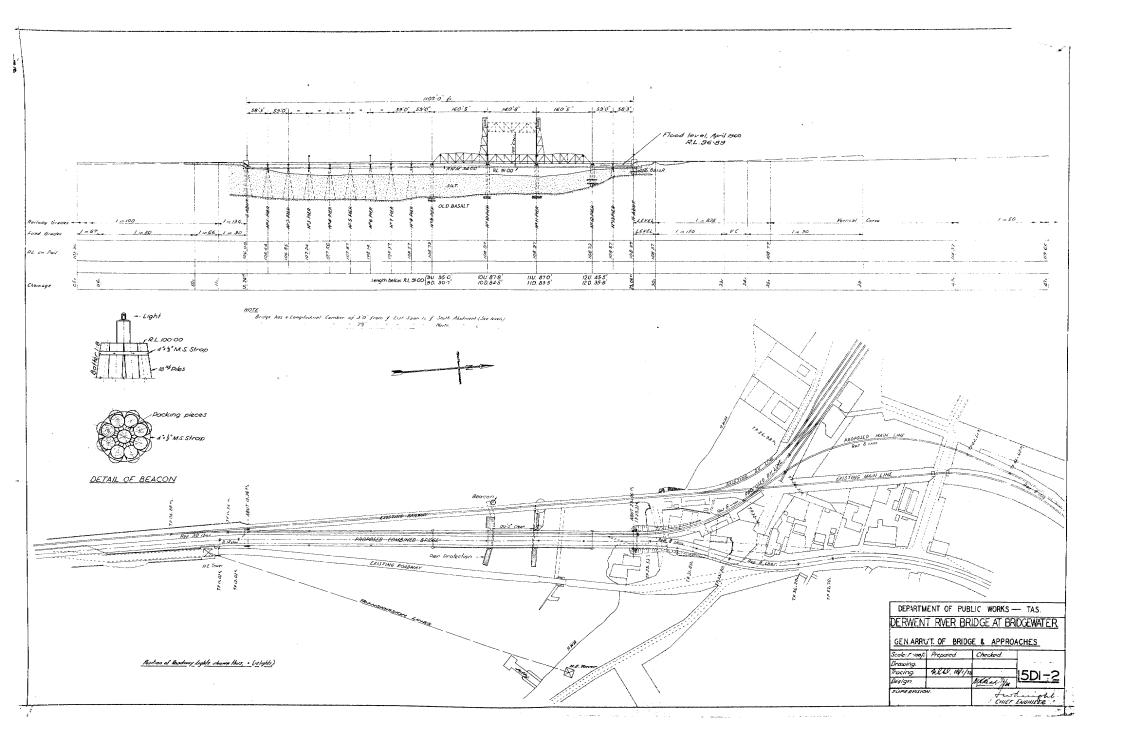
Page No	DrawingNo	Name1	Name2
	D1	PRELIMINARY WORK - SURVEYS, ETC	
2	D1-01	COMPREHENSIVE LAY OUT	
3	D1-02	GENERAL ARRANGEMENT OF	BRIDGE AND APPROACHES
4	D1-03	LONGITUDINAL SECTION OF	RIVER BED AND BORINGS
5	D1-04	RAILWAY LONGITUDINAL SECT-	ION AND ROAD DEVIATION
	D1-05	ROAD PLAN	
6	D1-06	NORTHERN APPROACH CROSS	SECTIONS
7	D1-07	RAILWAY AND ROAD DEVIATION	SECTIONS
8	D1-08	SOUTHERN APPROACH PLAN	
9	D1-09	BRIDGE SUPERSTRUCTURE	
	D1-10	NORTHERN APPROACH PLAN	
10	D1-11	DOWN STREAM NORTHERN SIDE	FORESHORE
	D1-12	SOUTHERN END OF BRIDGE	
	D1-13	BRIDGE WIDENING FOR	DEVIATION
	D1-14	SOUTHERN END FALSEWORK	
11	D1-15	NORTHERN ABUTMENT SOUNDINGS	
	D1-16	SOUTHERN ROAD APPROACH	LONGITUDINAL SECTION

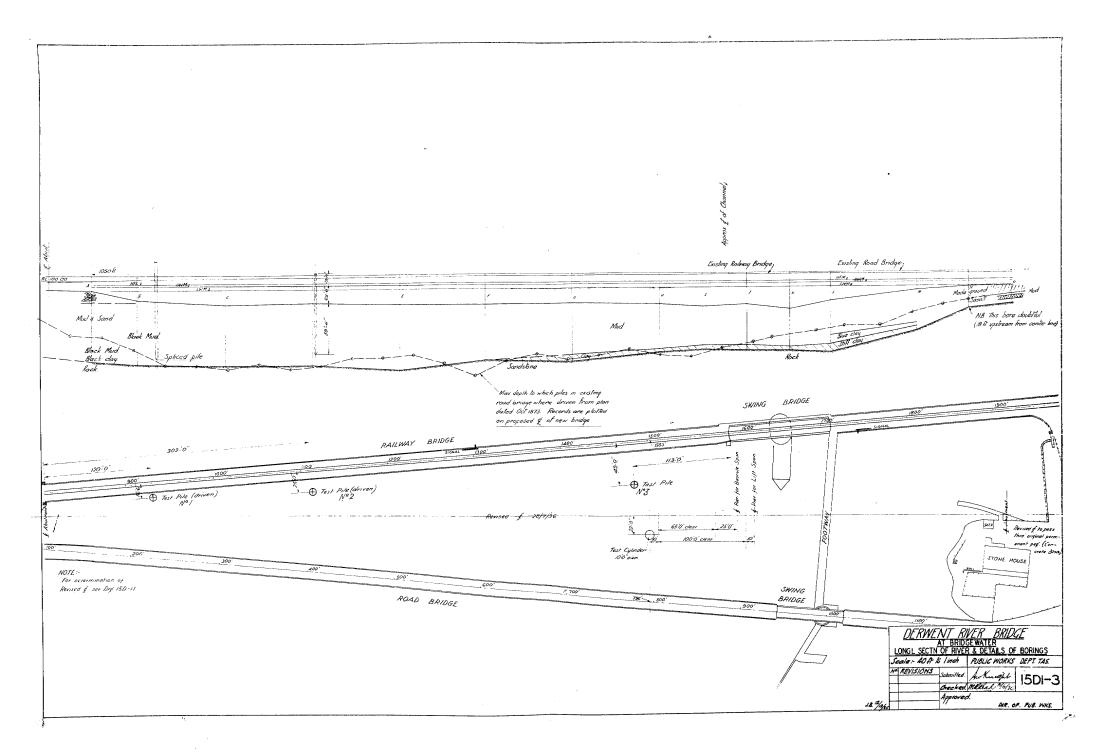
BRIDGEWATER BRIDGE

D1 - PRELIMINARY WORK

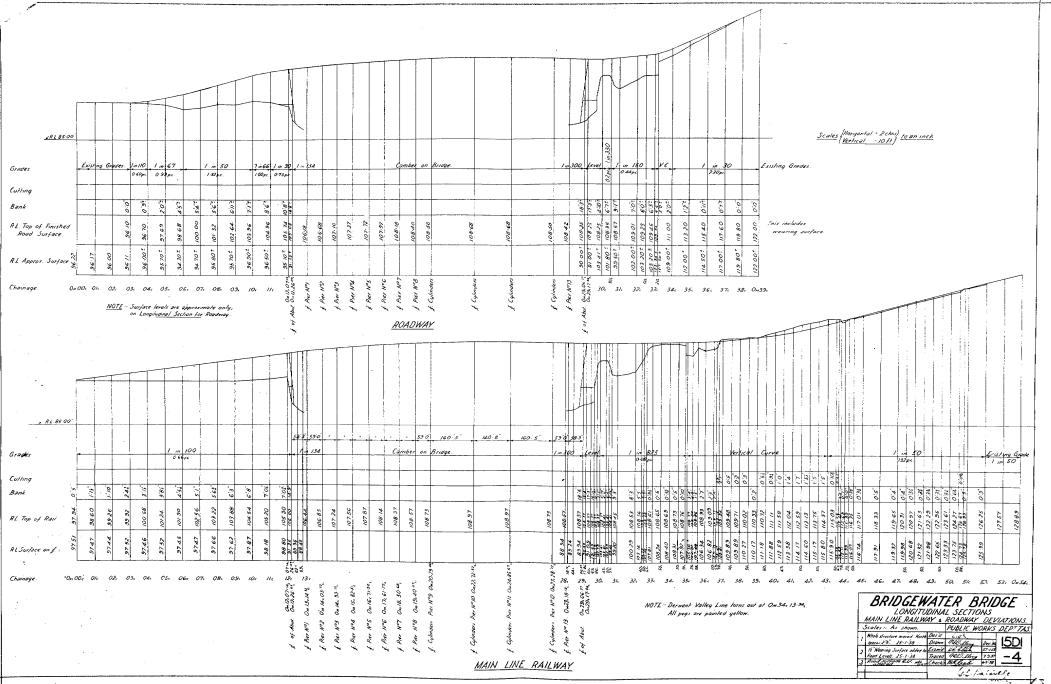
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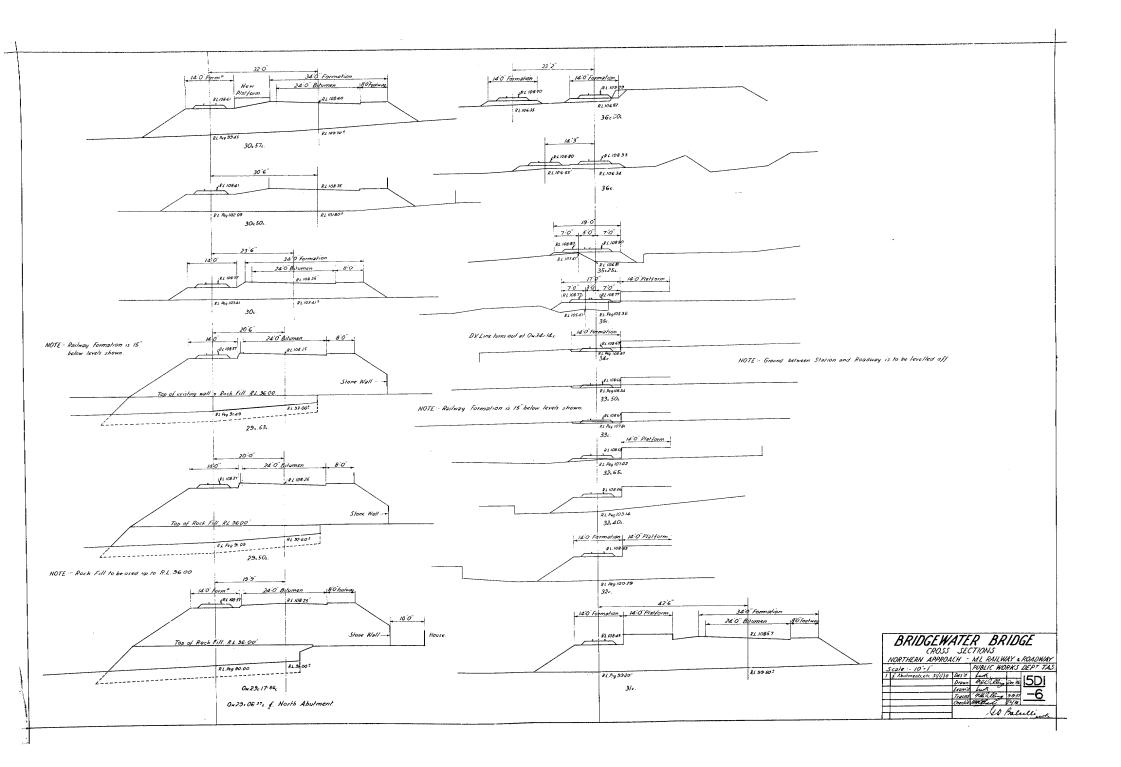


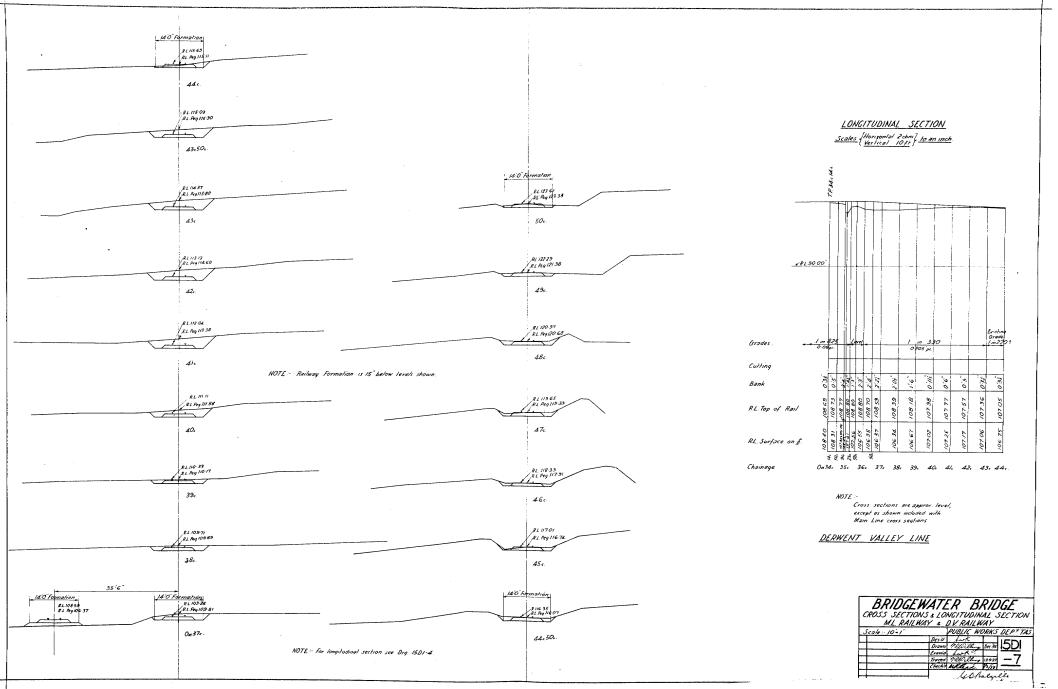




ANTER ALL



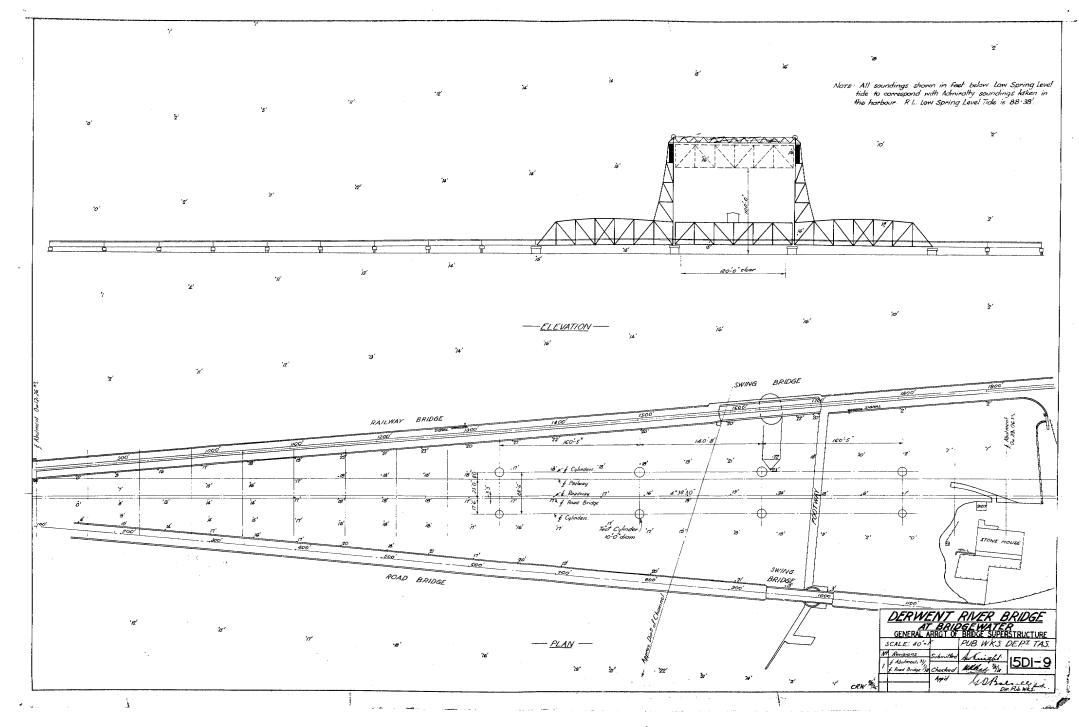


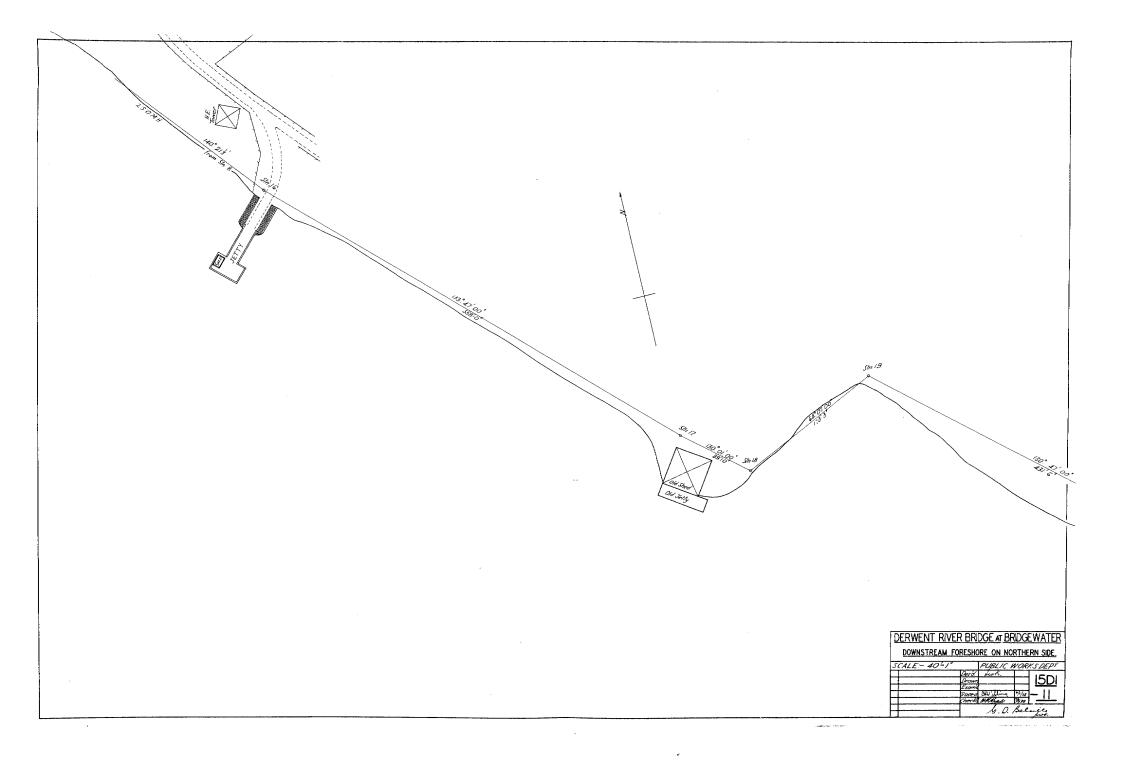


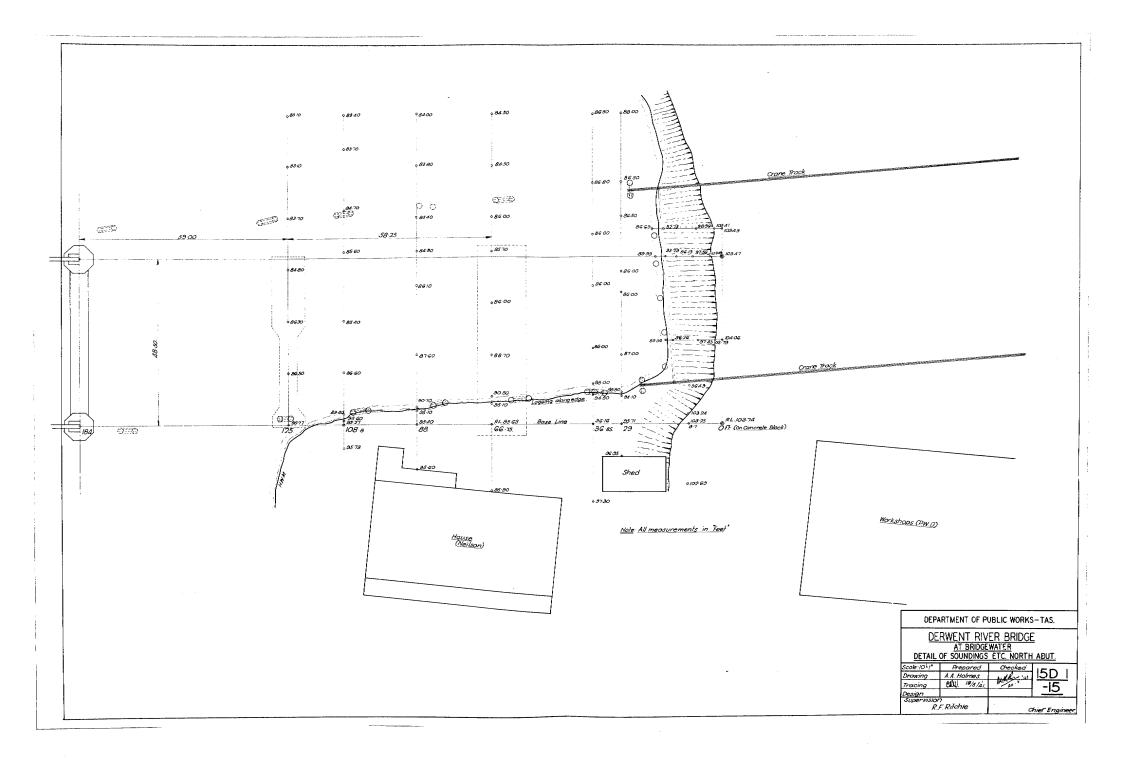
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THE THE APP Stn 14 Stat New Fence Rod. 30 cmis Tel Pole Rad. 12 chas. Way 238 30" I Road Bridge <u>अस्य स्वयं प्रस्य अस्य</u> Hew Fence 57 171717777777777777777777 10/11 and the second of the product of the first of the second sec 5. h. Le between minde fores Lifed 1 - 48 bothing 8 He 231 61 DERWENT RIVER BRIDGE AT BRIDGEWATER Southern Approach 1"-40" PUBLIC WORKS DEPT TAS Scale 1'= 40' Nº Revisions Submittee <u>|5D|-8</u> Checked Miller 1/19. Appril "Il talculle" *

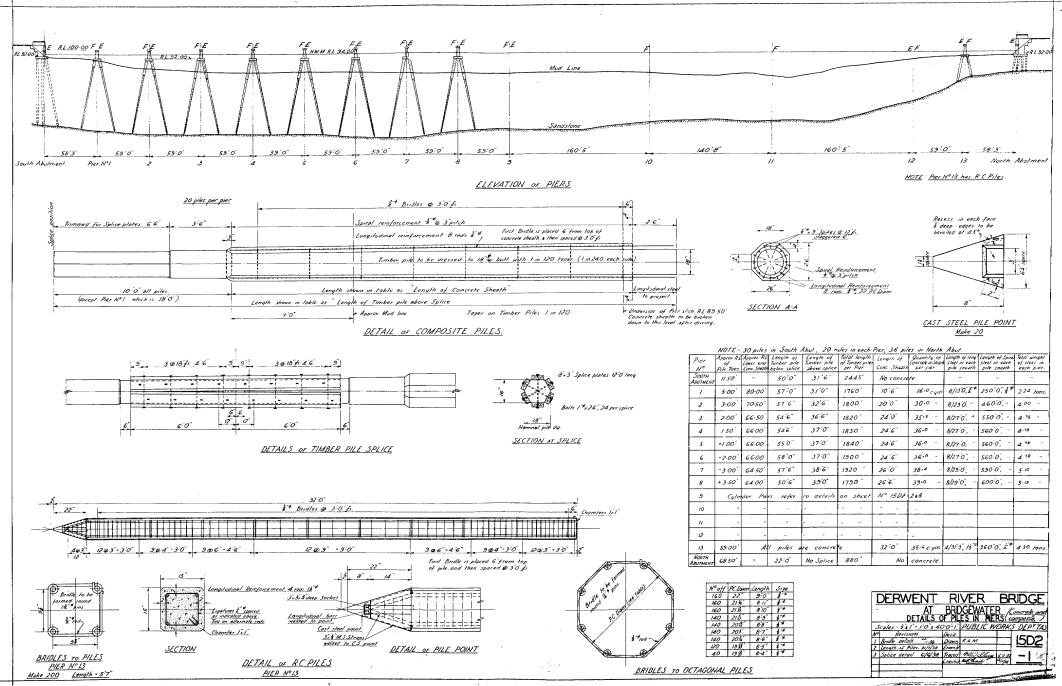






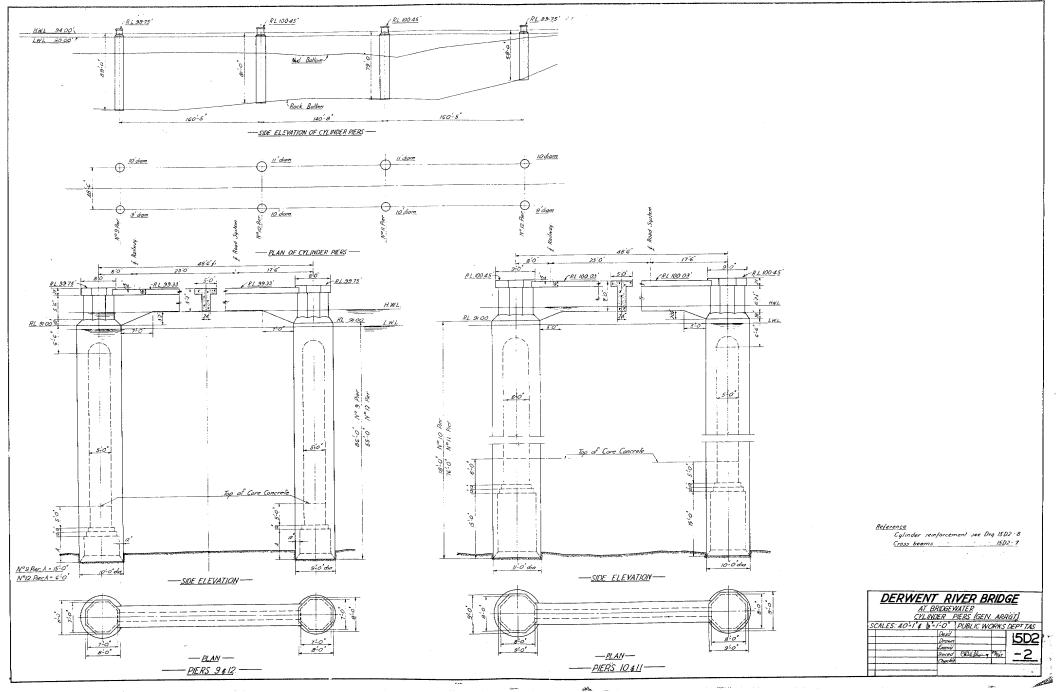
⊃age No	DrawingNo	Name1	Name2	Name3
	D2	SUBSTRUCTURE - CYLINDERS,	PIERS AND ABUTMENTS	
2	D2-01	PILES IN PIERS (CONCRETE	AND COMPOSITE)	
3	D2-02	GENERAL ARRANGEMENT OF	CYLINDER PIERS (1937)	
4	D2-03	SOUTHERN ABUTMENT	FOR SETTLEMENT SEE 15/D7-32	
	D2-04	NORTHERN ABUTMENT	SEE 15/D2-16 AND 17	
5	D2-05	PIER NOS 1 TO 8 AND 13		
6	D2-06	ABUTMENT AND PIER	REINFORCEMENT SCHEDULES	
7	D2-07	PIER NOS 9 TO 12 CROSS	BEAMS	
8	D2-08	9, 10 AND 11 FEET DIA	CYLINDERS	
9	D2-09	CYLINDER FALSEWORK AND	LOWERING GEAR	
10	D2-10	BOX GIRDERS FOR LOWERING 9	AND 10 FEET DIA CYLINDERS	AND CUTTING EDGE
11	D2-11	PILE PIERS FORMWORK SYSTEM		
	D2-12	PIER NOS 11 AND 12 FORMWORK		
12	D2-13	PYLONS AND LIGHT STANDARDSINU		
13	D2-14	PIER NOS 9 AND 12 BEAM	ARRANGEMENT	
14	D2-15	PIER NOS 10 AND 11 LIFT	SPAN BEARING WELLS	
15	D2-16	GENERAL ARRANGEMENT OF	NORTHERN ABUTMENT	
16	D2-17	NORTHERN ABUTMENT		
17	D2-18	NORTHERN ABUTMENT TIE BAR	AND ANCHOR	
18	D2-19	PIER PROTECTION		
19	D2-19A	PIER PROTECTION EXTENSIONS		
20	D2-20	PIER NO 11 PROTECTION		
	D2-21	RIVER BED PROFILE (1973)		
21	D2-22	PIER INOS 4 AND 6 STEM	RESTORATION AND FALSEWORK	
22	D2-23	PIER NOS 9 TO 12 CROSS BEAM	STRENGTHEINING	GENERAL ARRANGEMEN
23	D2-24	EXISTING CROSS BEAM	PREPARATION	
24	D2-25	GIRDER FABRICATION		
25	D2-26	GIRDER INSTALLATION		
26	D2-27	CONCRETE AND REINFORCEMENT		

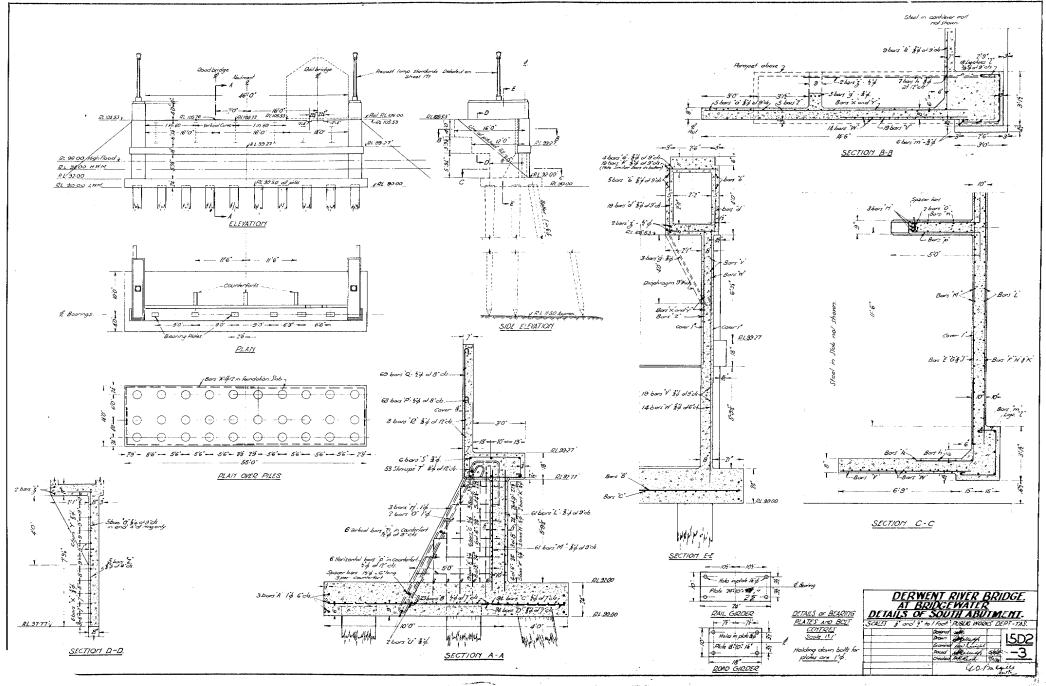
BRIDGEWATER BRIDGE D2 - SUBSTRUCTURE TABLE OF CONTENTS

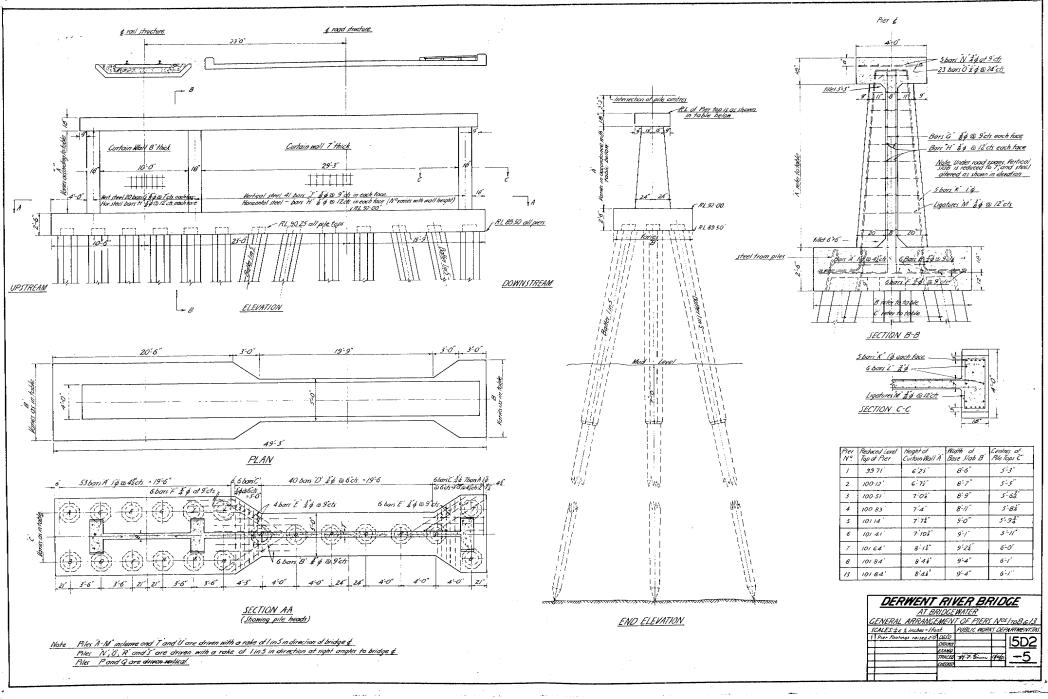


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STEEL LIST FOR	OUTH ABUTMENT DR	G.I5D2-3	STEEL LIST FOR NORTH ABUTMENT DRG 1502-4
Mark Noff Length Size World Length Weig	ht Shape	Remarks	Mark Nº off Length Size Order List Weight Shape
AS 12 380 10 12 18 577	See detail	To outside of Footing	AN 12 380 14 12 18 91/105 See detail To outside
BS 23 540 1 69 18 829		Longitudinals in footing	BN 23 540 24 69 18' 829" Straight welded Longituding
CS 94 13-6 24 94 14 879		Transverse in footing	CN 94 136 19 94 14 879 "Itraight Transverse
DS 94 50 84 24 20 180	~ .	" (toe)	DN 94 50 34 24 20 180
ES 9 480 24 27 16 28	· Straight welded	Horizontals in back of abut wall (bottom)	GN 9 48-0 14 27 16 289 " Straight welded Horizontals
FS 5 480 20 15 16 160		front	HN 5 480 14 15 16 160
65 6 480 ±9 18 16 192	e e	" back " " (middle)	JN 8 480 24 24 16 256"
HS 3 480 24 9 16 96		front "	KN 4 480 24 12 +6 128"
JS 5 480 24 15 16' 160	r		LN 61 90 84 32 18 217 " Verticals
KS 2 480 19 6 16 64	6 a 6	" "front " "	MN 61 90 34 32 18 217 Straight
LS 61 7-0 3 4 31 14' 163	Straight	Verticals ""	NN 12 16-4 184 12 +8' 730" See detail Bors in ce
MS 61 TO 39 31 14 163		Verticals back	ON 12 12-5 14 12-14 449" = 10-6 = "
NS 9 146 19 9 16 384	" See detail	Bars in counterfort & "	PN 68 8'9 2'9 34 +8' 409" See detail Verticals in
05 6 10-6 14 6 12' 192	8-6		QN 59 11-9 2 4 69 +2 553
PI 68 8'9" 1" 34 18' 409	" See detail	Verticals in curtain wall & transverse in cap.	RN 8 50-0 3 4 20 -20 150" Straight welded Horizontals
QS 69 11-9 14 69 12 553	о р н	a a the second	SN 6 52-0 2 4 5 + 12 108 " " Longitudin
RS 8 500 29 20 20 150	" Stroight welded.	Horizontals "	TN 53 9'0 4 21 H 81 See detail Ligatures
55 6 520 79 6 12 100		Longitudinals in cap.	UN 6 6-0" # 3 12 54 Straight Spacer bars
TS 53 9-0 # 27 18' 81	" See detail	Ligatures	VN 44 7-6 8 22 16 132 - Horizontals.
US 6 60 34 2 18' 54	" Stroight	Spacer bars in footing to NSO bars	WN 38 17-0 34 38 18 713 " Verticals
VS 38 7-6" 3 4 19 16' 114	" "	Horizontais in wing walls (outside face)	XN 12 11-0 30 12 12 150 " Horizontals
WS 28 146 89 28 16' 467		Verticais	YN 12 15-0 \$\$ 12 +16 200 " "
XS 12 11-0 3 4 12 12' 150	И µ	Horizontals " " (inside face)	ZN 10 9'6" 5 4 5 20' 104 " See detail Vertical
VS 12 150 50 12 16 200	4	,	aN 10 40 54 2 20' 42" (traight "

Horizontals " pylon: (sides)

Verticals

Verticals

Bars

Longitudinols "

Horizontals -____

Ligotures "

Ligatures in columns.

Verticals in counterforts

Spacers to bars in counterforts

Verticals -

Transverse

4

top & bottom

haunch under pylons

Verticols in wing walls etc. See sectors BBacc

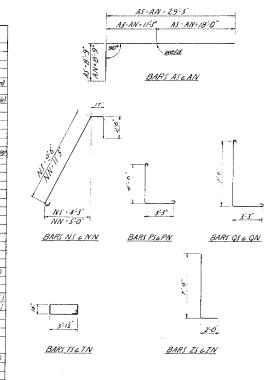
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Longitudinals in bottom of pylons (inside)



Remarks

To outside at tooting



5

14

4 · 9- 0

2:2" BARS IS & IN 2'-6" 2'-6"

0

- 1 BARS pS

Pres st. d

167921-2-38

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DEFARTHENT OF PUBLIC WORKS - TAS. DERWENT RIVER BRIDGE AT BRIDGE WATER STEEL LISTS FOR ABUTMENTS AND PIERS

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Mel 2/3/34.

MAR 43/31

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9 0-8" 144 1 6' 25. TOTAL WEIGHT IN SOUTHERN ABUTMENT 9060 LBS. = 4-04 TONS

See detai.

Straight

4.6 - - 77

Straight

See detail

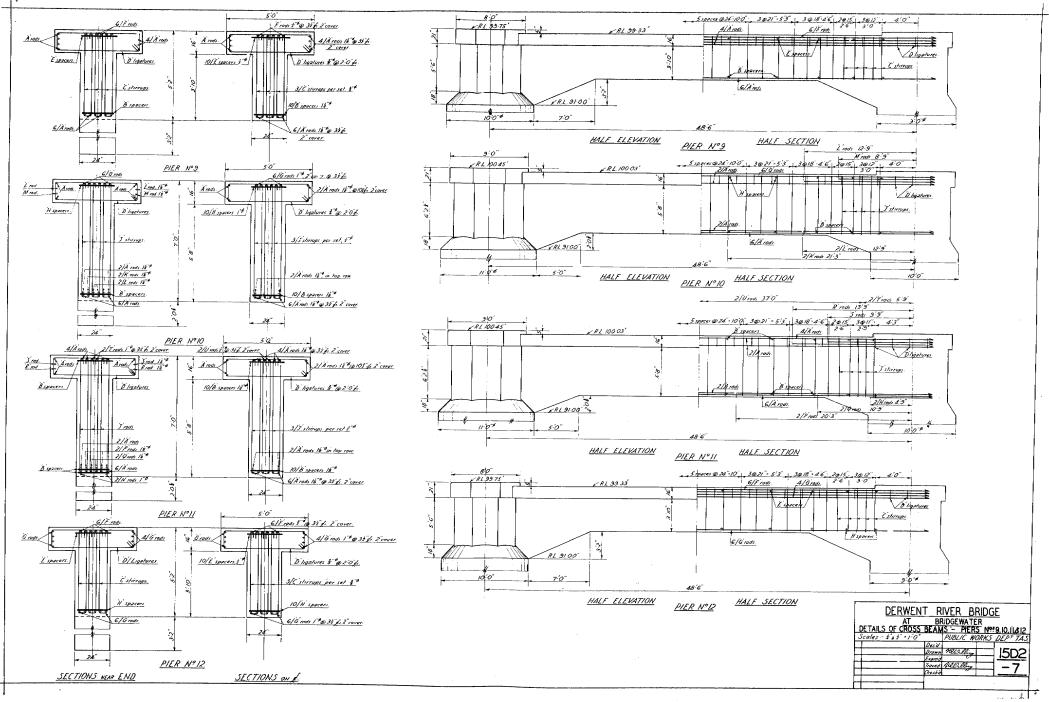
Straight

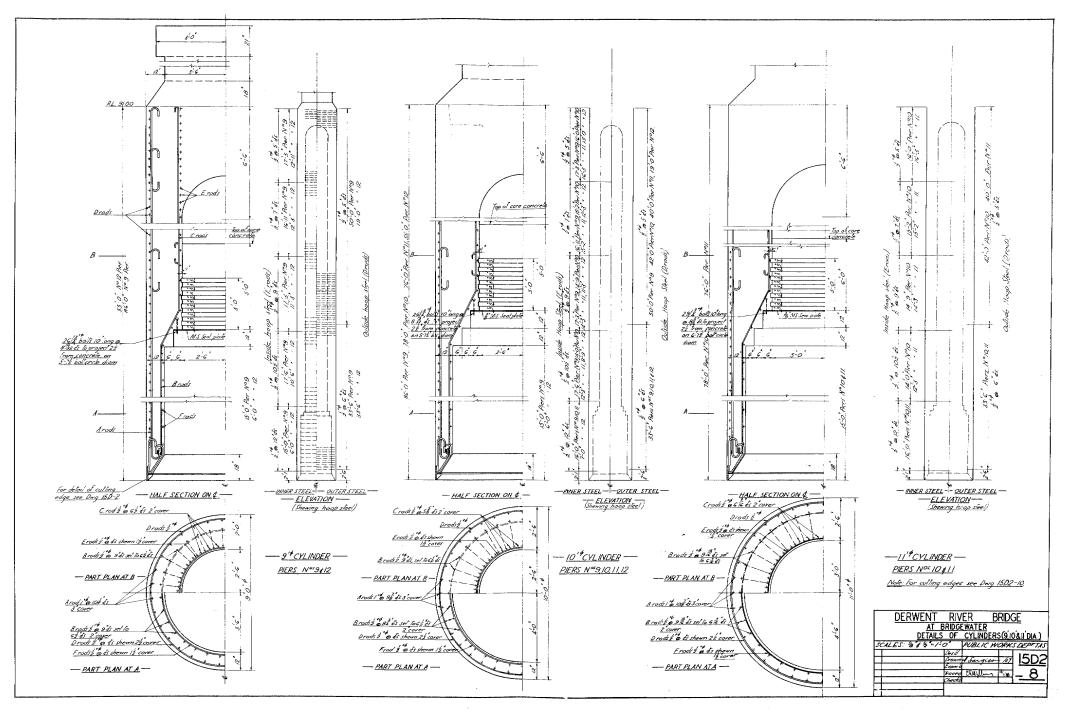
See detail

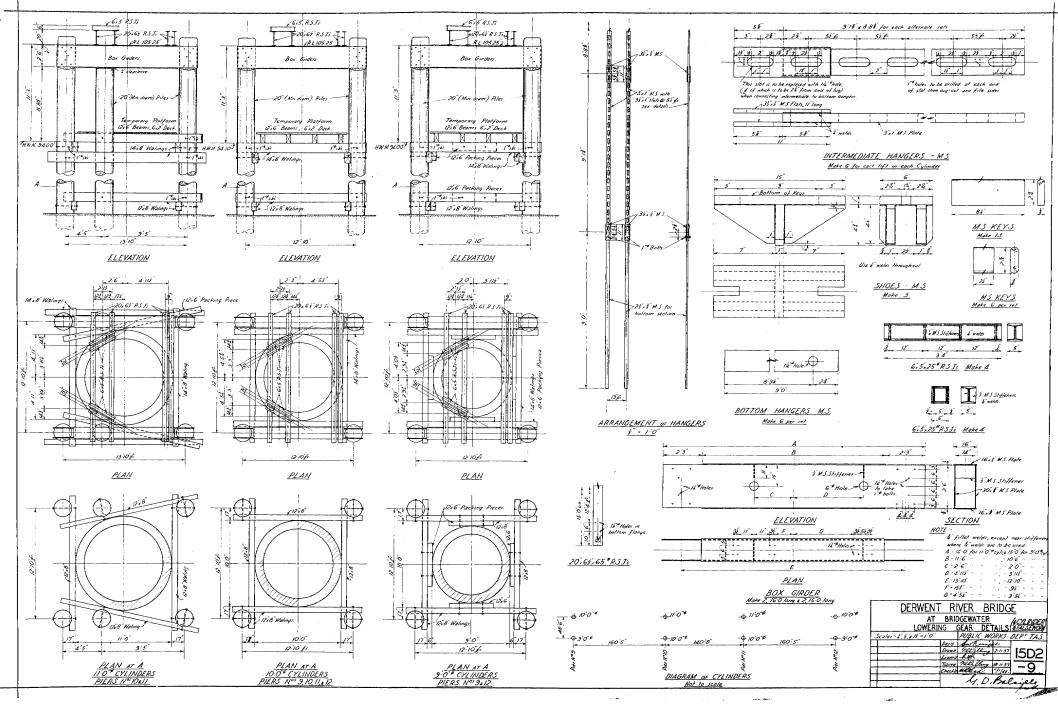
Straight

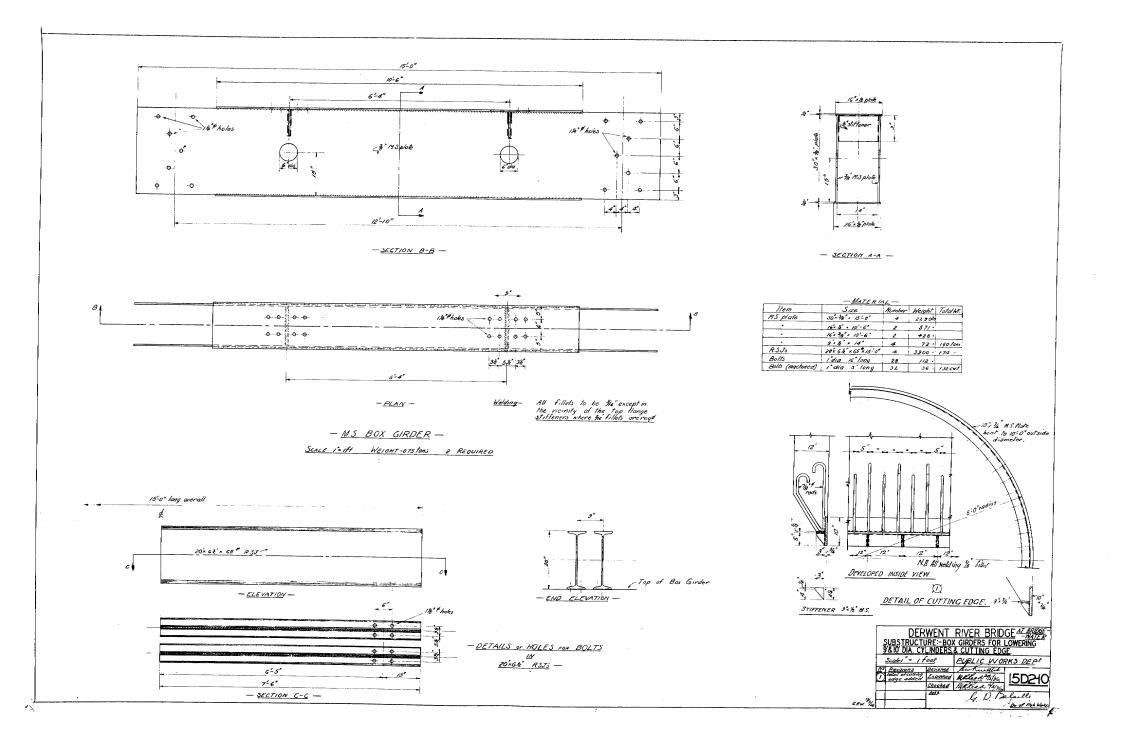
STEEL LIST FOR PIERS NOS. I TO 8 AND I3 DRG. I5D2-5

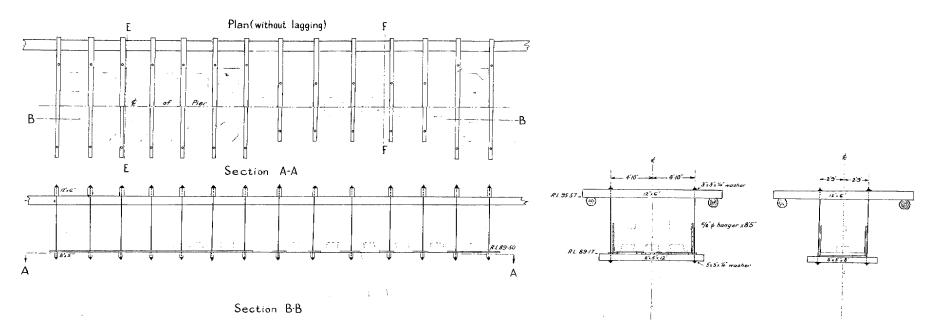
51222 2551	TON TIEND 1100, 110 0 AND 15 5110, 1502 5			
Mark North Length Size North Length Weight Shape	Remarks	Mark Nºoff Length Size Nºoff Length Weight	Shape Remarks	5-5-
AP 540 9-9 14 210 20 1441816s = 7-9" =	Transverse in footings All piers	18 8-6	Straight Verticals in columns Pier 1	
BP 54 48'9 \$ 4 135 20' 4005 " Strought welded	Longitudinals in footings(middle)	18 8'11	2	BARS KS & KN
CP 108 9-6" ## 54 16' 1296 " (# 4-6'88-0" =)	Transverse in factions a state	18 9-3		DAILS KJE-KIV
DP 360 5-10 2 4 120 18 3244 . E 4.4		18 9-3 18 9-17	" " 4	2-6" 2-6"
EP 90 70 20 45 14 946 Stroight	Diagonals "	LP 18 9-11 3 \$ 81 20' 3311 lbs	* * * * 5	1
FP 54 200 \$ \$ 54 20 1622 "	Longitudinals in footings(outside)	18 10-2	6	
122 8-9 14 122 18' 3298 -	Verticals in curtain walls Pier I	18 10-5	· · · · · · · · · · · · · · · · · · ·	4
19 ×1/22 J-2	· · · · · · · · · · · · · · · · · · ·	18 10-7		Ś
2 122 9'6 122 9'10 122 9'10 122 10'2' \$\$\$ 244 20' 7330 "	" • • • 3	18 10-7	/3	
2 22 9-10	• • • • • • 4	MP 273 10 30 30 137 18 927	See detail Ligatures in columns All piers	5
2 2 122 10-2 2 4 244 20 7330			Straight welded Longitudinals in cap "	
5 122 10'5		OP 207 3-9 2 9 52 16' 556"	Straight Transverse in cop ""	/3
8 25 122 10-8		TOTAL WEIGHT IN ALL PIERS= 64455 LBS		
\$ \$ 122 10-10 \$ \$ 366 12' 6595		Contraction in ALL 1210 CT. TO LEA	000,000	BARS pN
	A	12 22		
HP 182 42-0 34 273 30' 3090 " Straight welded	Horizontals in curtain walls All piers			
30 12-4 See detail	Main bars in columns Pier I	Pier N	1º Dimension A	
30 12.9	- 2		8'-6"	7
$30 \ 13^{-1'}$ $30 \ 13^{-5}$ $1' = 180 \ 14' \ 6728 = 100$	" * * • • 3		8'-11"	3 8
30 13-5 10 100 14 0120	• • • • • 4		9'-3" 2'-3" + 2'-3" +	-
KP 30 13-9	• • • • • 5		9'-7	
30 14-0	• • • • 6	8 5	9'-11" BARS MP	A
30 14-3		6	10-2"	
30 14-5 1 \$ 90 16' 3845 "		BARSKP 7	10'-5"	
30 14-5	/3		10'-7"	
		24"	10'-7"	
		H		





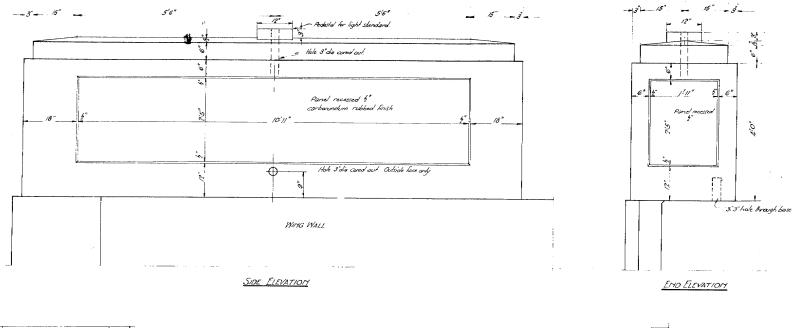




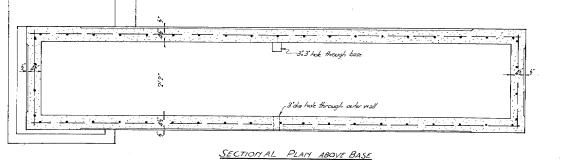


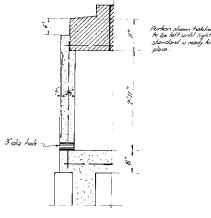
Section E-E

Section F-F

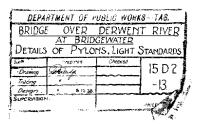


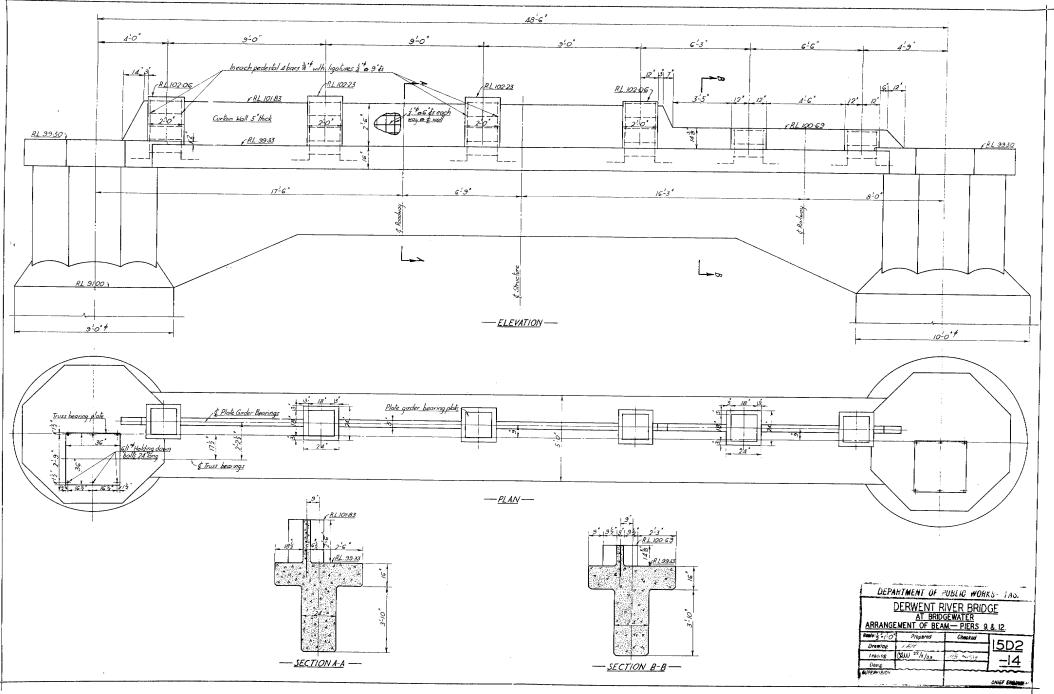
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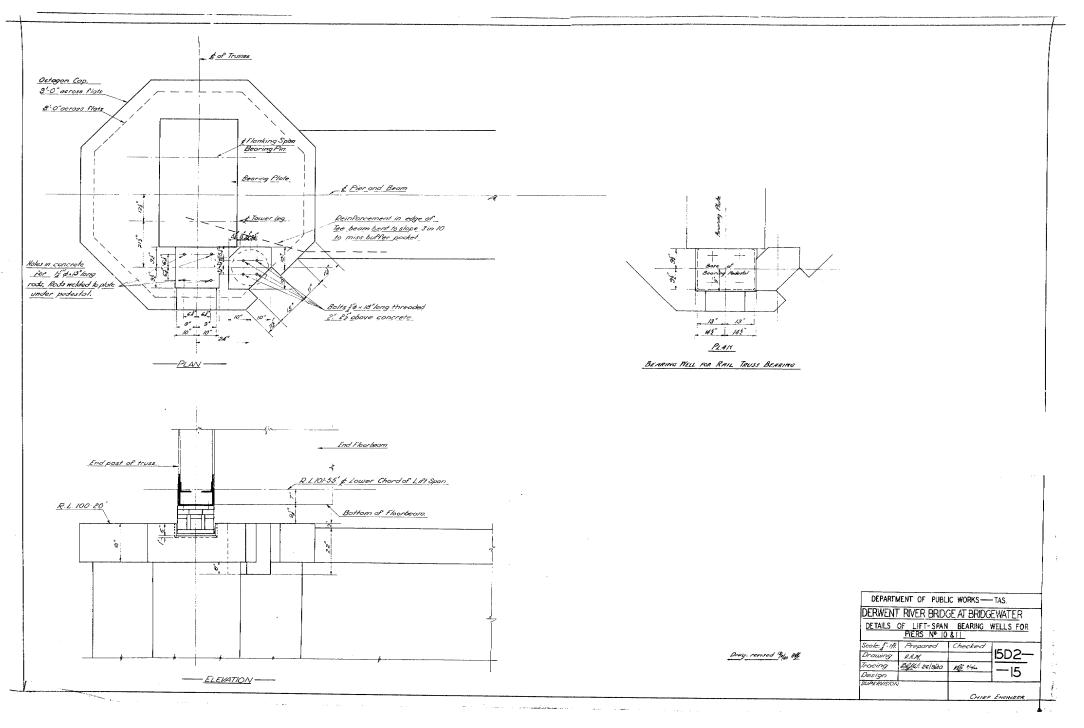


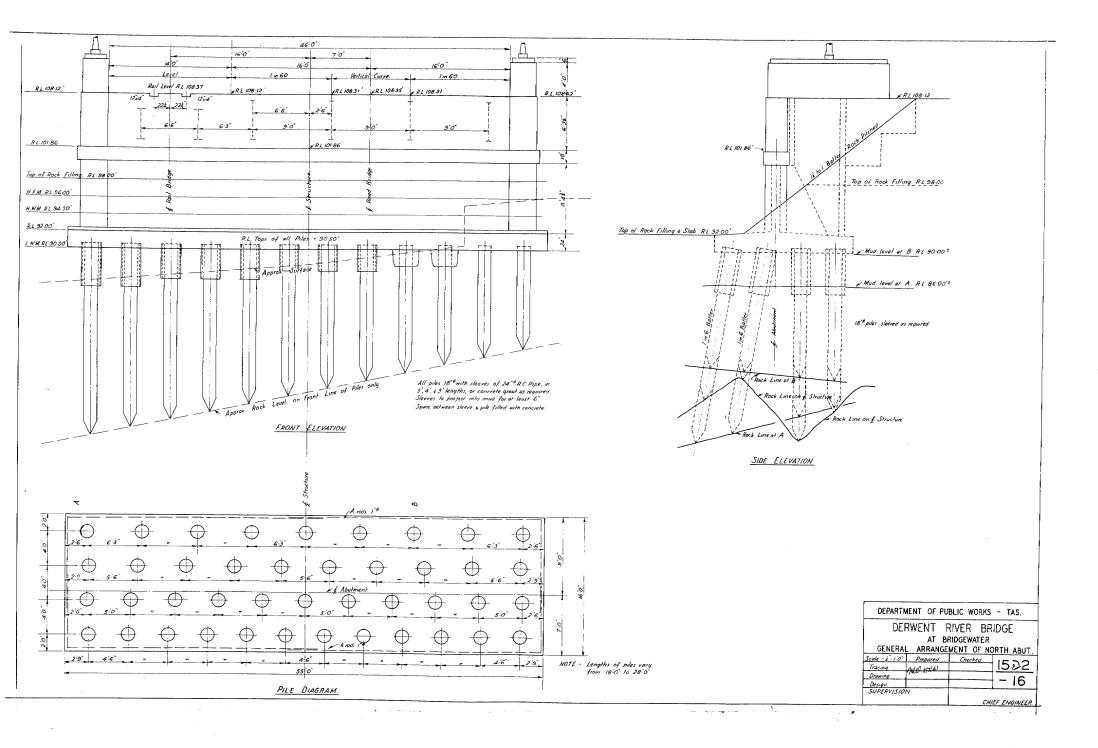


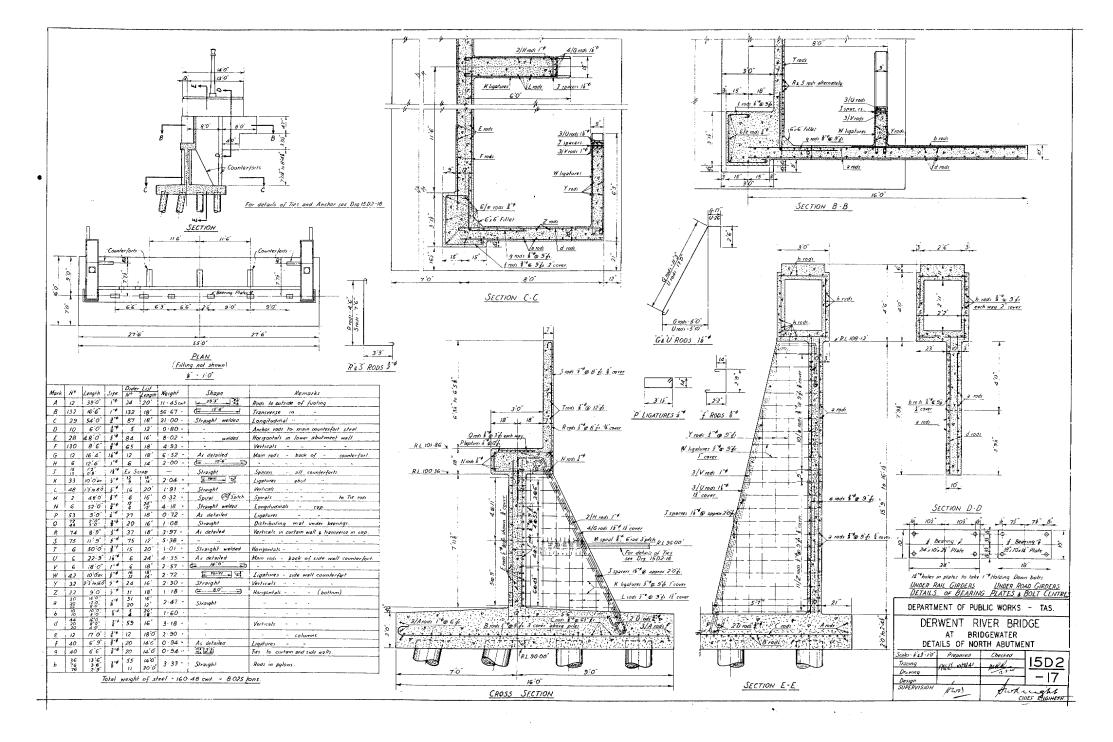
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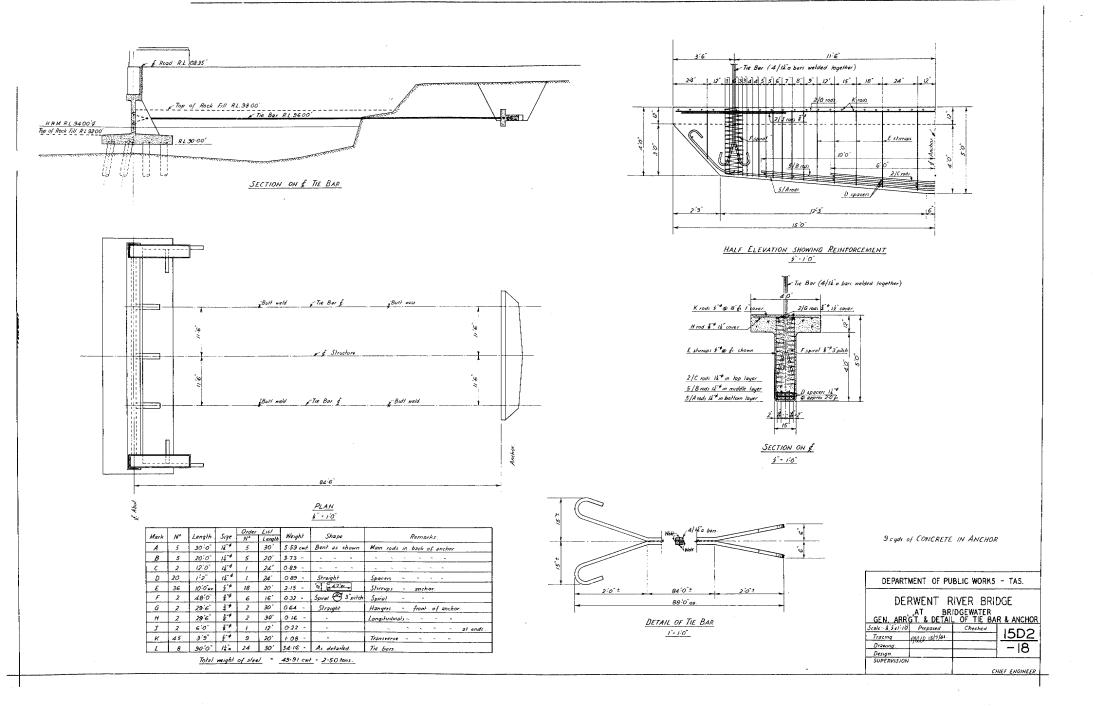


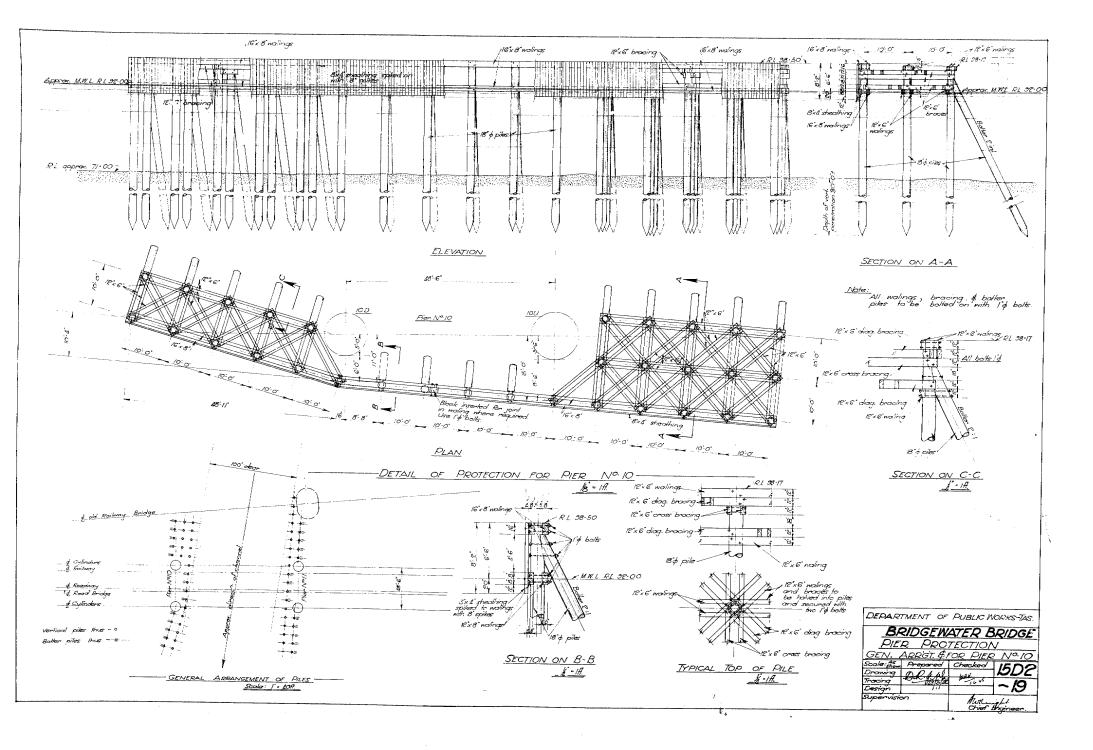


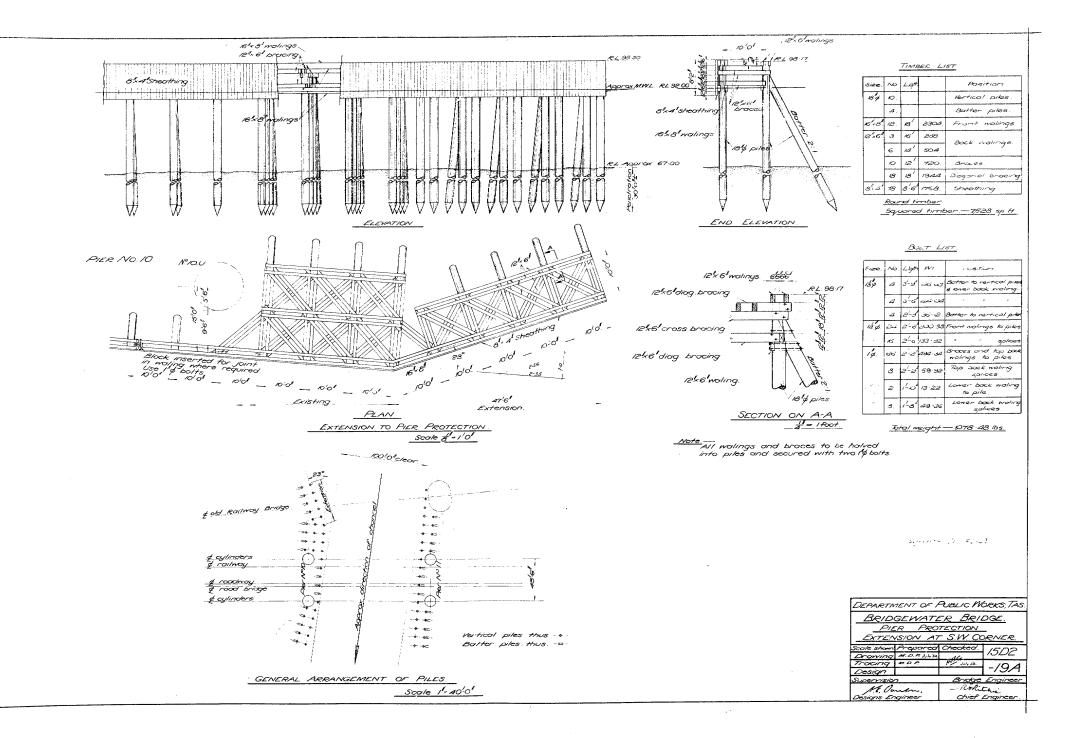


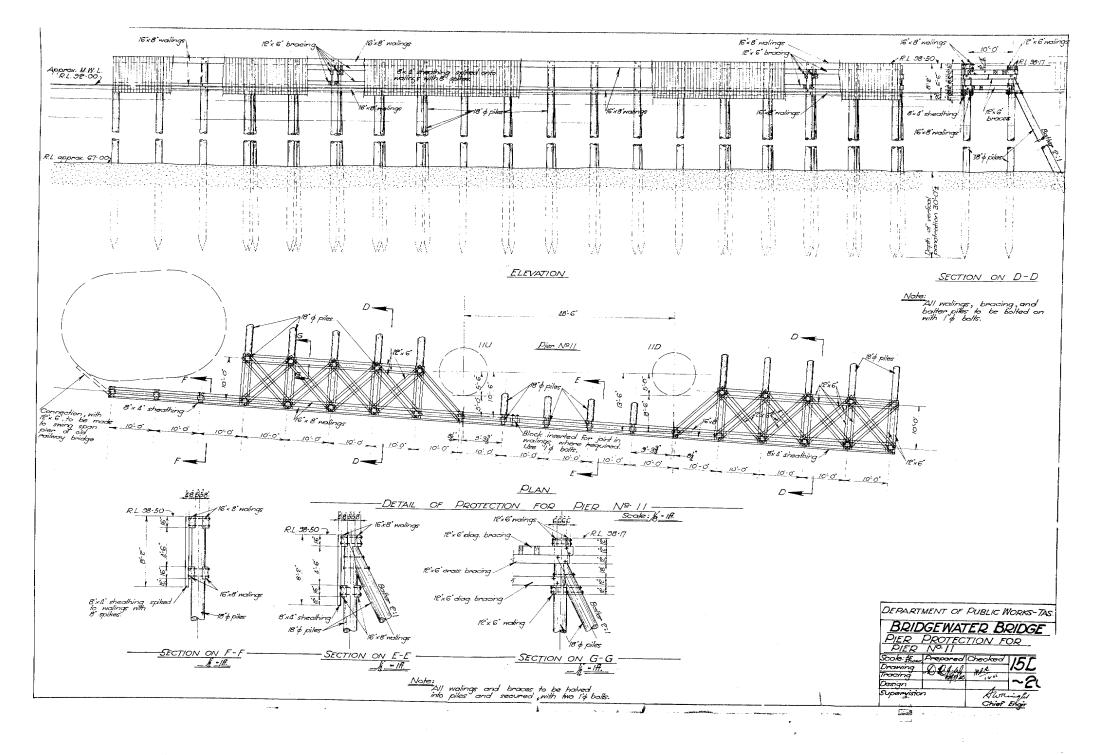


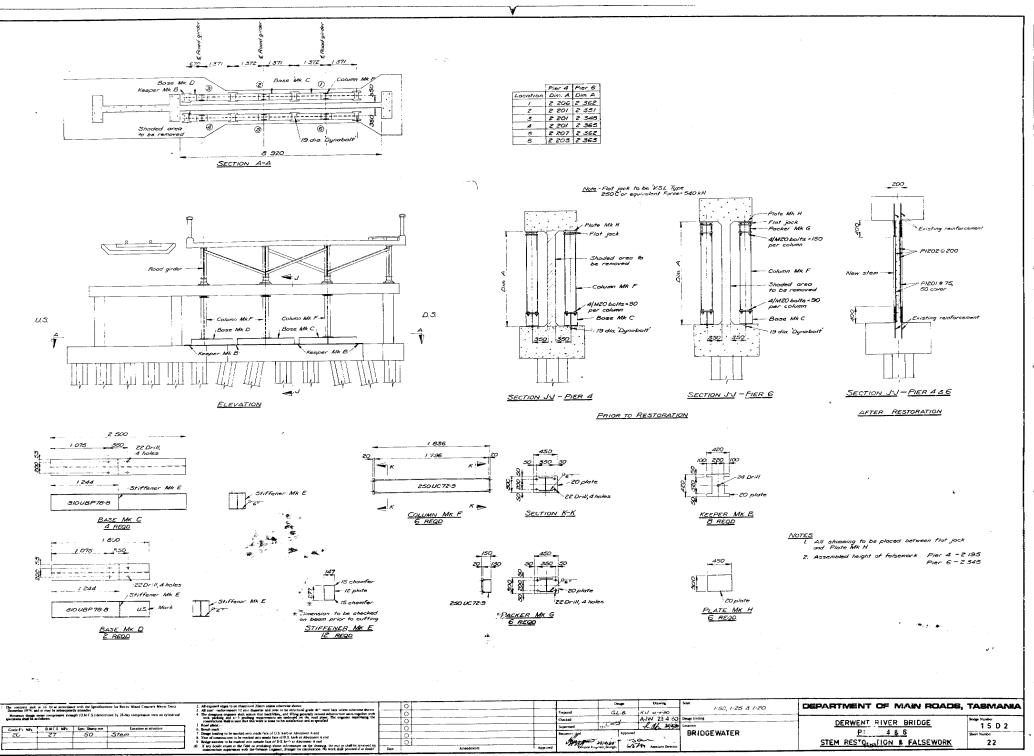


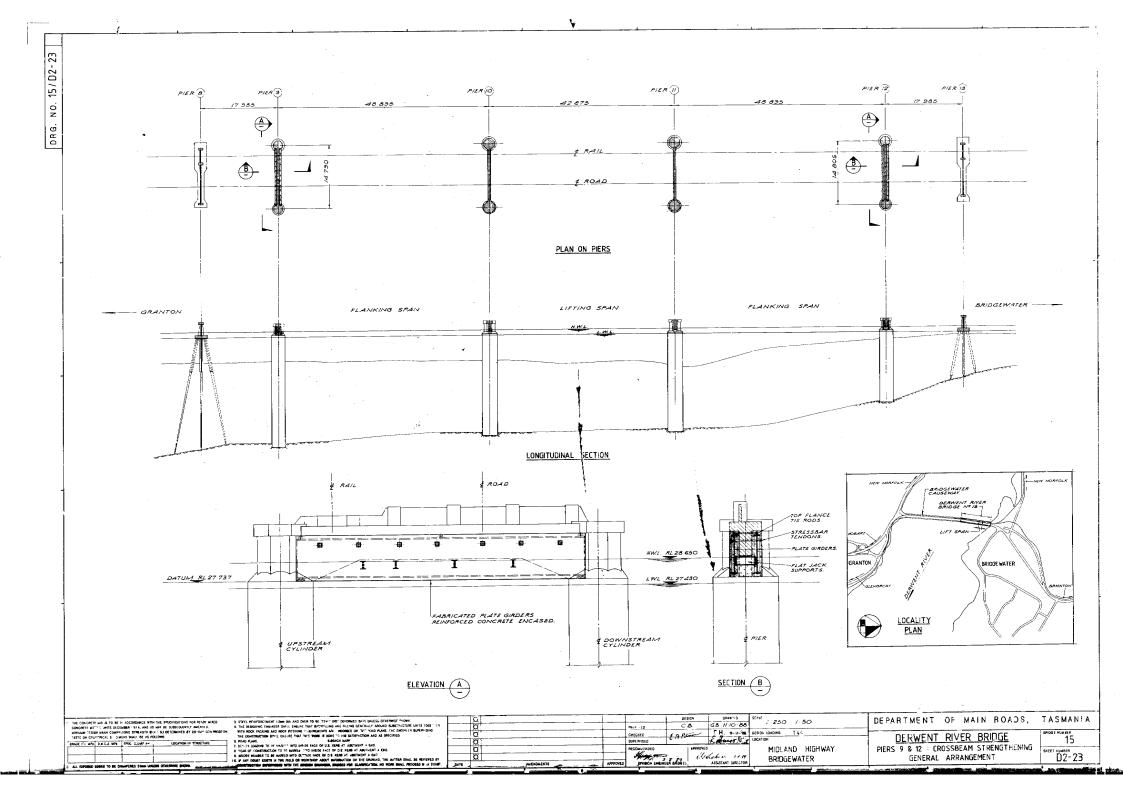


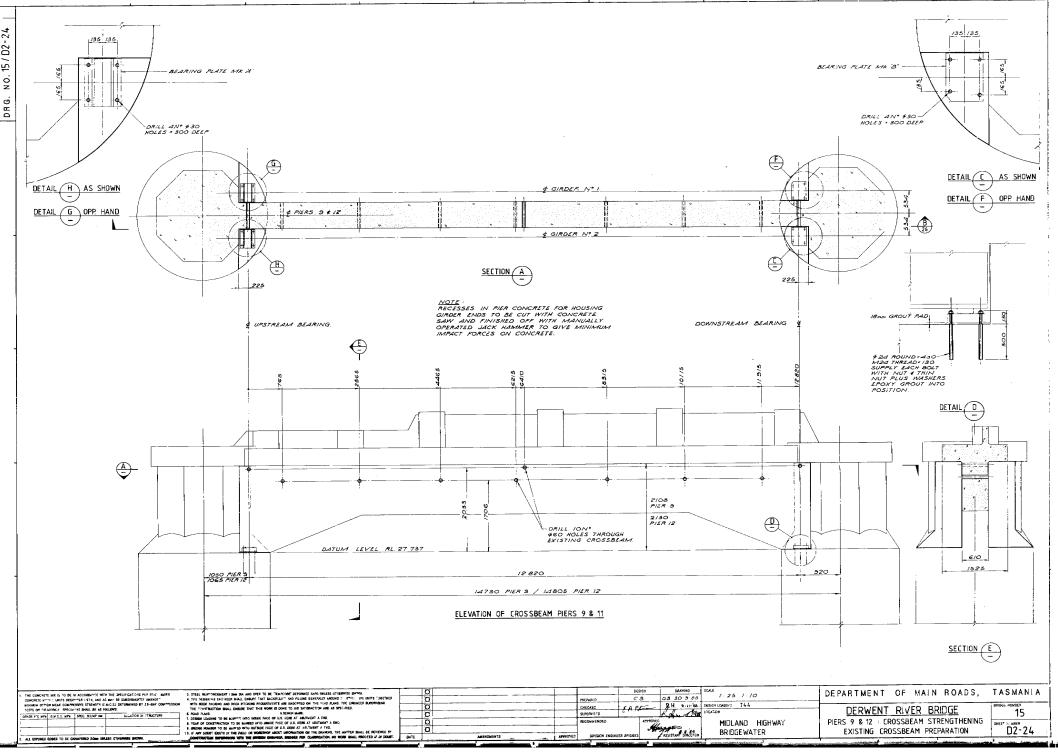




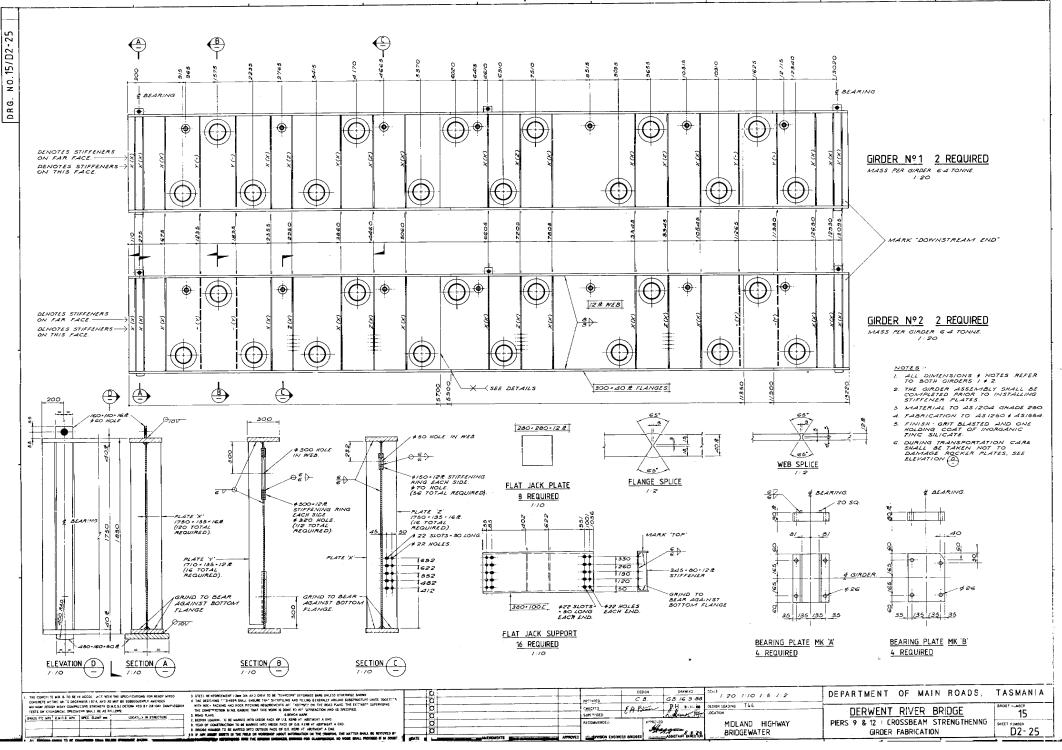








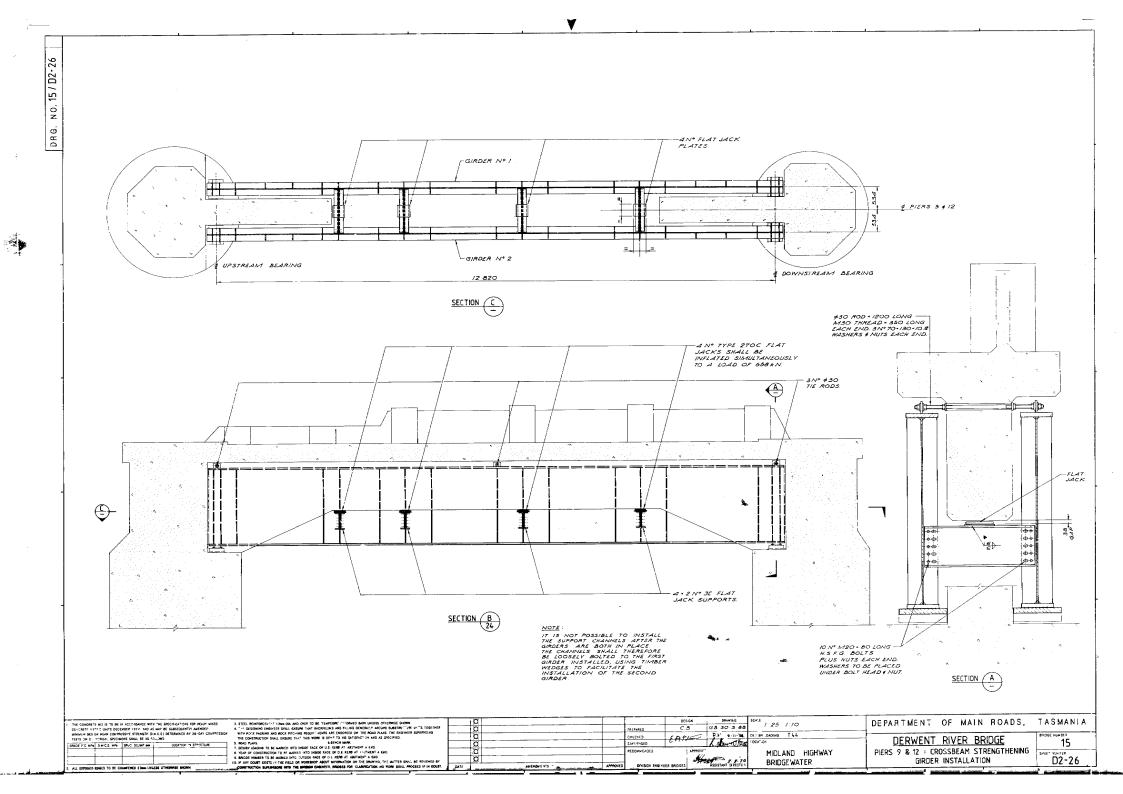
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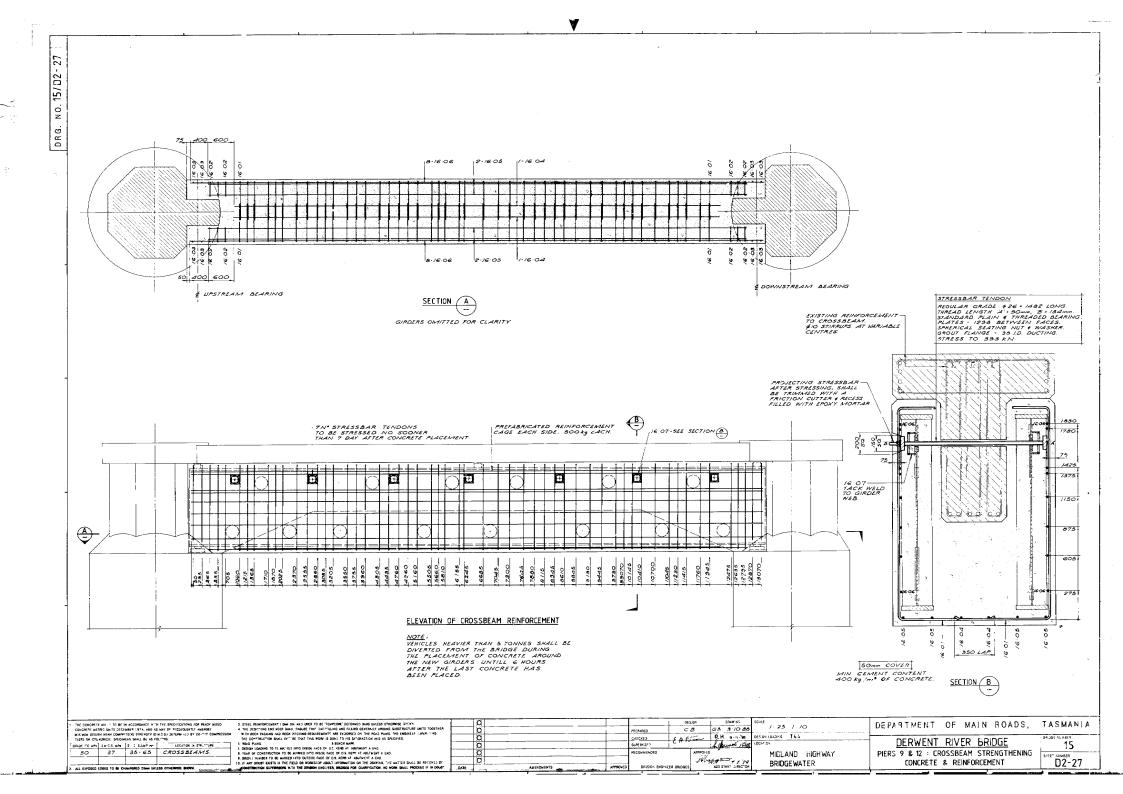


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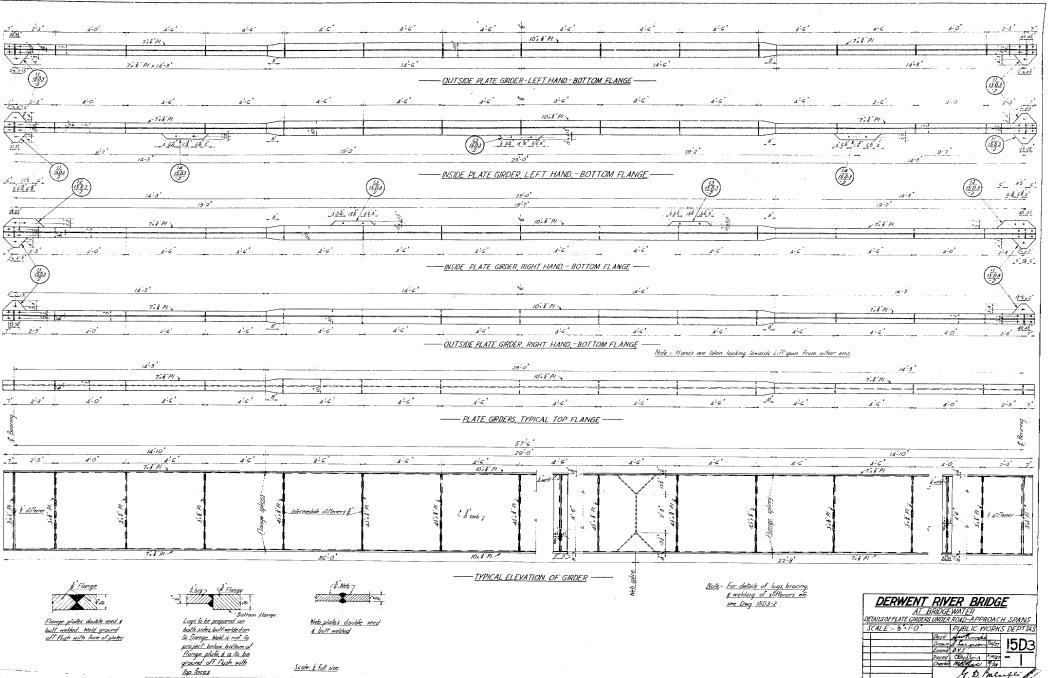


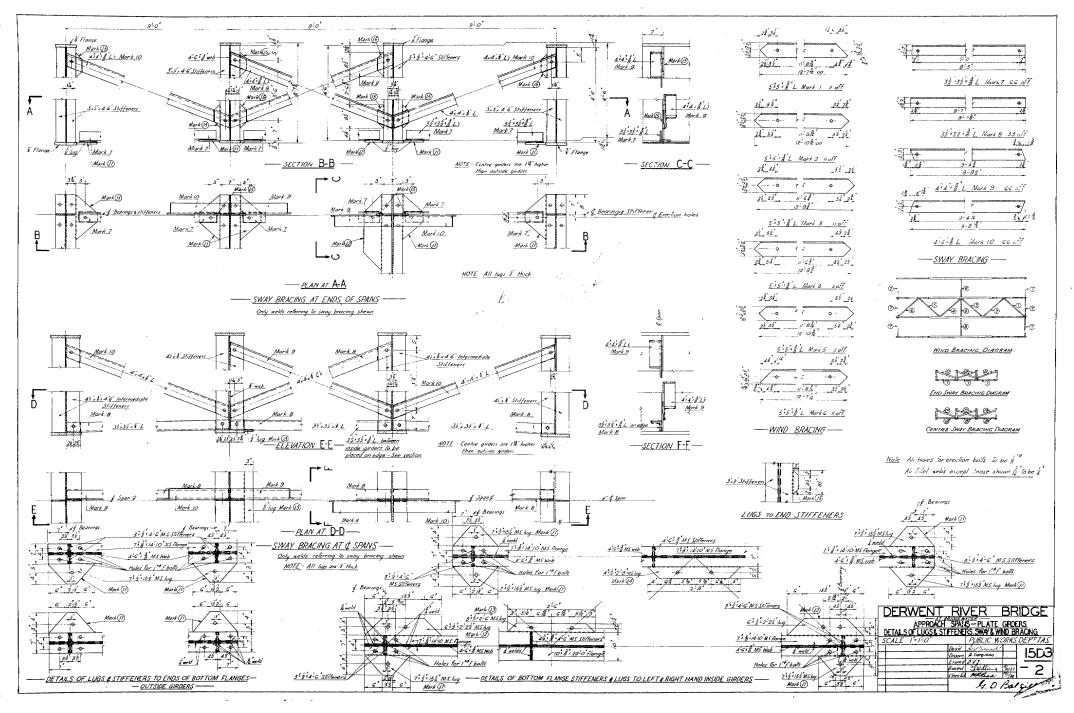
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14	D3-11	LIGHT STANDARD		
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19	D3-16	APPROACH SPAN UNLOADING	FRAME J	

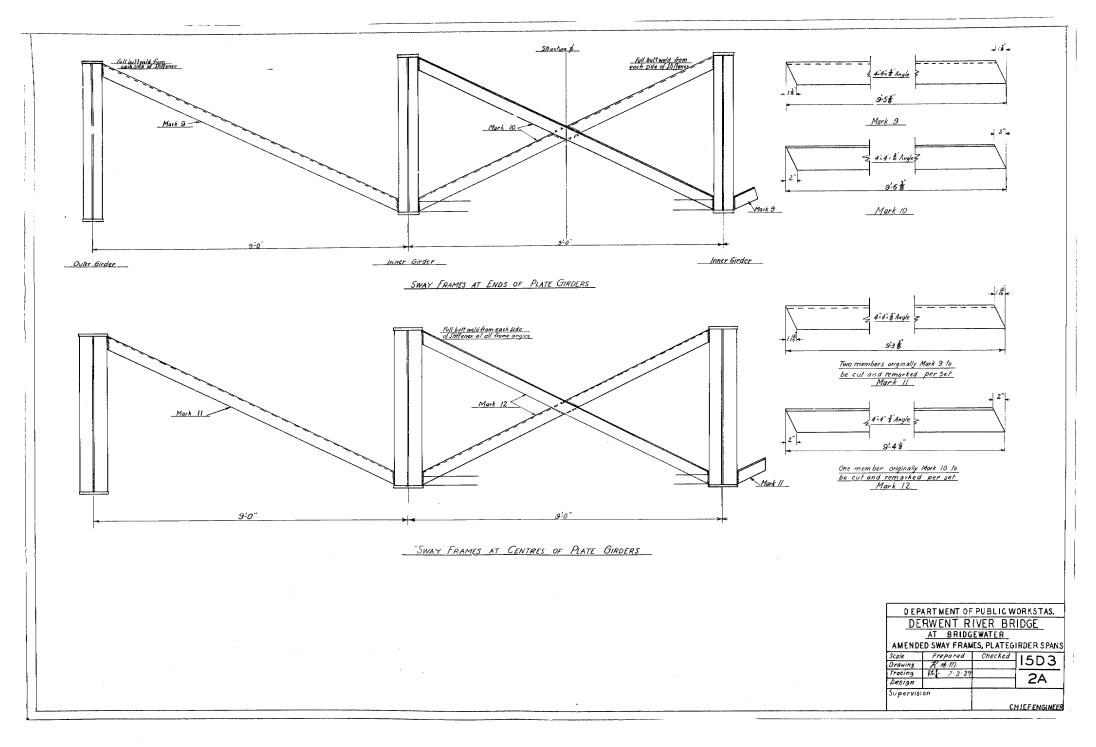
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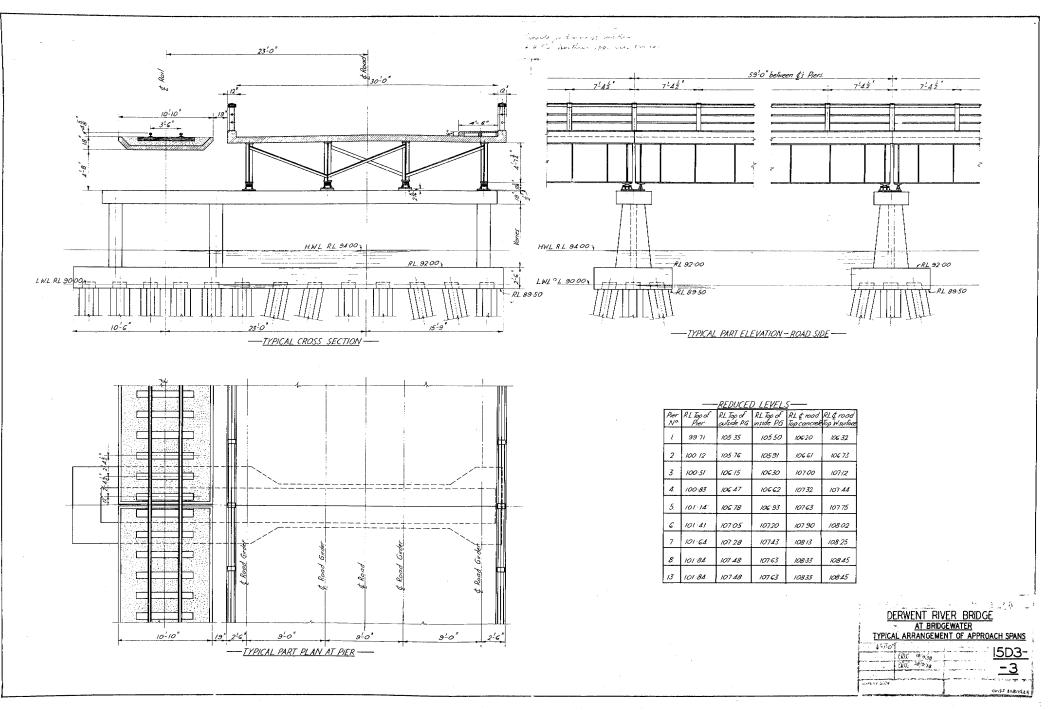
D3 - APPROACH SPANS SUPERSTRUCTURE

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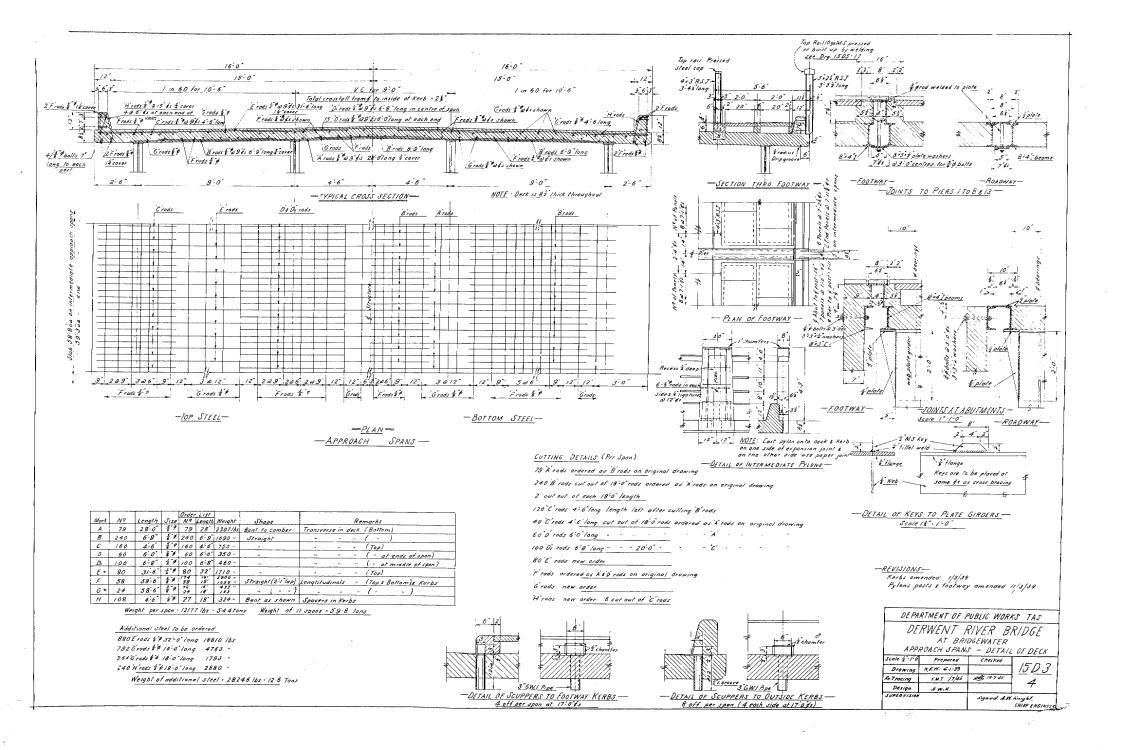


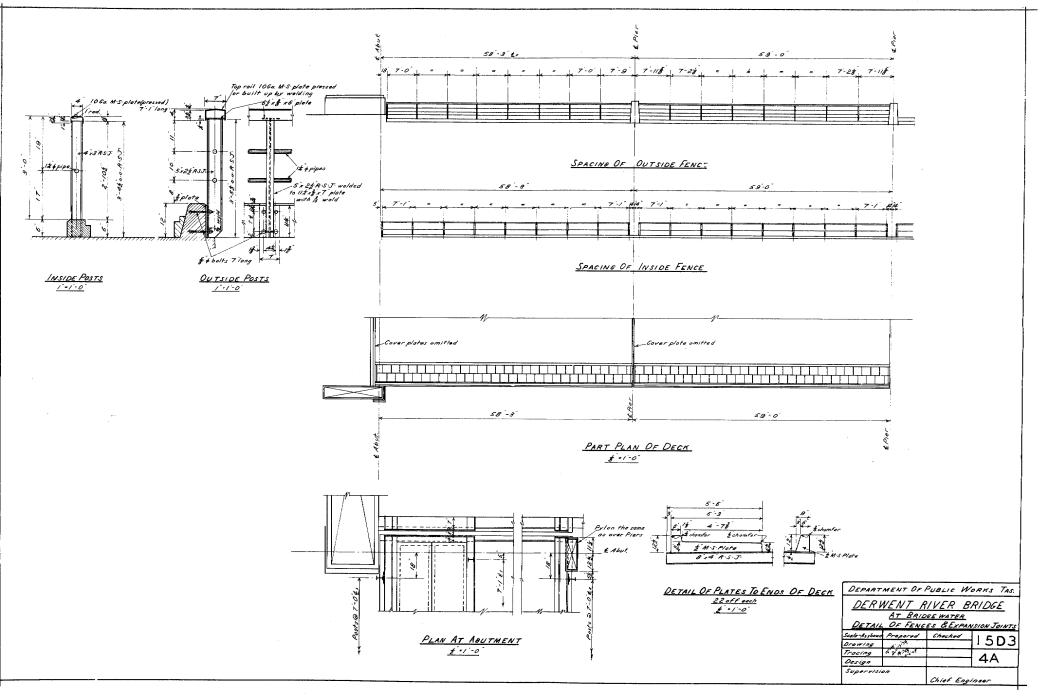


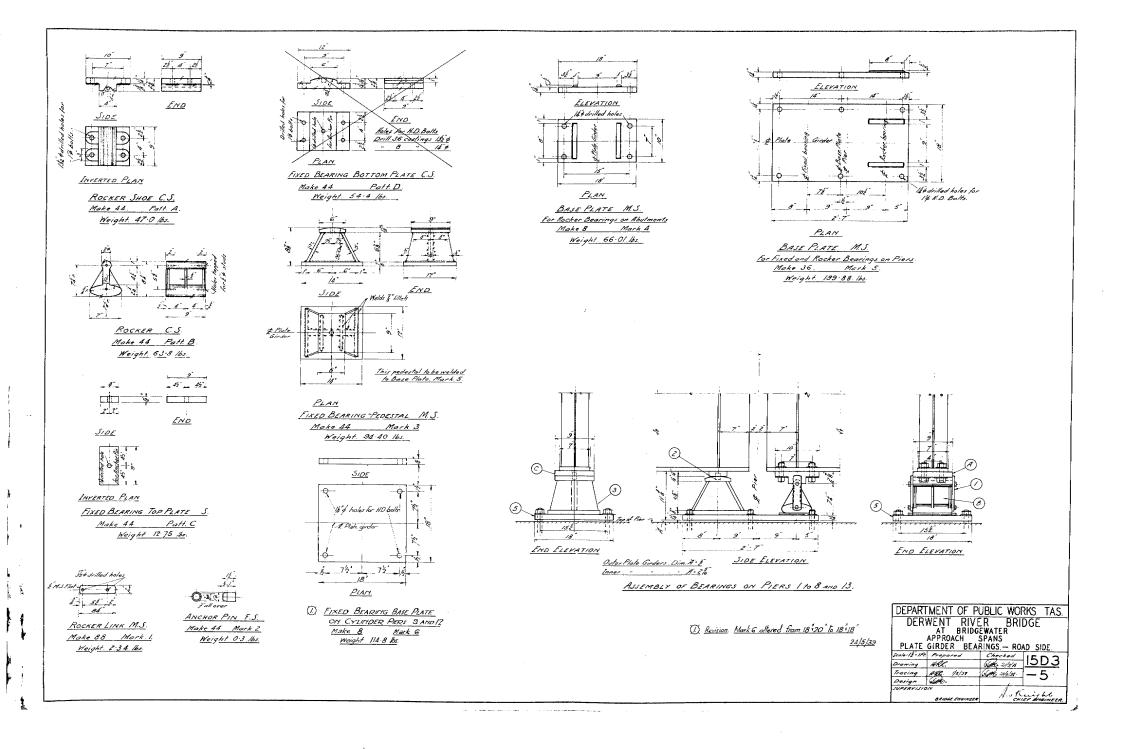




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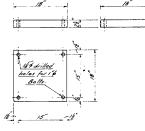


J. . . 35 EMS Plate to tholes for 20 stords

<u>ROCKER GUIDE M.S.</u> <u>Make 44 Mark 6</u> <u>Neight 141 ^{Nes}</u>

f all over A Sec 140 ANCHOR PIN F.S.

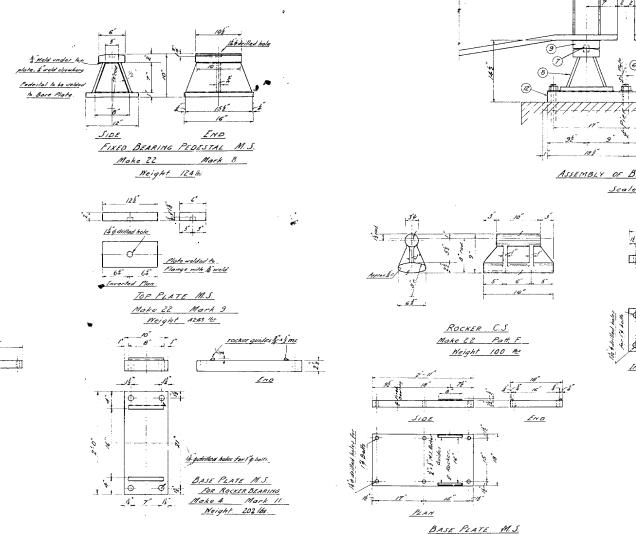
Korfixed Bearing Moke22 Mork 7 Weight 0.5 15



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BASE PLATE M.S. FOR FIXED BEARING Make 4 Mark 10. <u>Weight 230 Mar</u>

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Bearing Wells L'deep 162 1 ASSEMBLY OF BEARINGS ON PIERS Scale 12" - IFt. 7" 12 Holes drilled & tap for \$ \$ Studs END SIDE 12 INVERTED PLAN ROCKER SHOE C.S. Make 22 Patt. E. Weight 92.12 161. Reference:

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1 & Bolts

N.D. Balts is

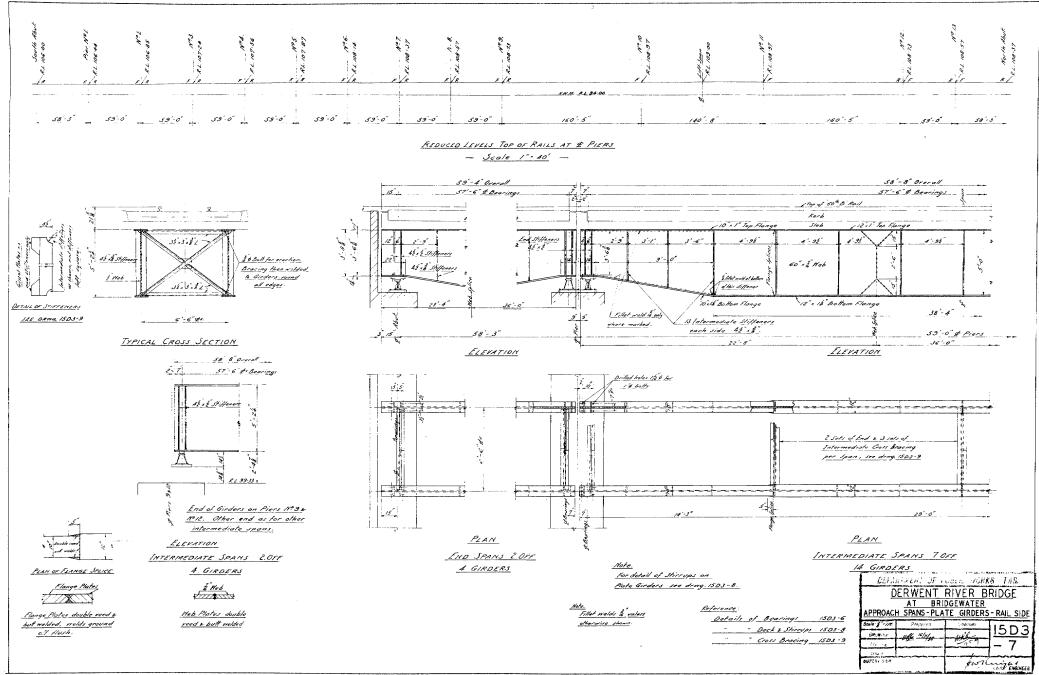
studs

~	~	Deck & Stirrups	1503-2
		Cross Bracing	1503-5

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DERWENT RIVER BRIDGE						
	APPROACH SPANS - BEARINGS - RAIL SIDE					
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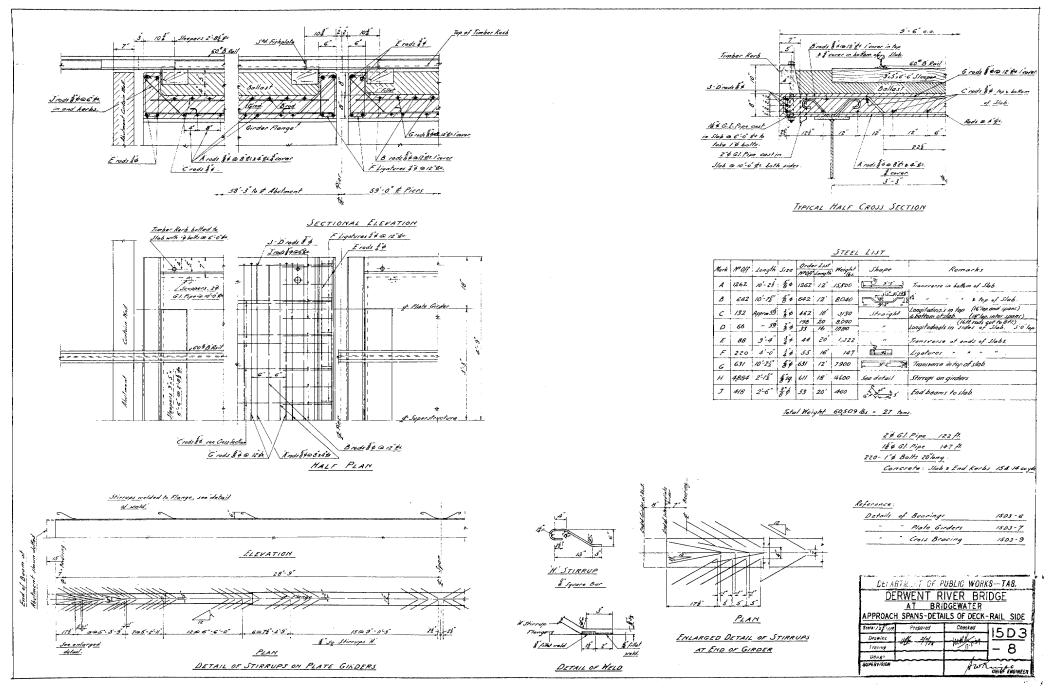
Make 18 Mork 12 Weight 448 lbs

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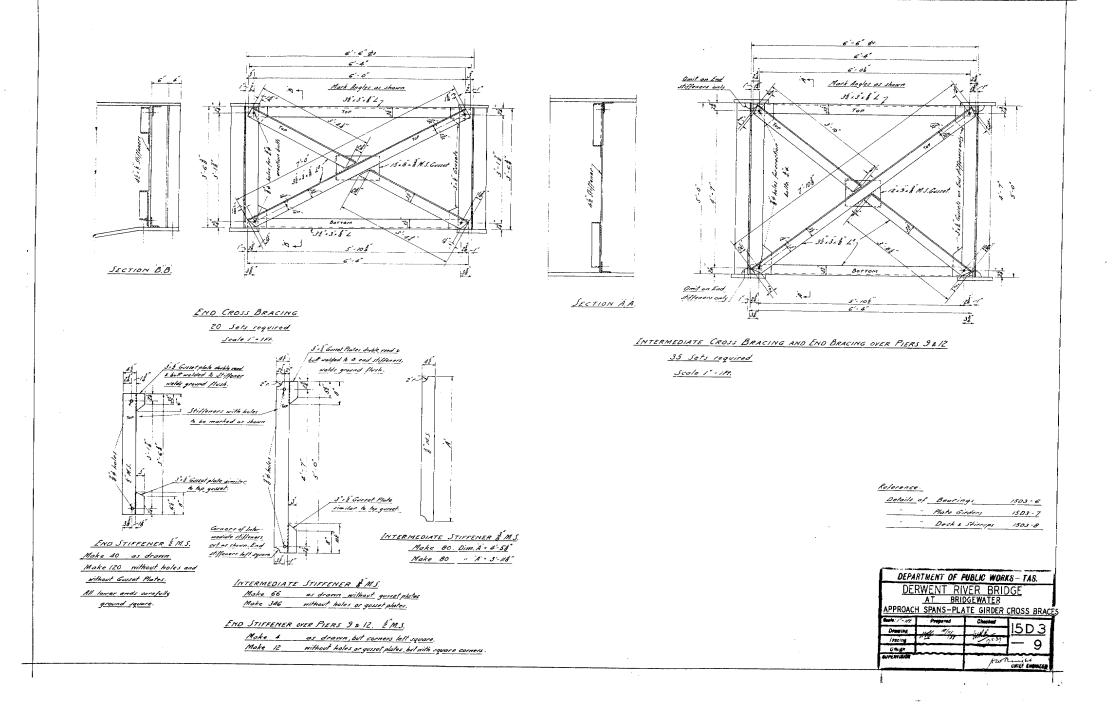


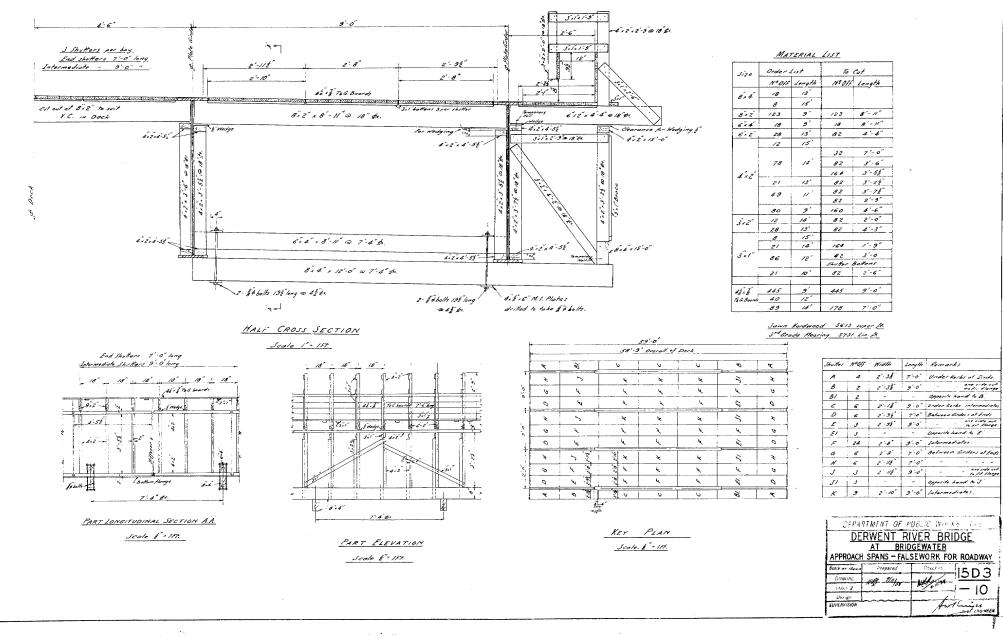
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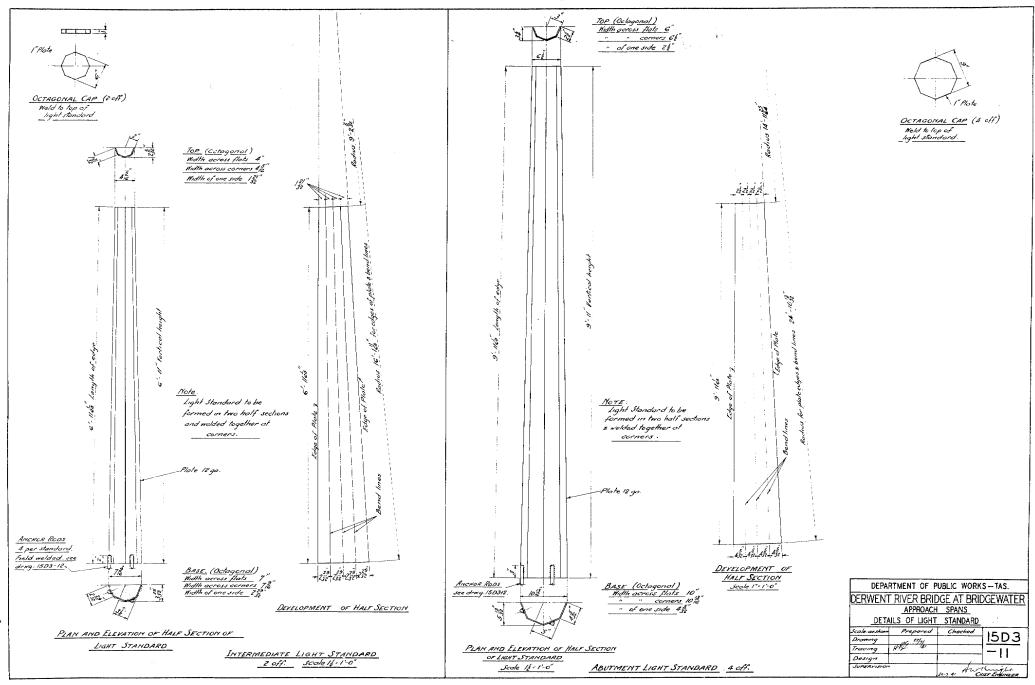
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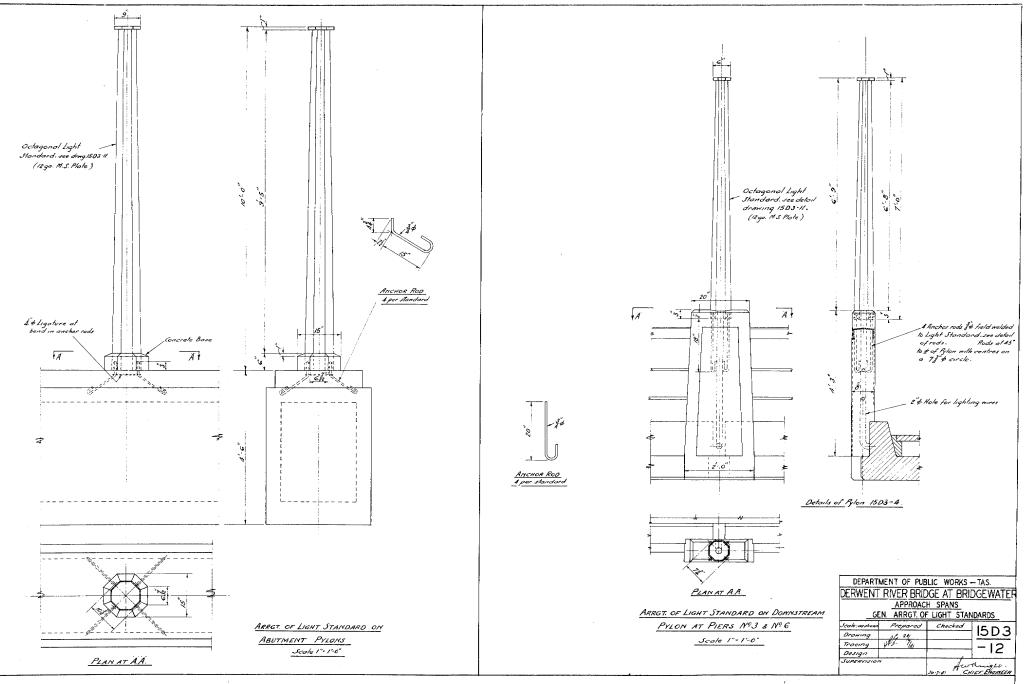


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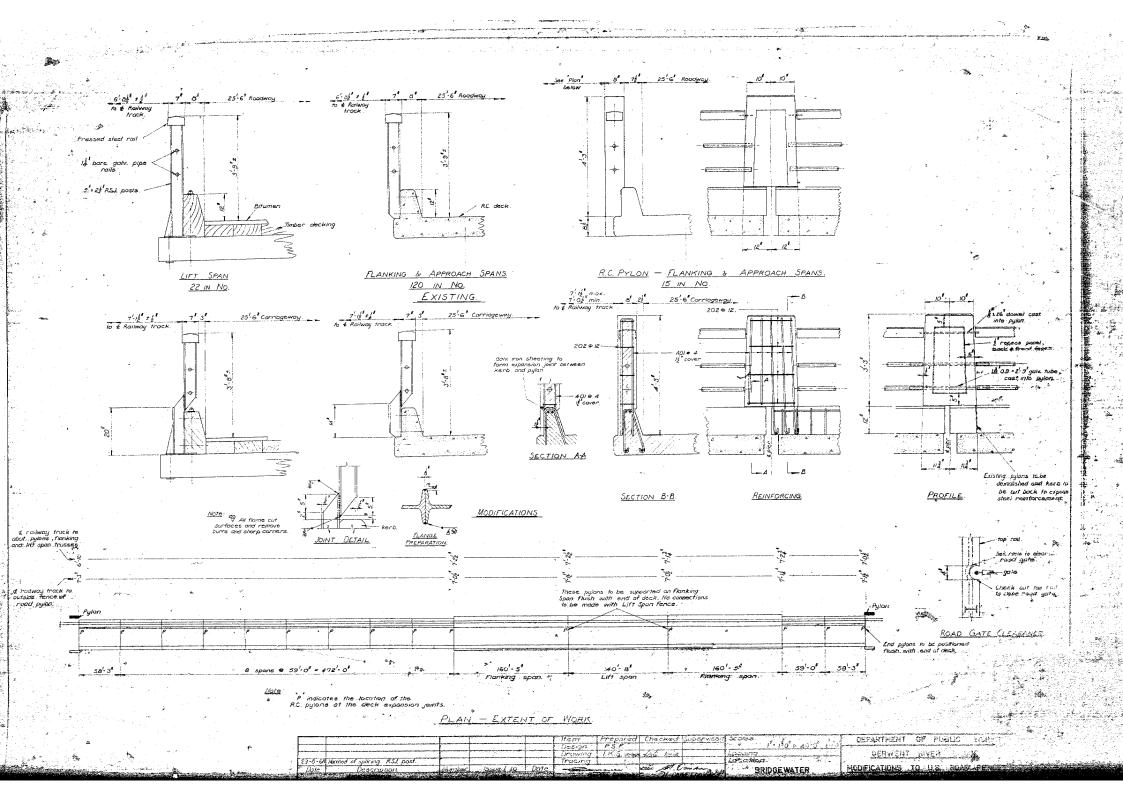


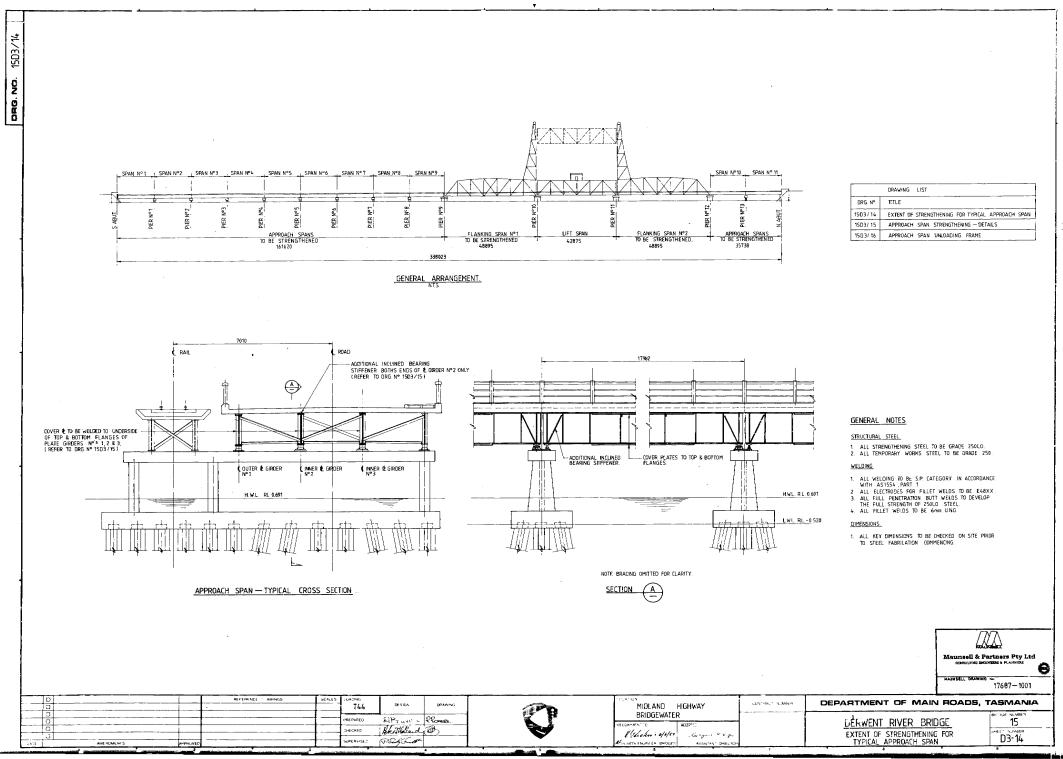




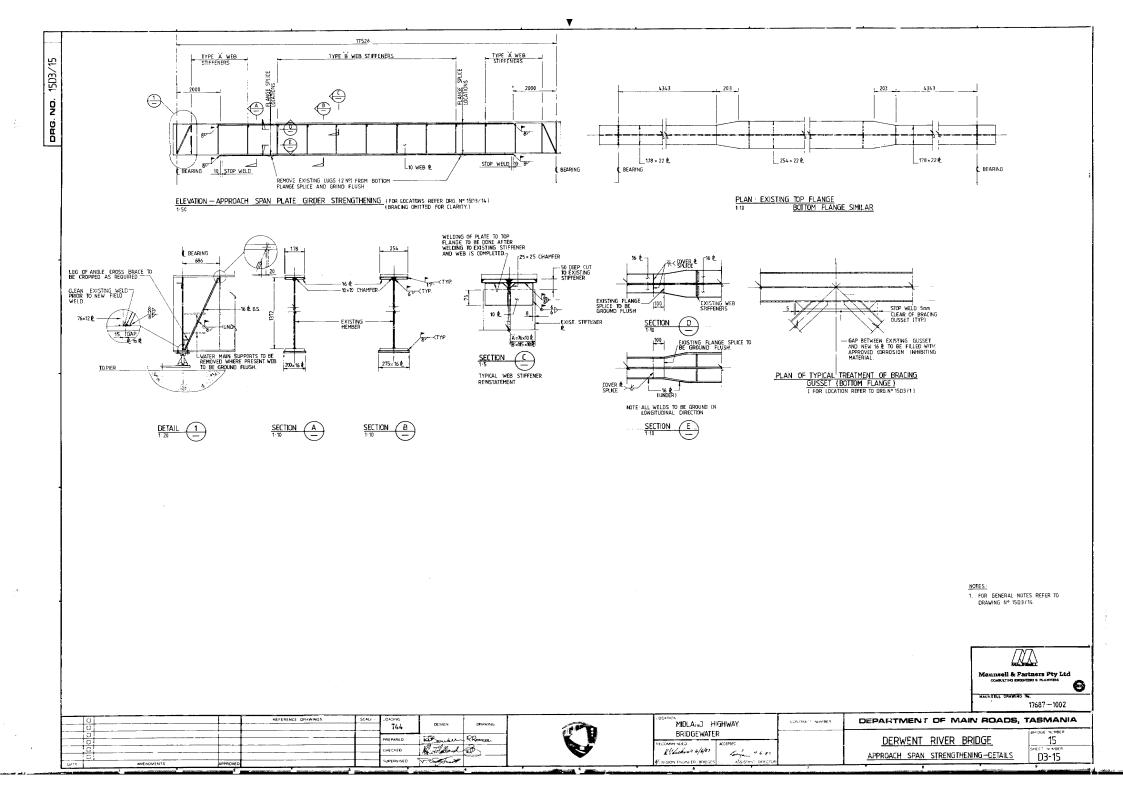


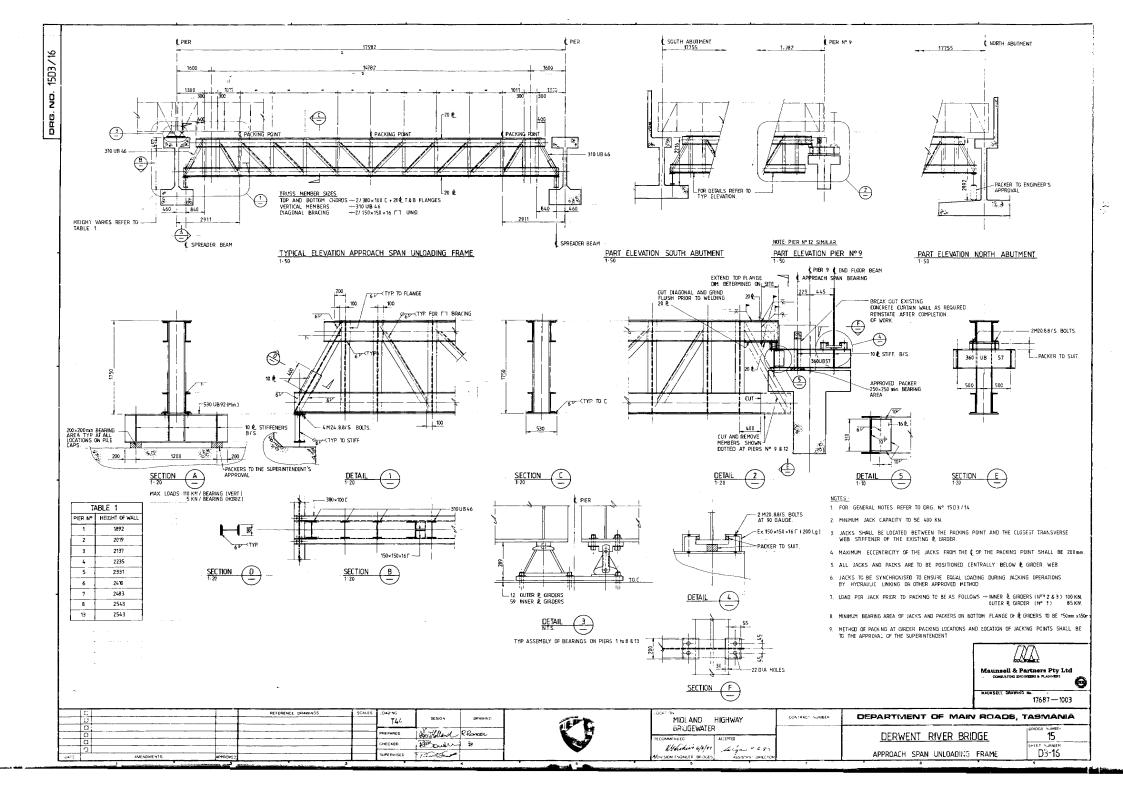
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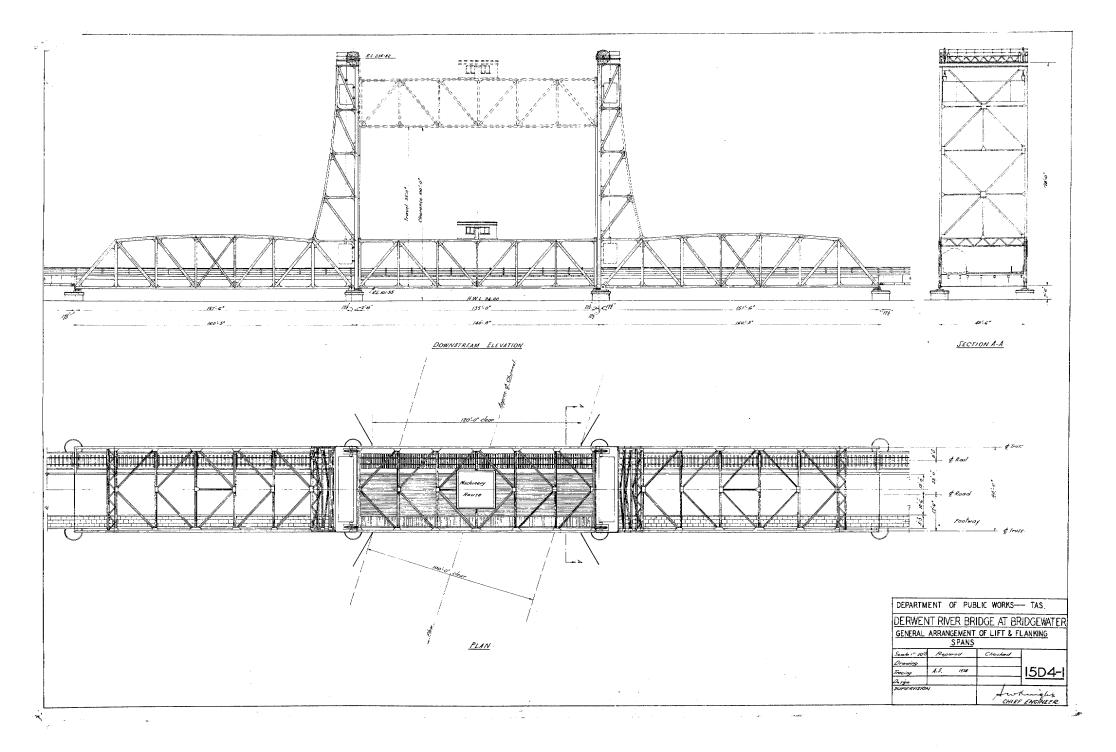
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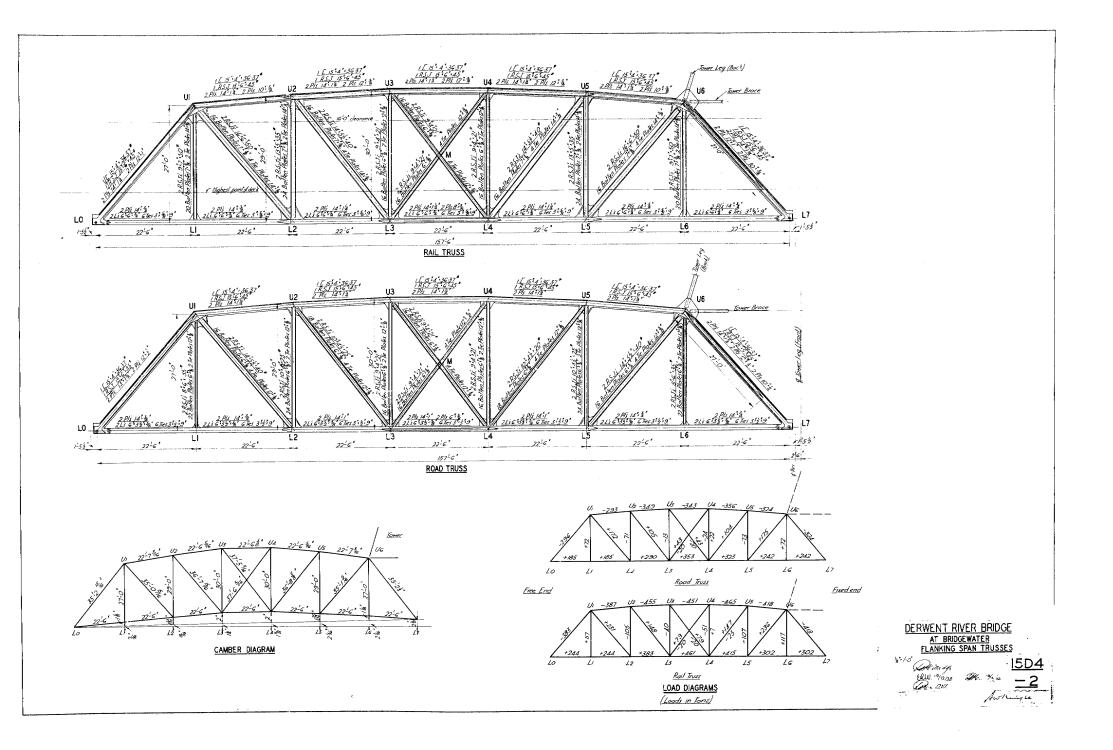


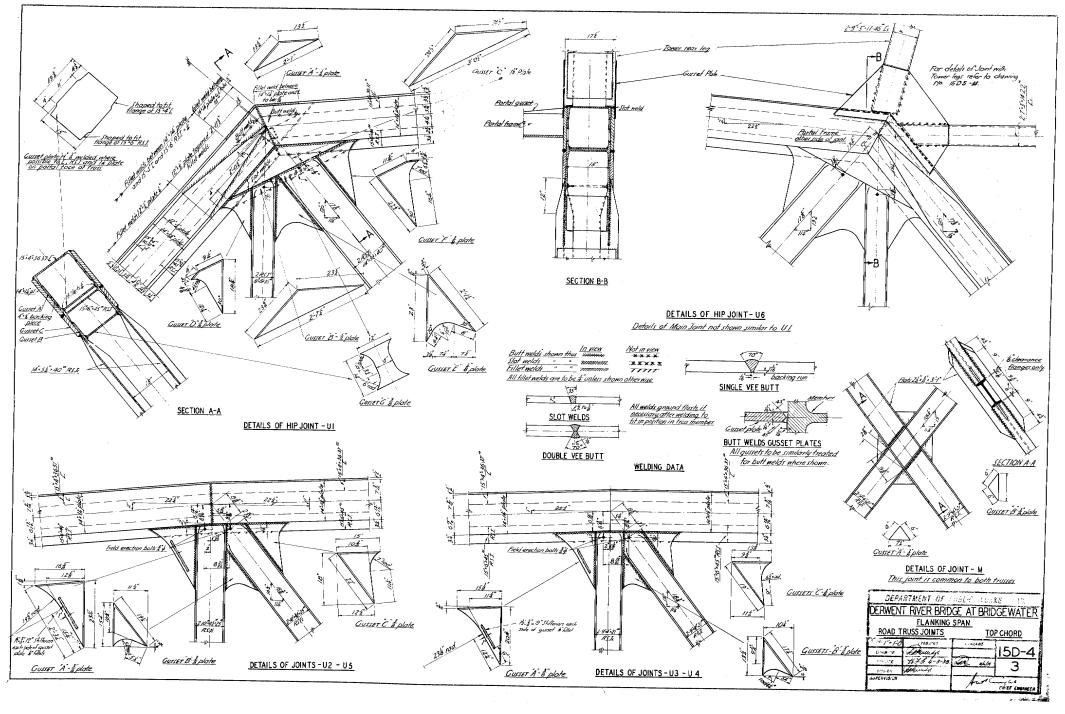


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3	D4-02	FLANKING SPAN TRUSSES	
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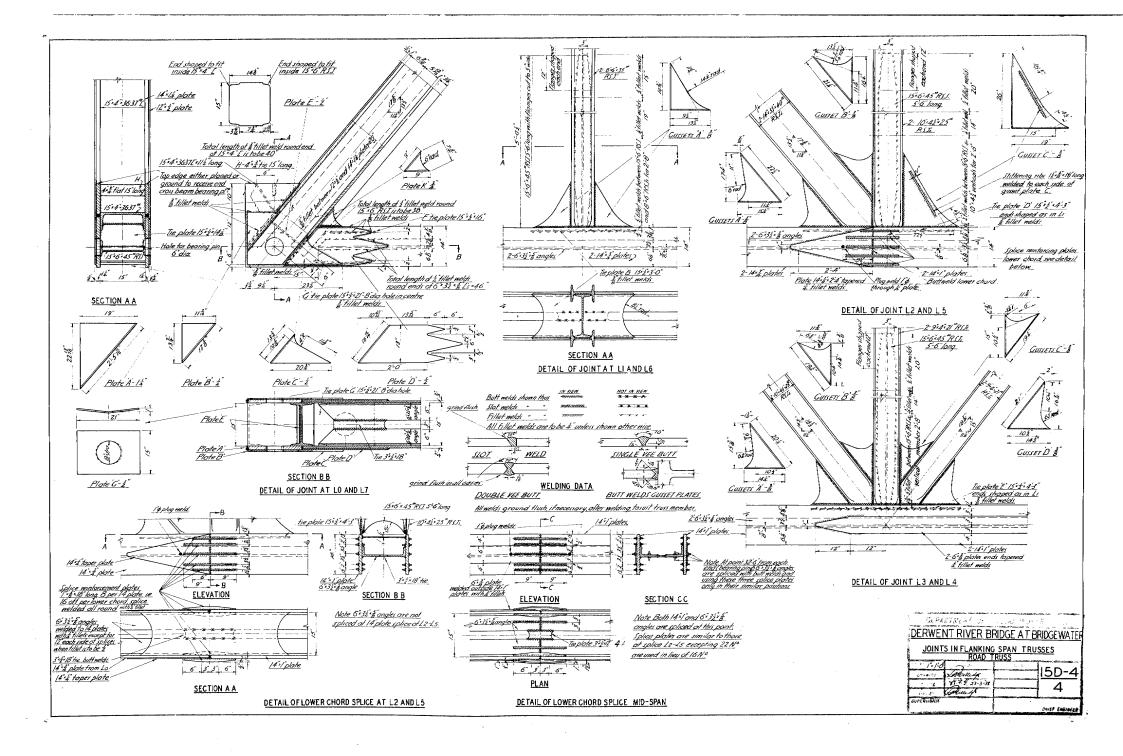
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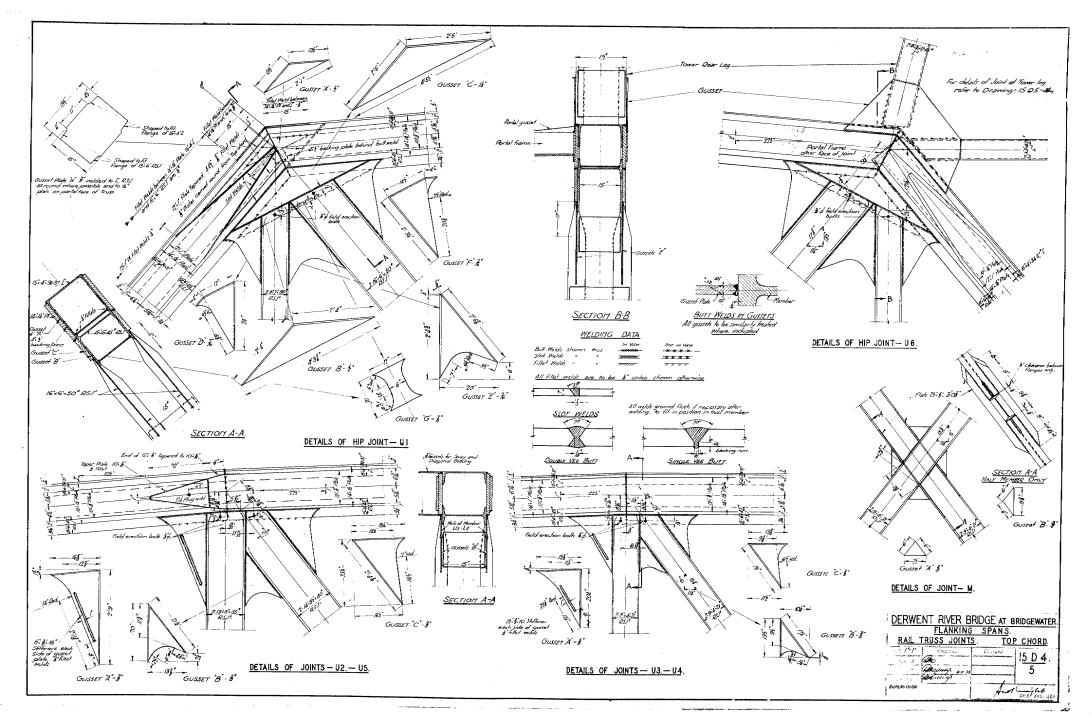


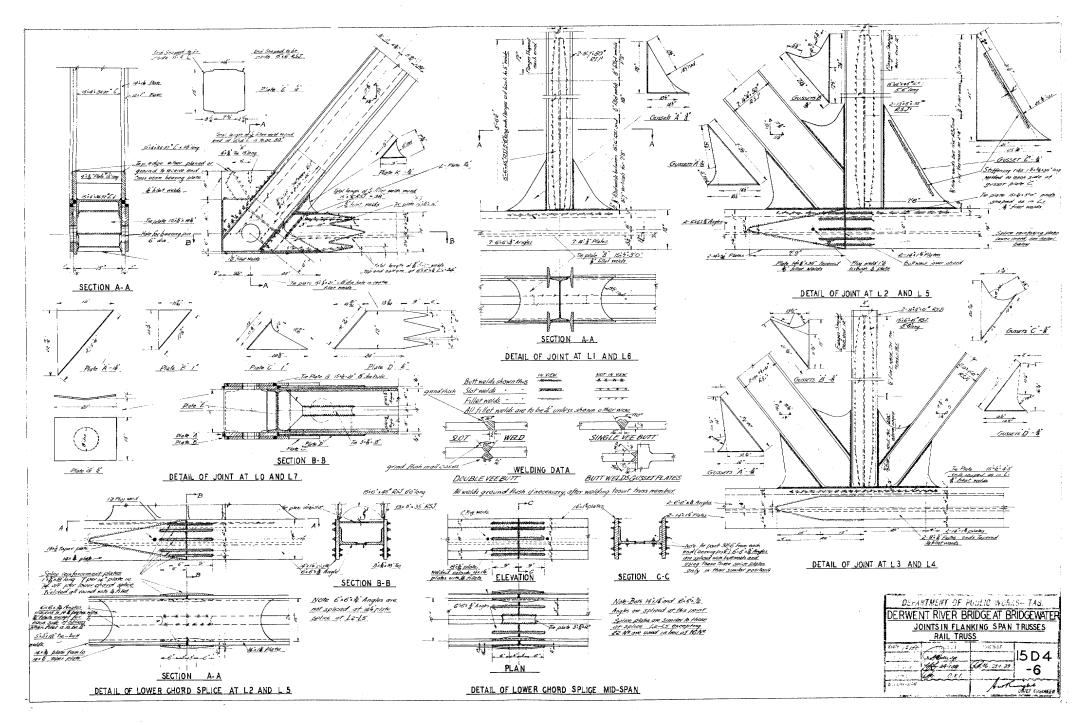




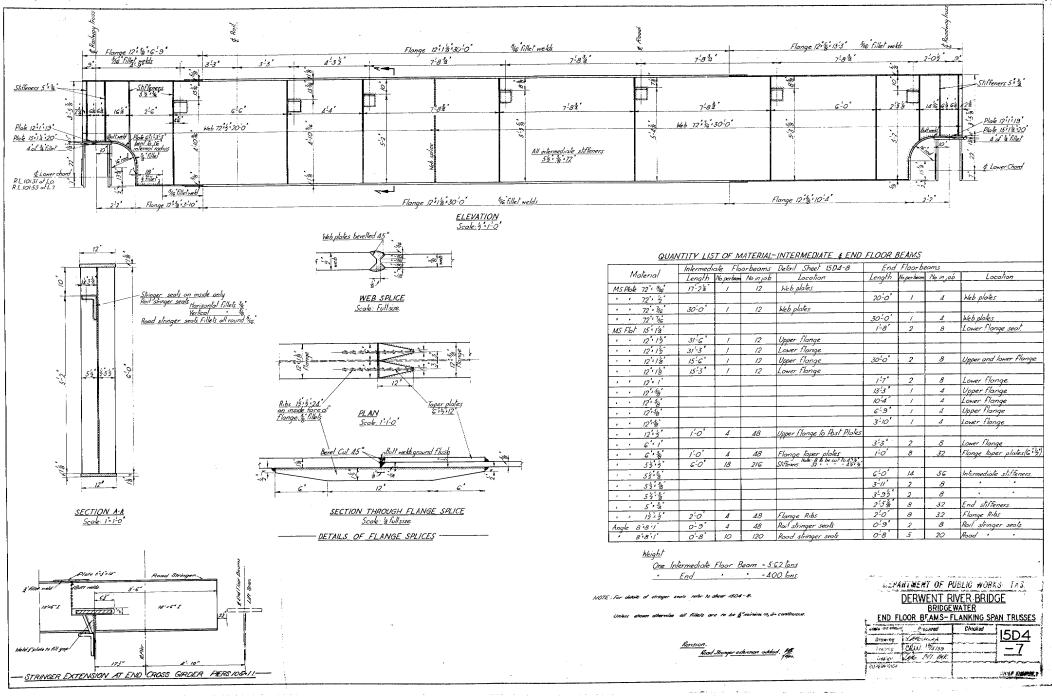
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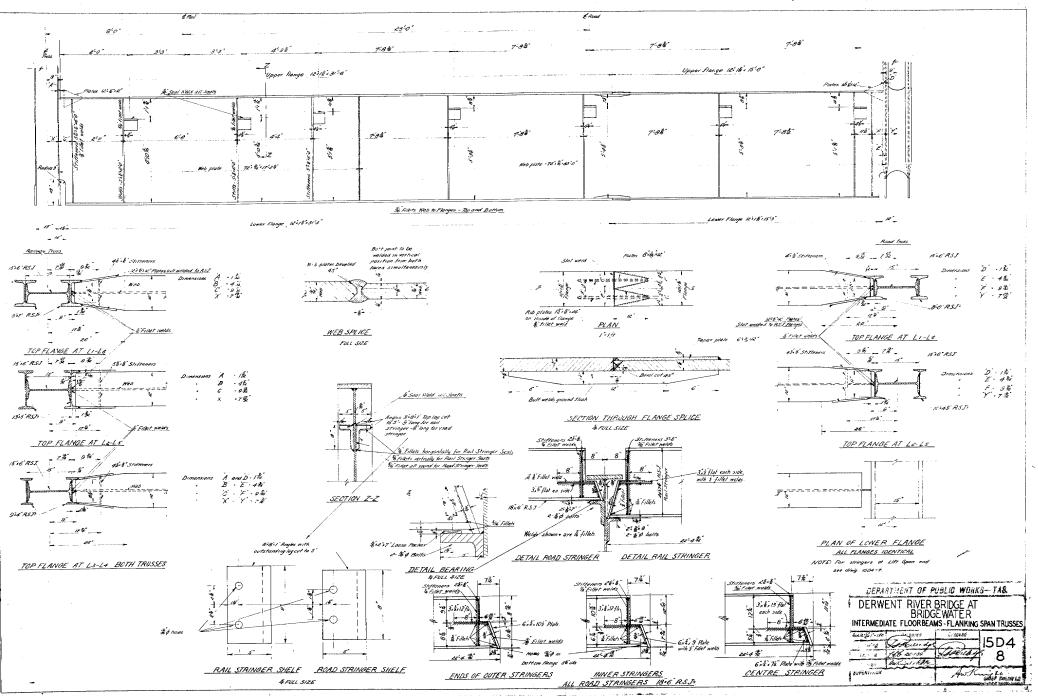




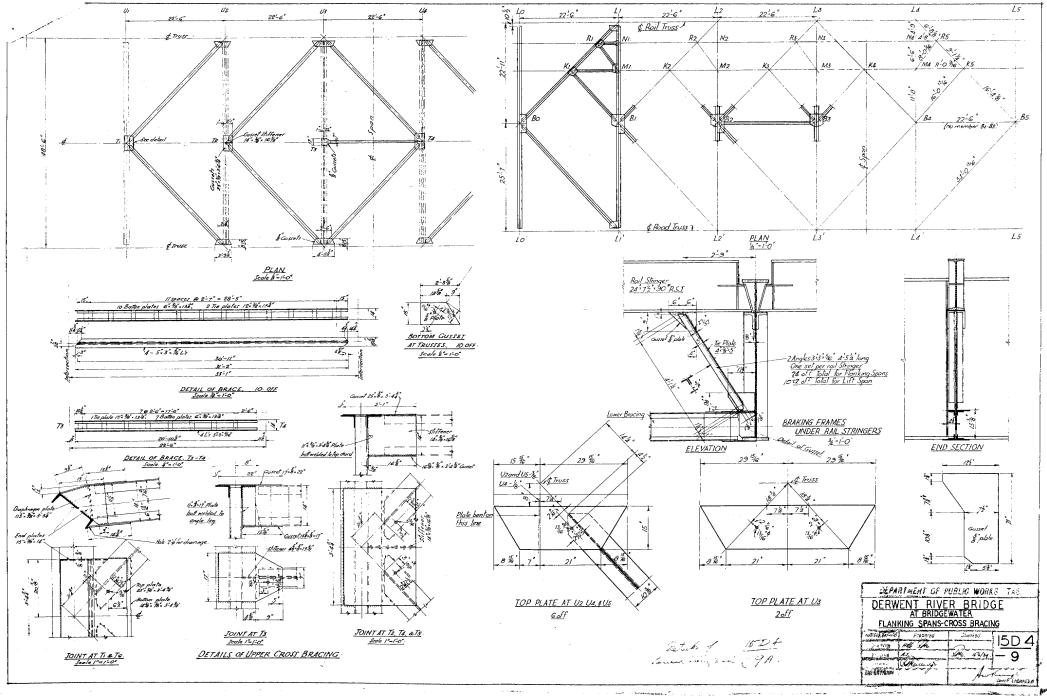




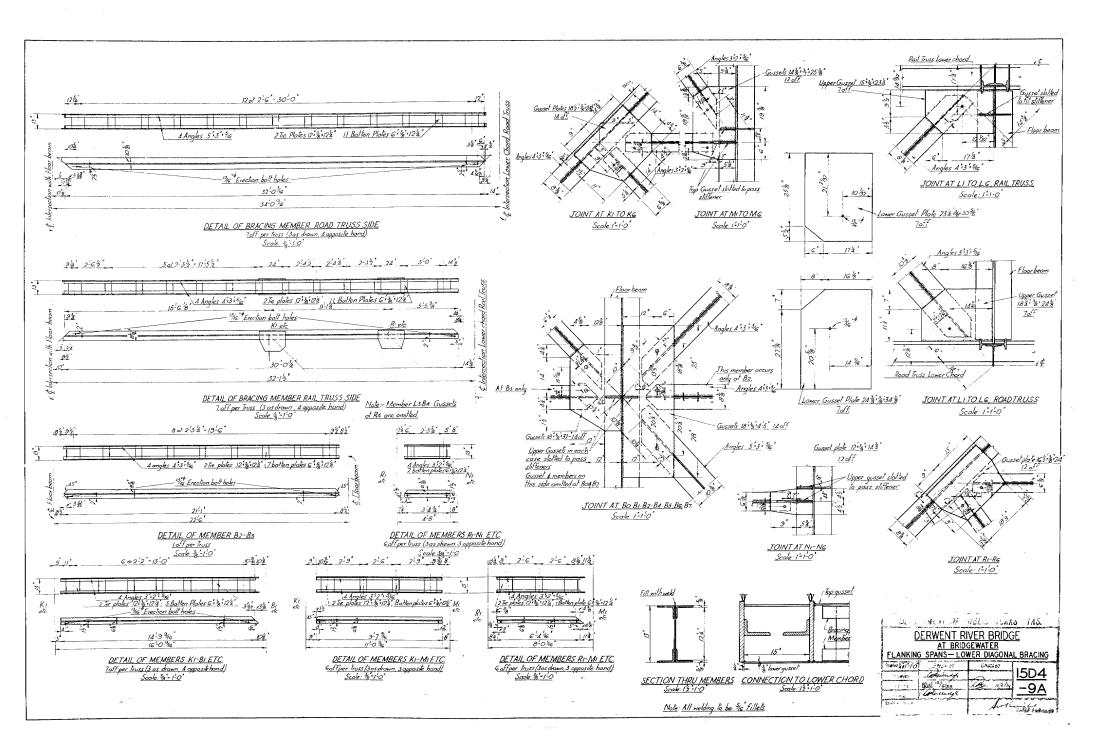


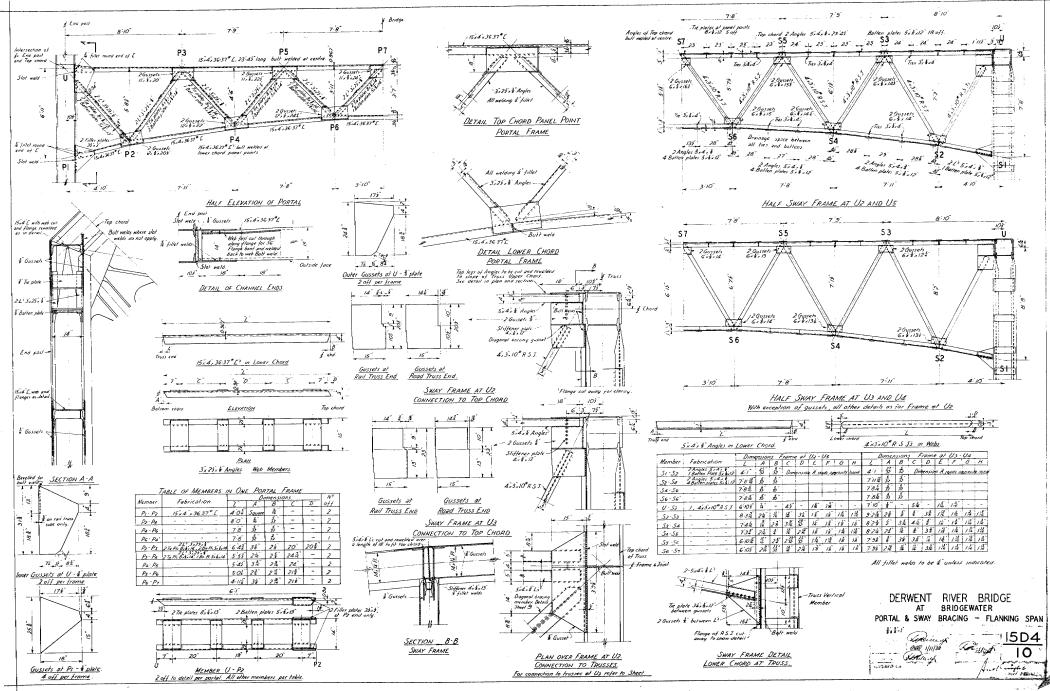


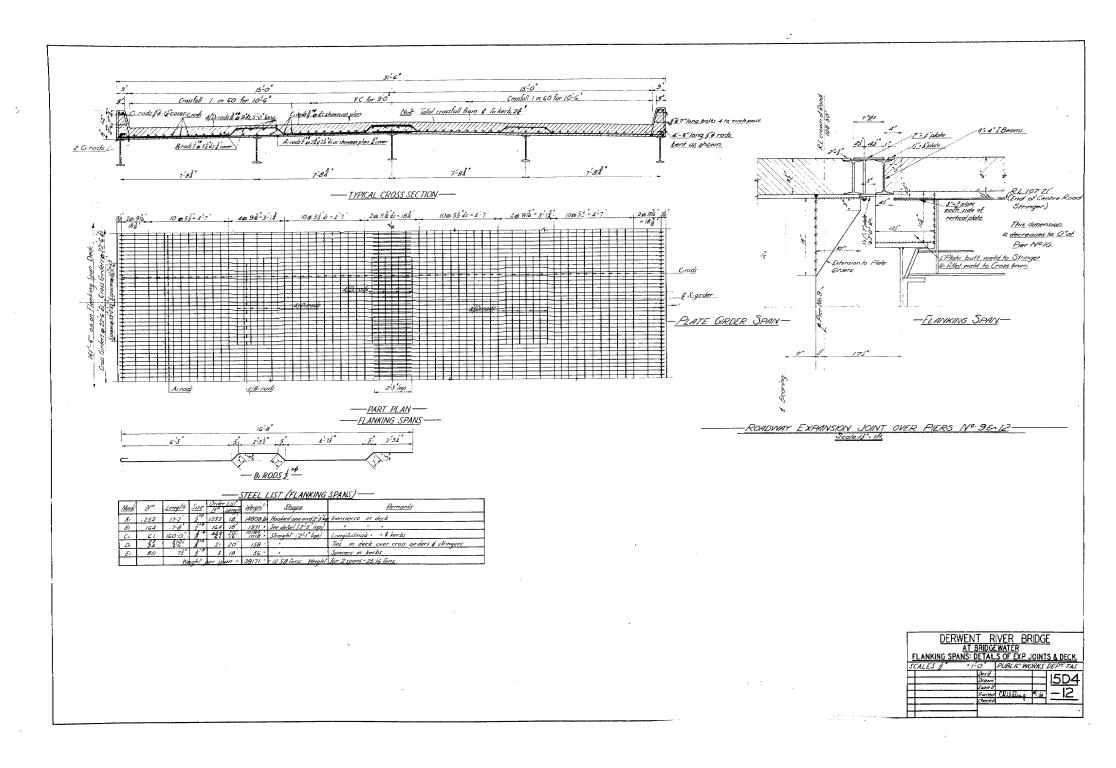
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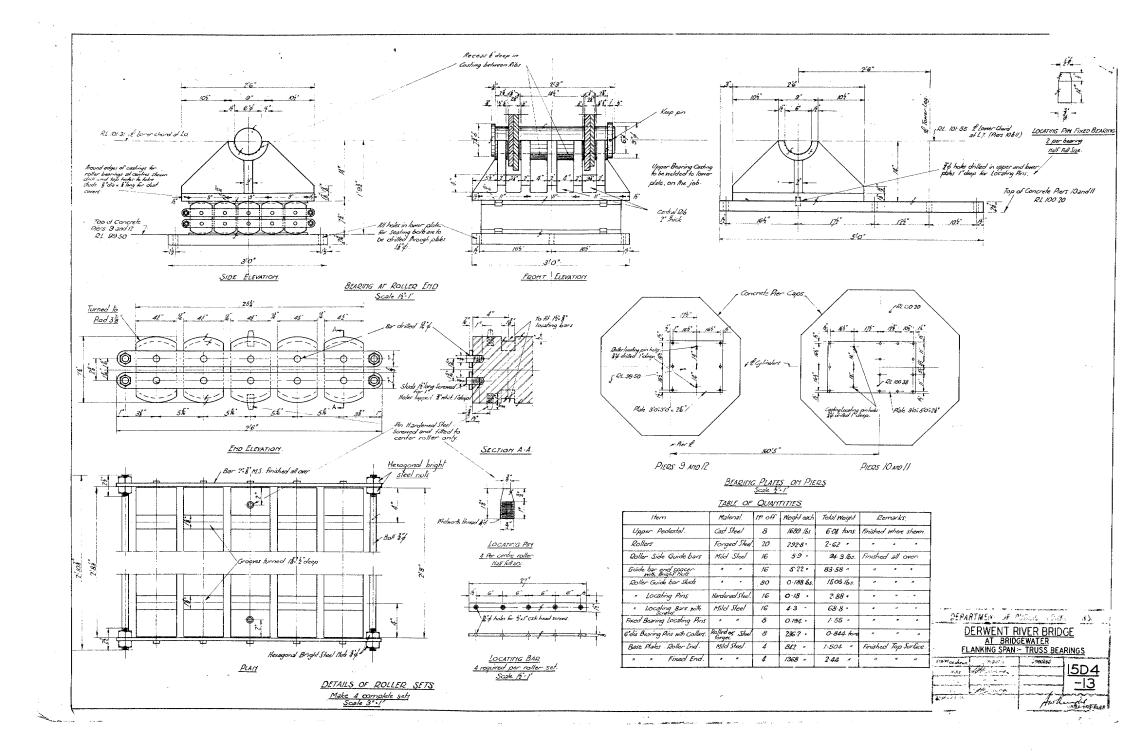


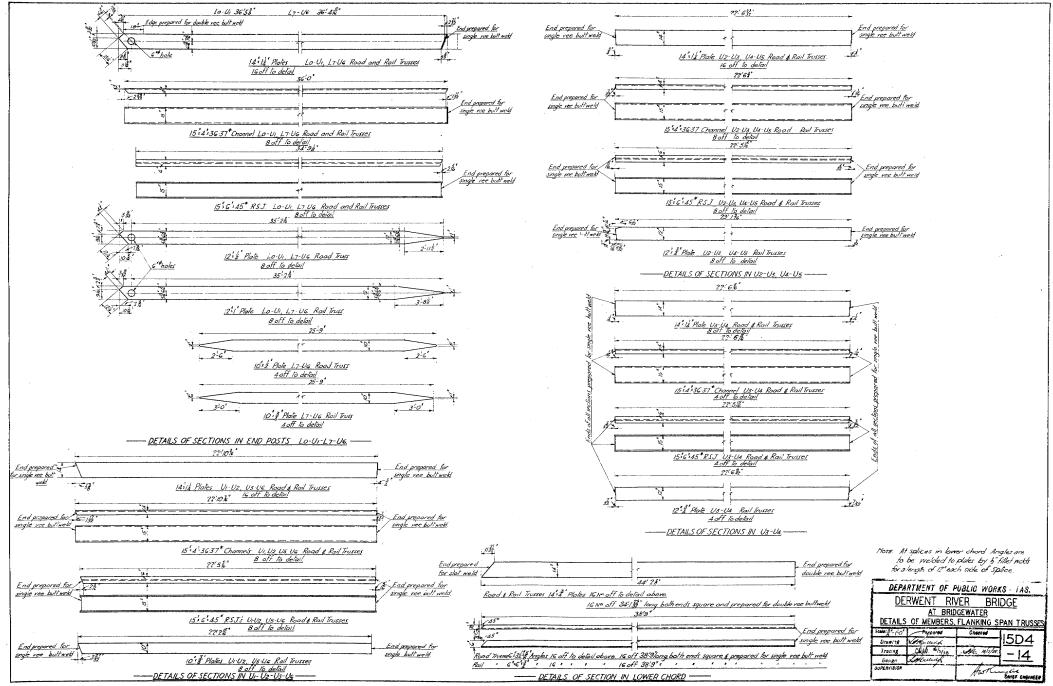
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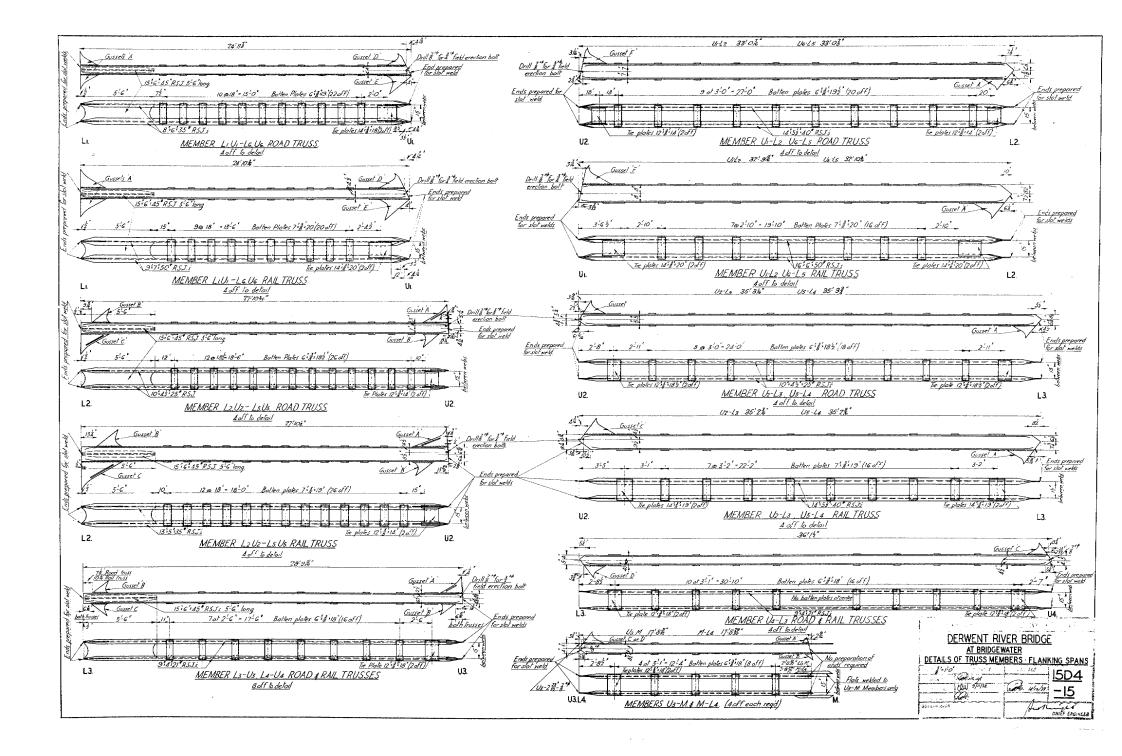


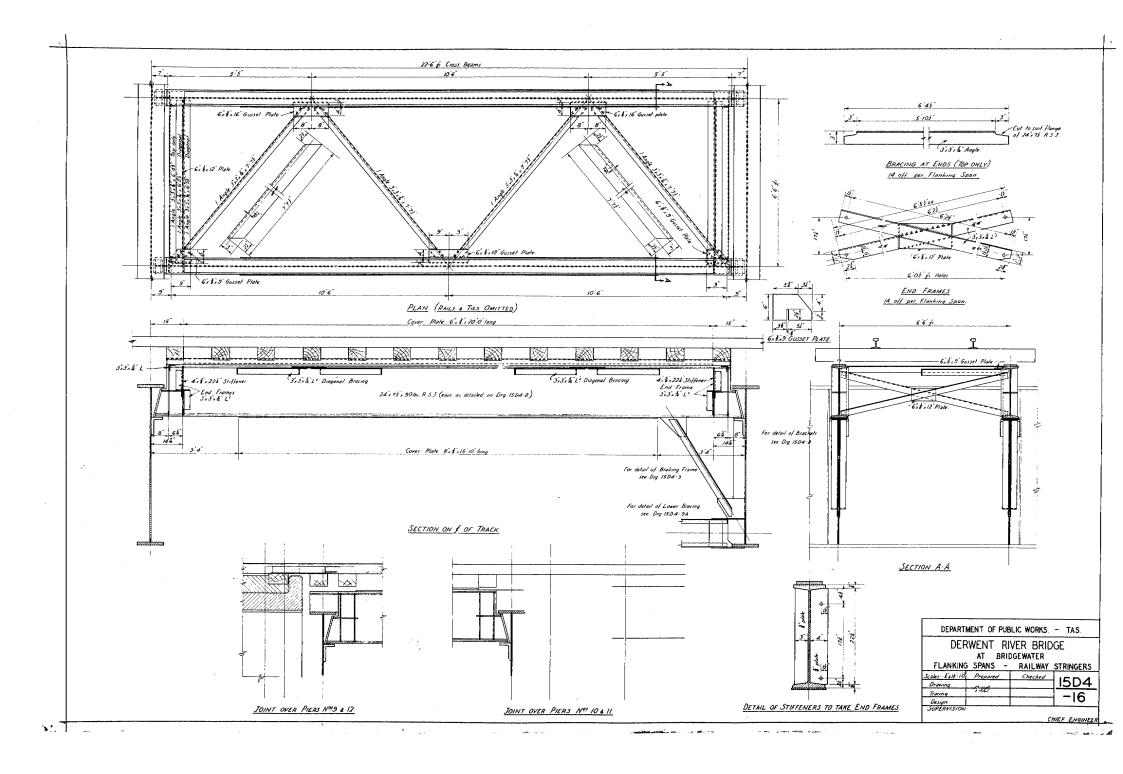


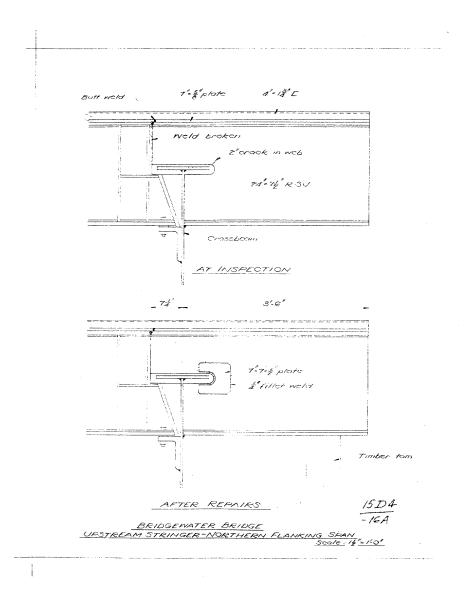




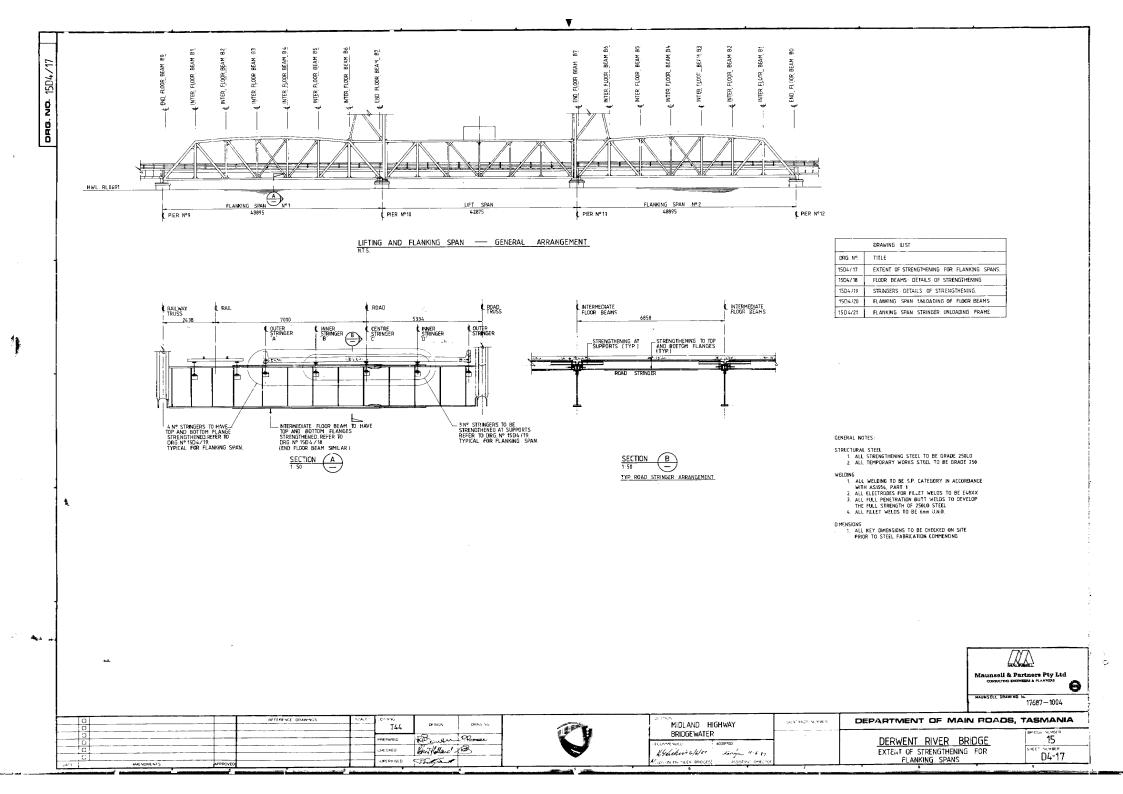


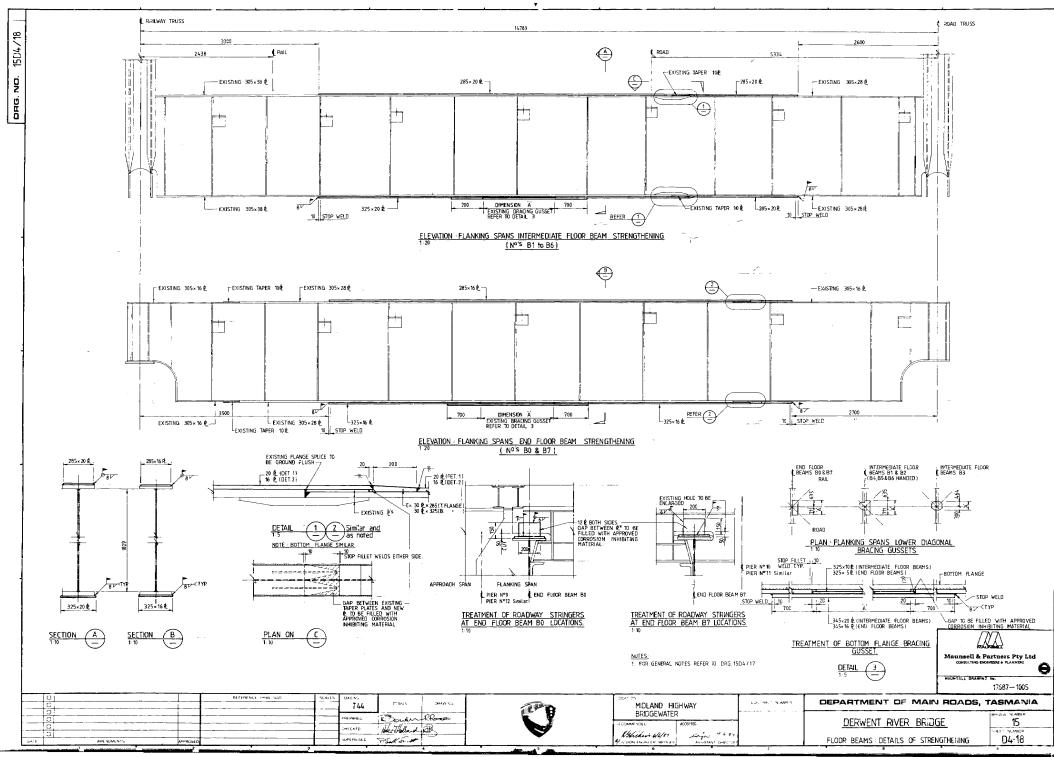


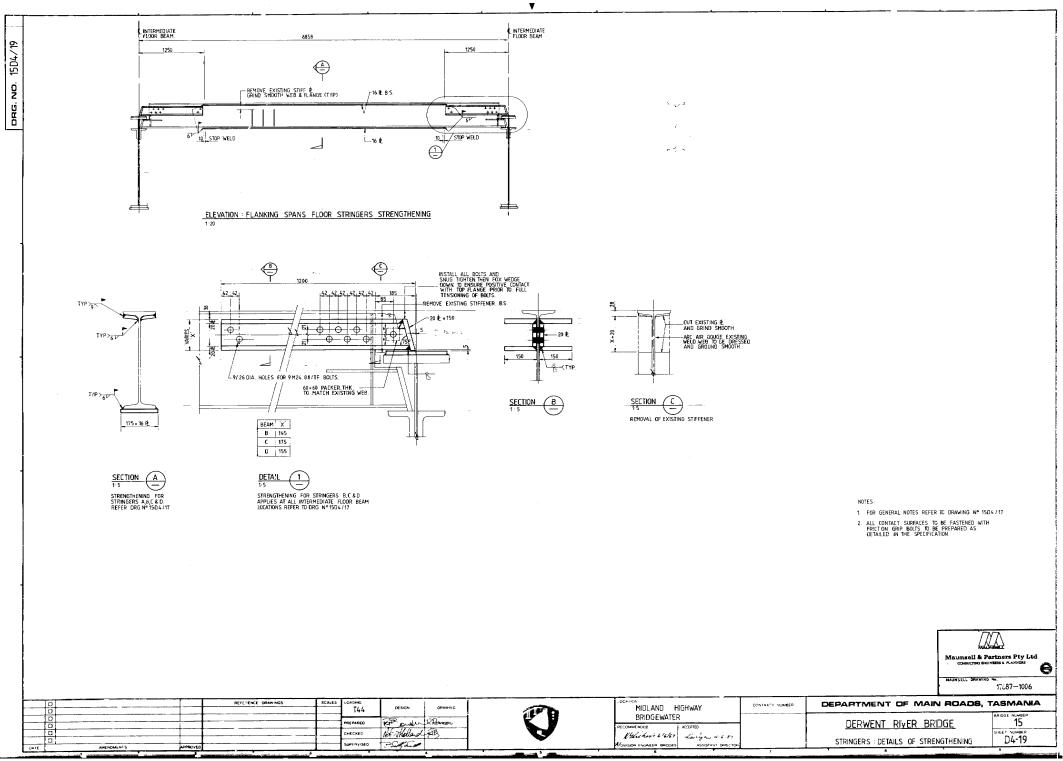




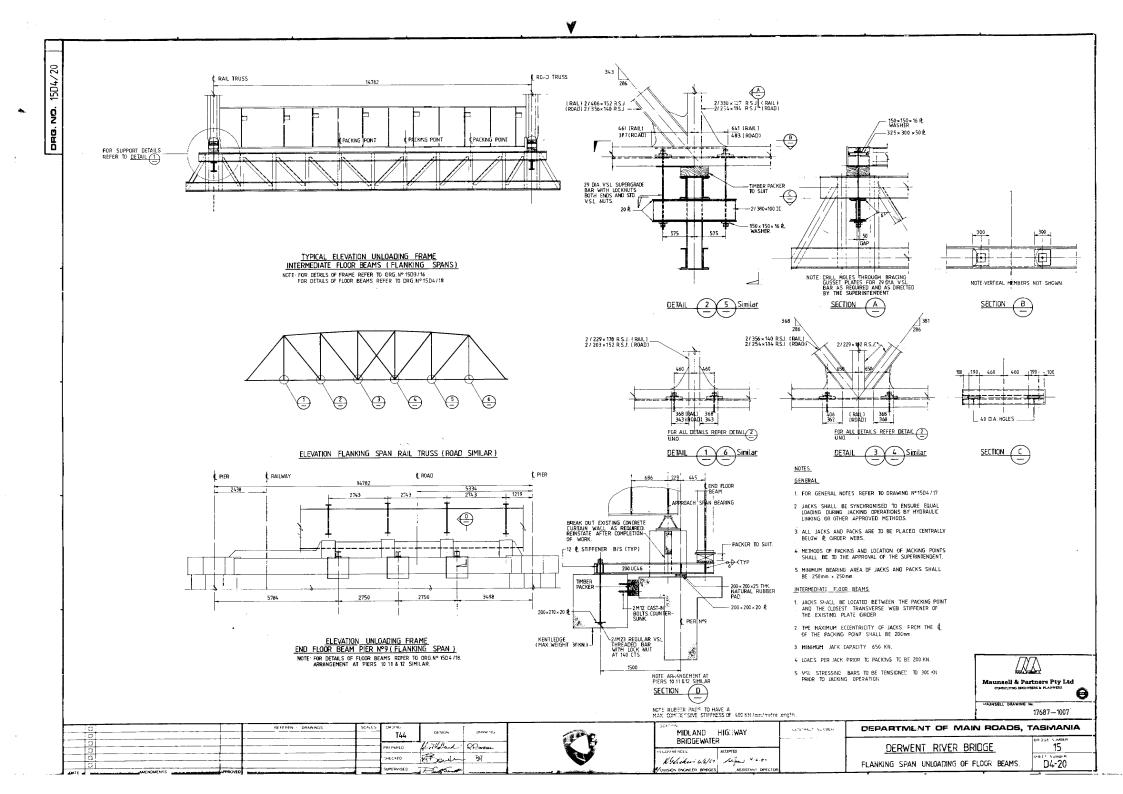
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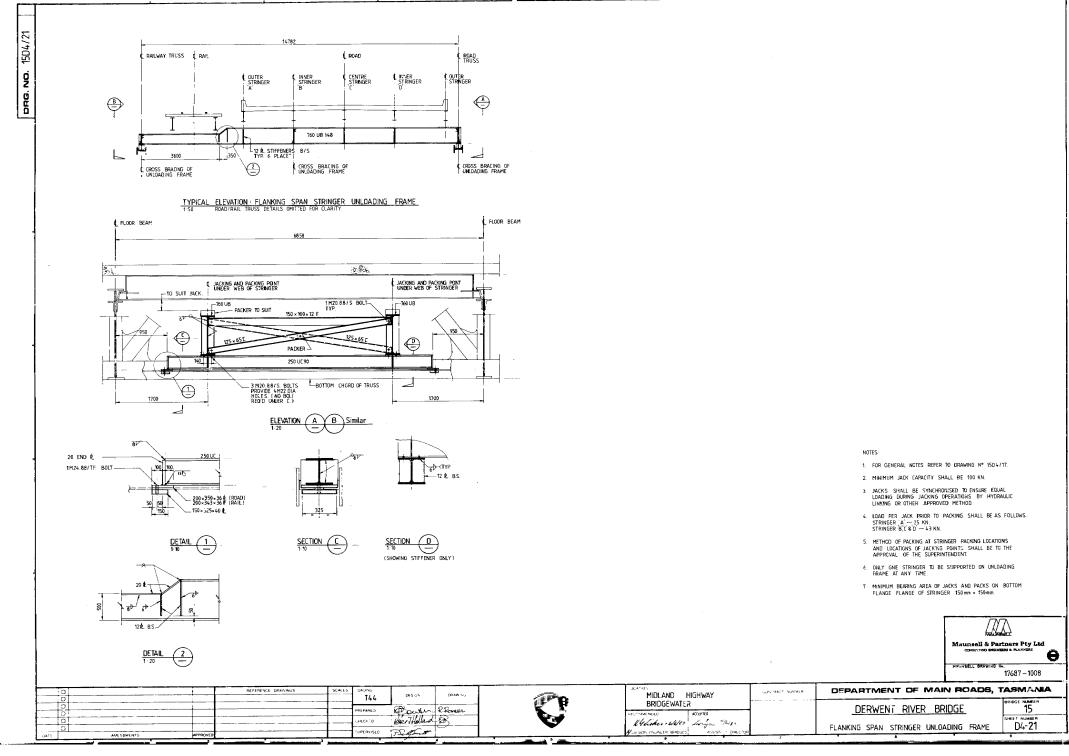






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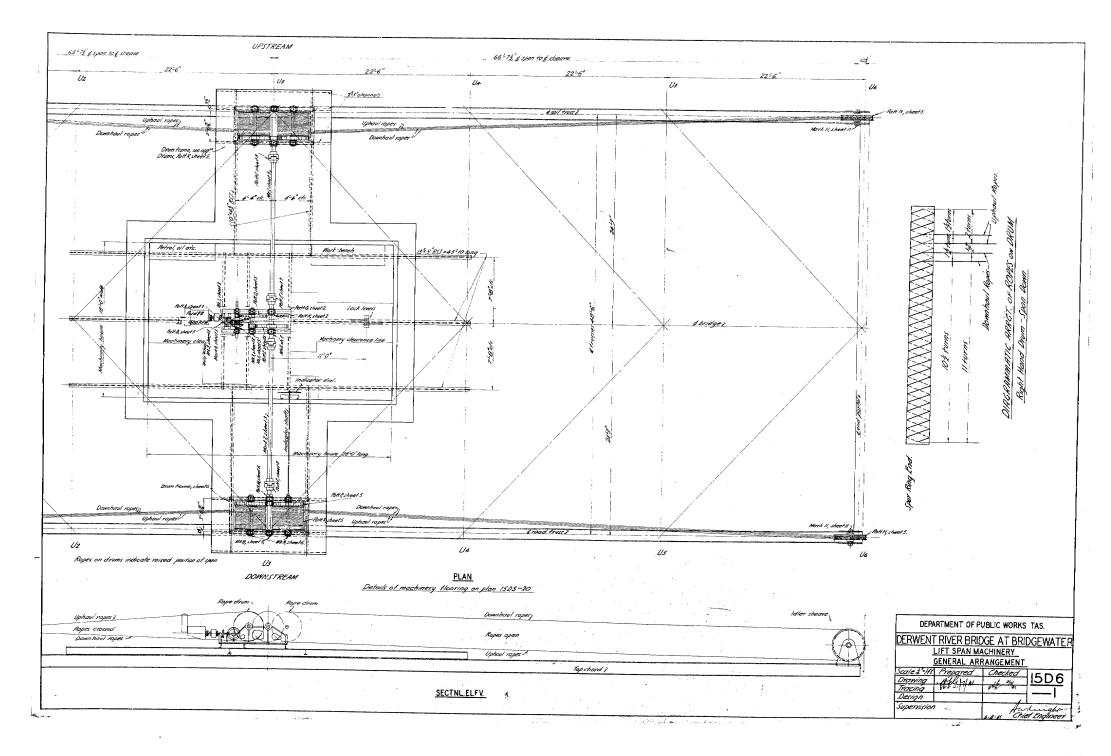


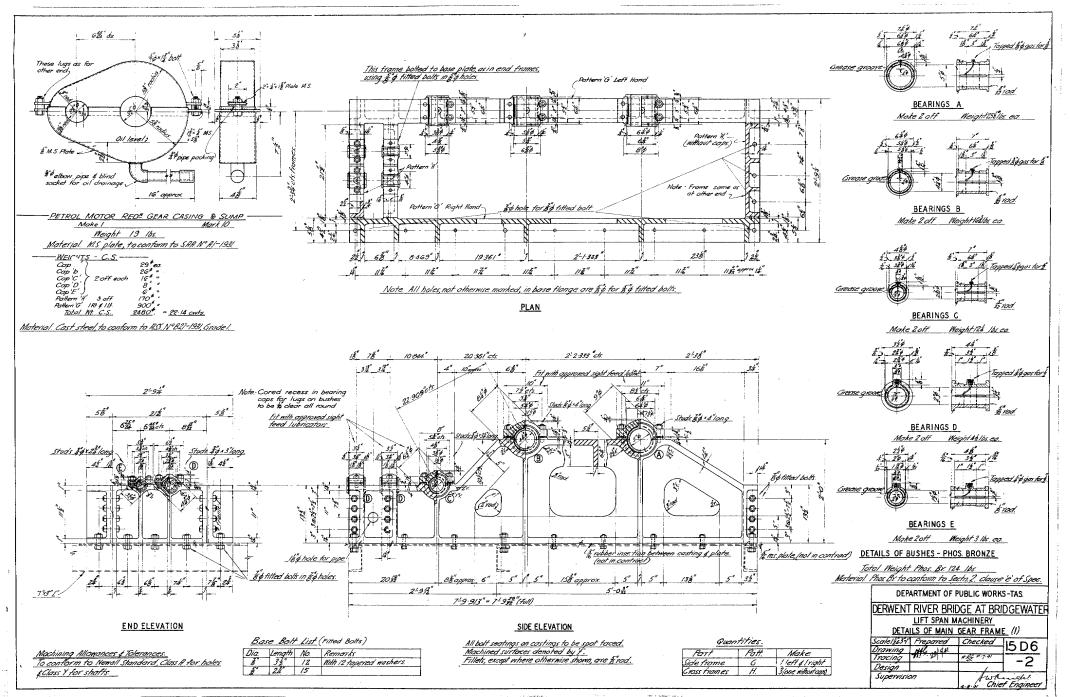
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4	D6-03	SHAFTS AND GEARS		
5	D6-05	SPUR WHEELS, DRUM AND IDLER	SHEAVE	
6	D6-06	CAST STEEL DRUM FRAMES		
7	D6-07	HEIGHT INDICATOR		
8	D6-08	PNEUMATIC BUFFERS		
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10	D6-09A	ROAD GATES COUNTER WEIGHTS		
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11	D6-11	COUNTER WEIGHT SHEAVE,	TRUNION HEELAND LINK	BEARING
12	D6-12	ROPE SOCKET AND CAST STEEL	CLAMP	
13	D6-13	RAIL LOCK MACHINERY	ARRANGEMENT	
14	D6-14	LOCKING BARS AND COVER		
15	D6-14A	LOCKING BARS AND COVER	AMENDMENTS	
16	D6-15	STOPS ASSEMBLY		
17	D6-16	RAIL LOCKING BAR STOPS		
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20	D6-19	TRAFFIC GATES GUIDE LUG		
21	D6-20	ROPE ANCHOR BLOCK ROPE DRUM		
	D6-21	RAIL LOCKING BAR CLEVIS	PLATE (1968)	
22	D6-22	MAIN SWITCH BOARD WIRING		
23	D6-23	WIRING DIAGRAM		
24	D6-24	DESK CONTROL WIRING		
25	D6-25	CONTROL CIRCUITS WIRING		
	D6-26	RAIL LOCK AUXILLIARY AND	LIMIT SWITCH	
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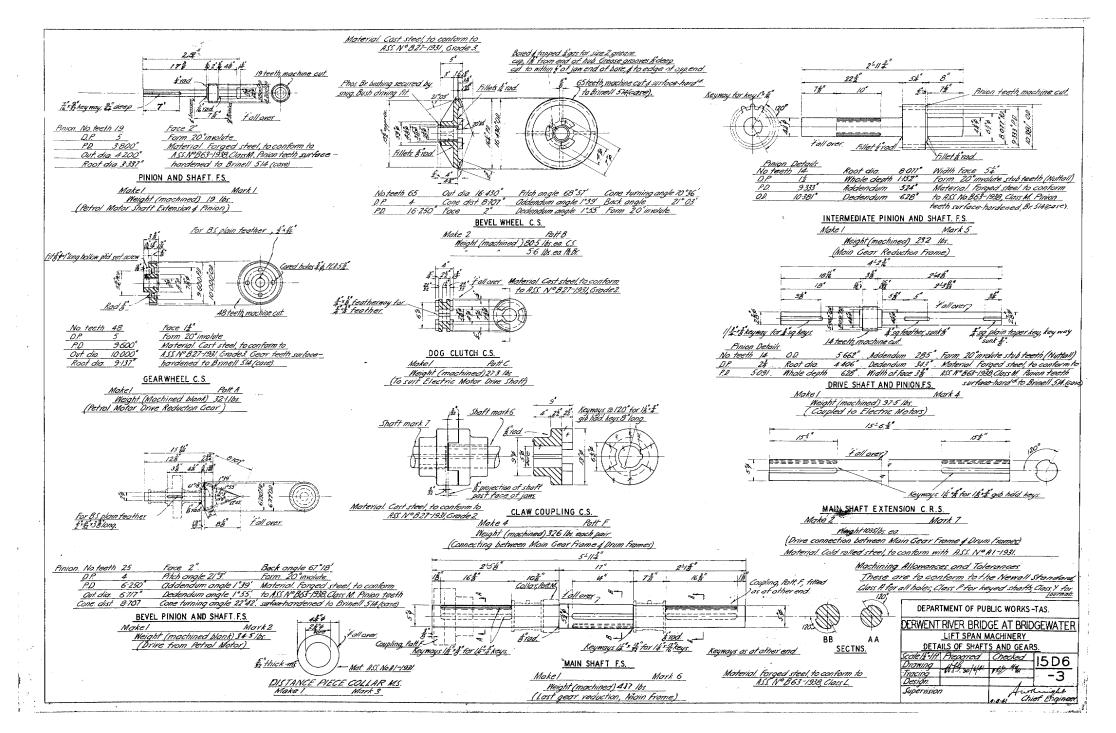
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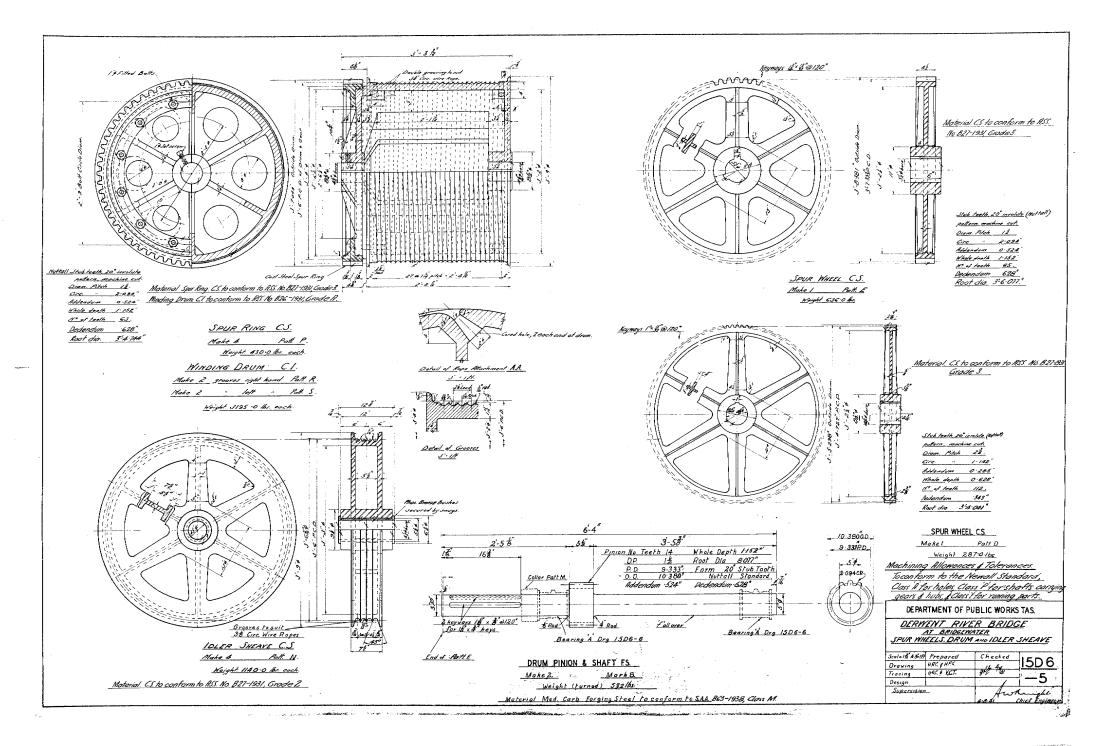
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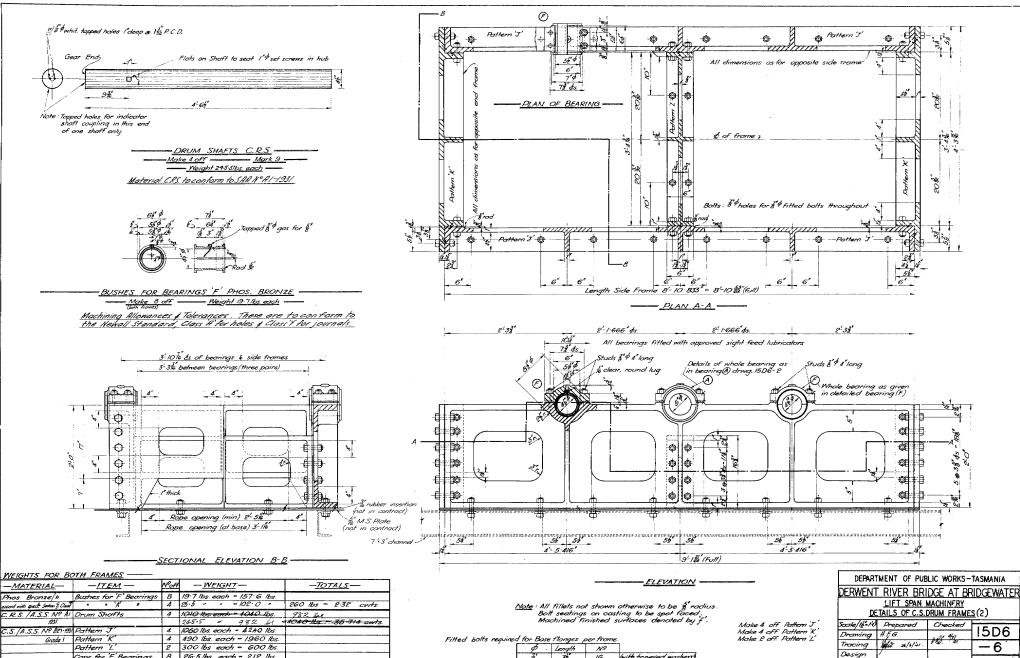
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Caps for 'F' Bearings 8 26:5 lbs. each = 212 lbs. Caps for 'A' Bearings 4 29 lbs. each = 116 lbs. 3128 lbs. = 63 6 cm/s.

Bolts & Studs - 216 required



(with topered washers)

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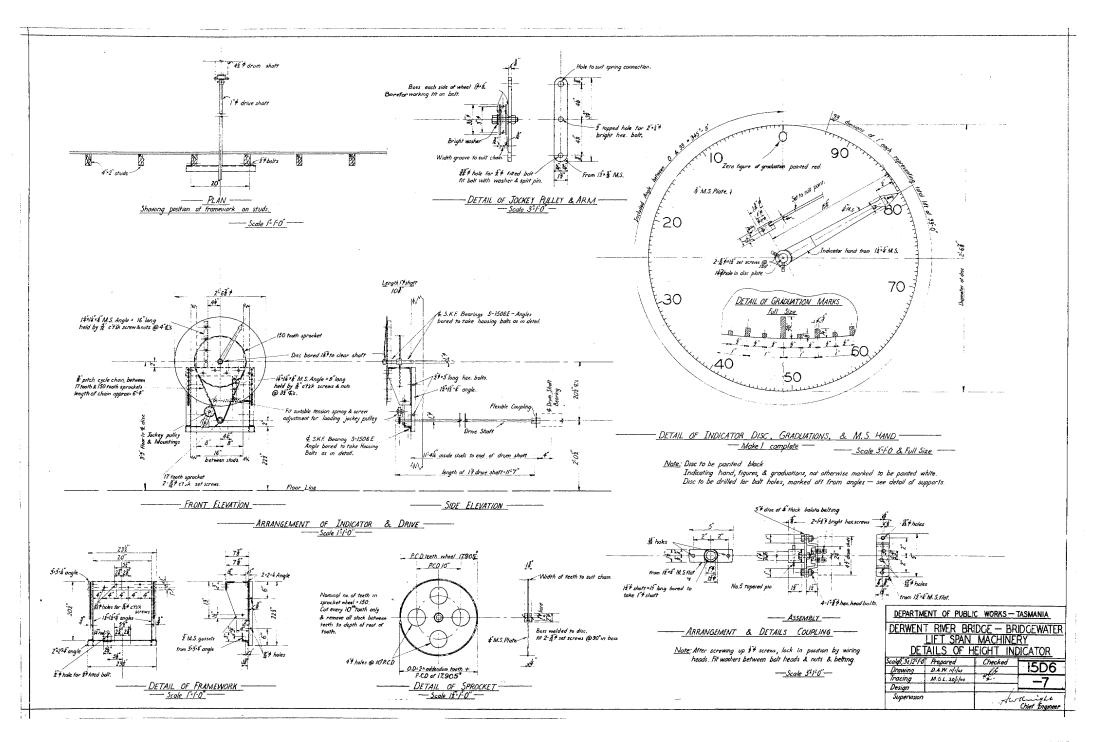
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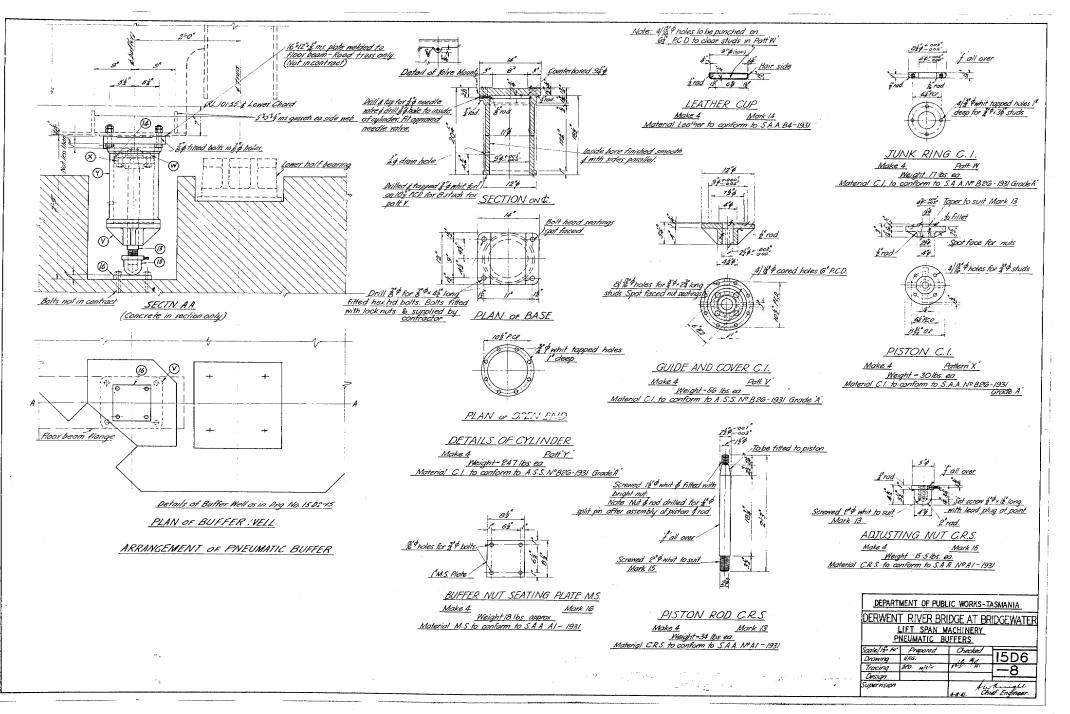
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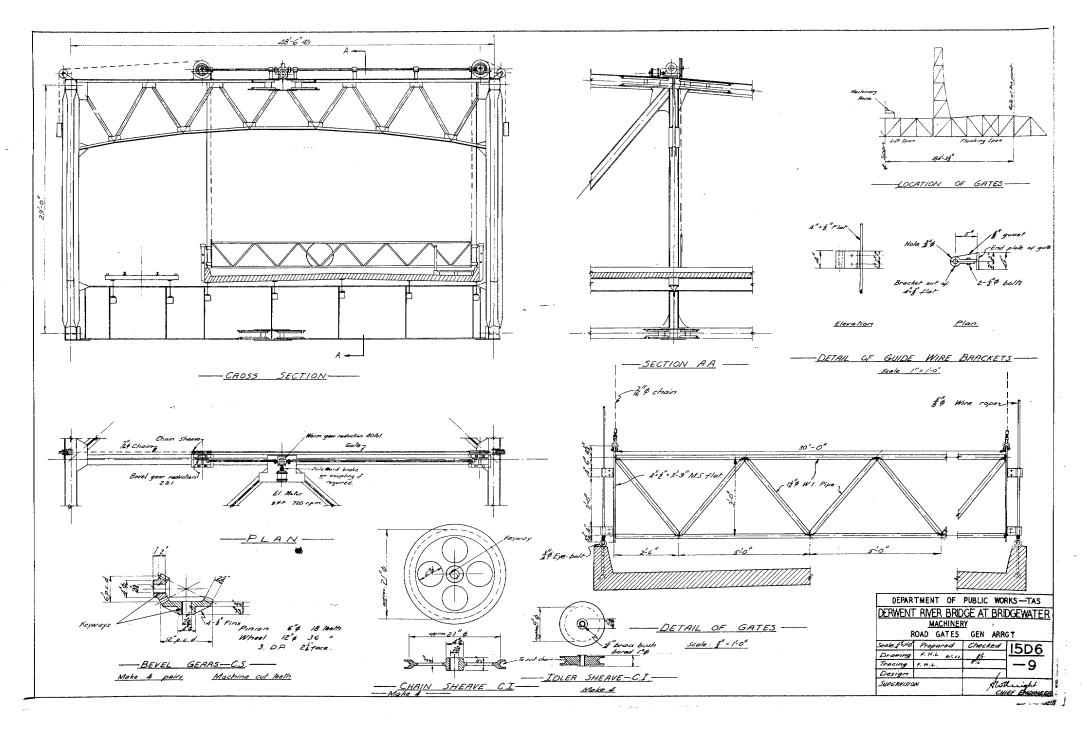
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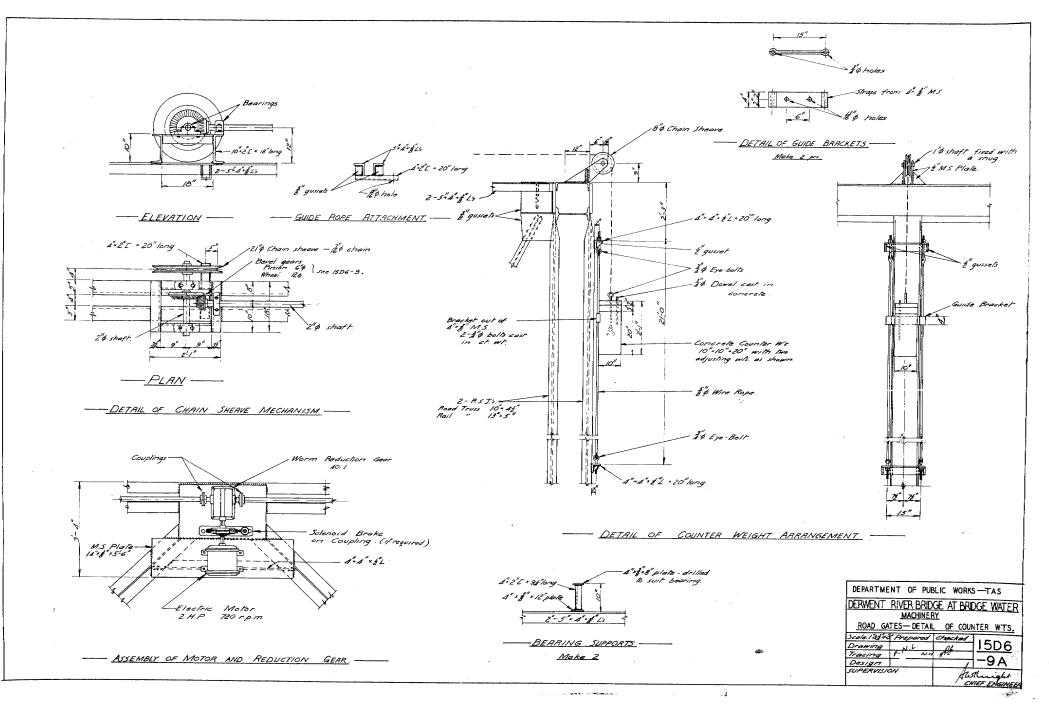


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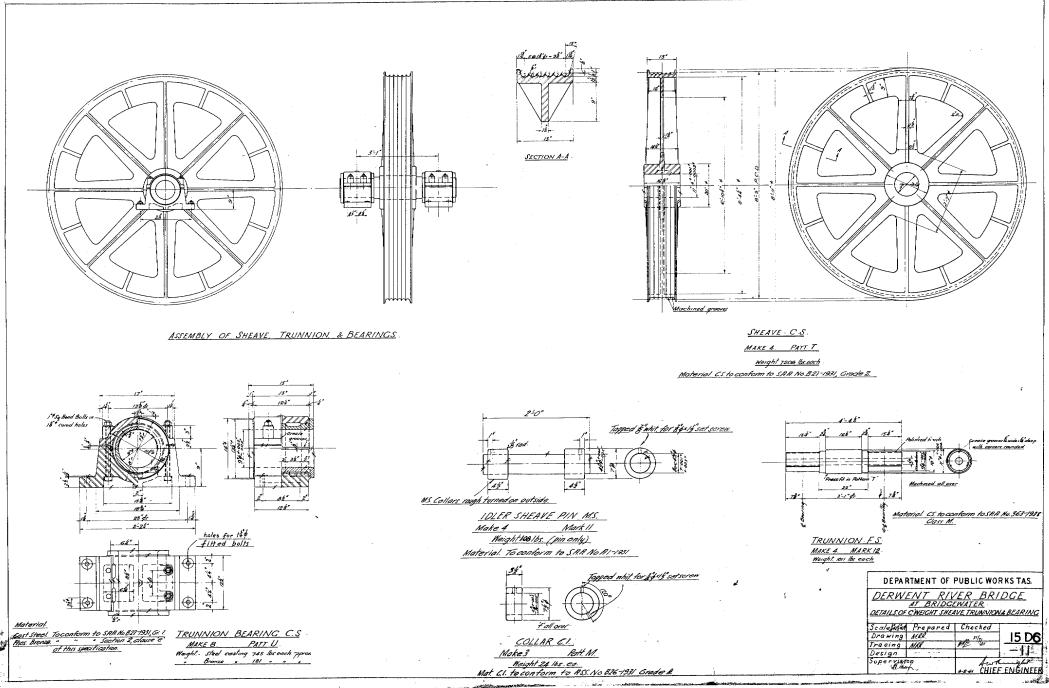


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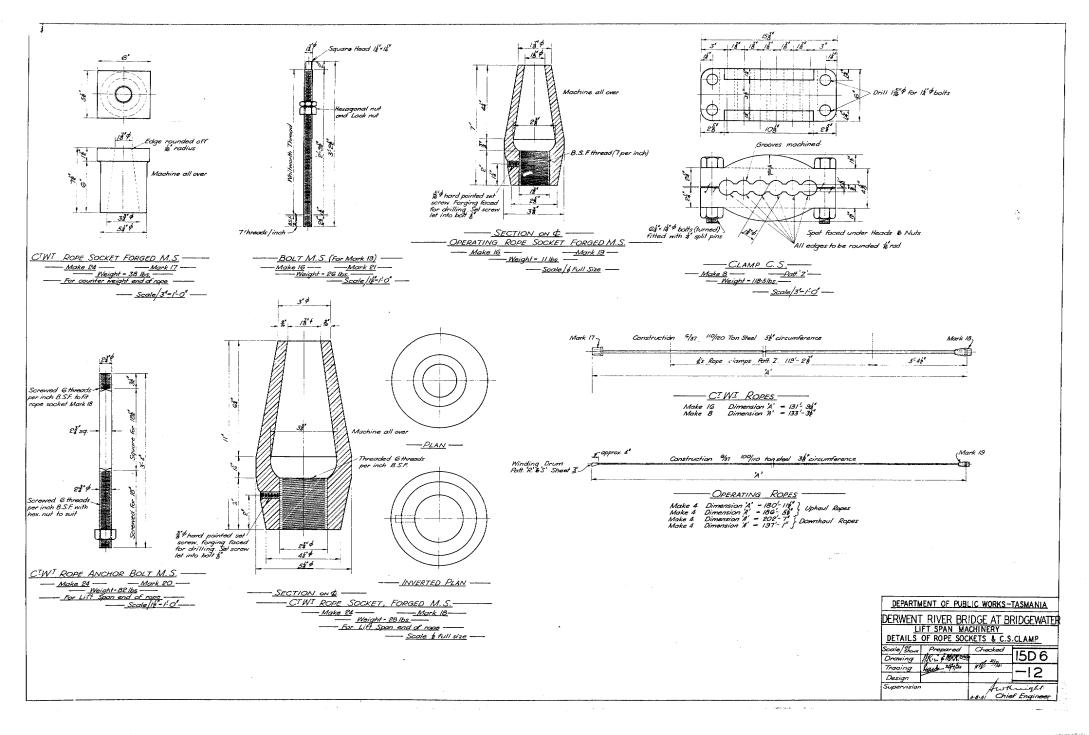




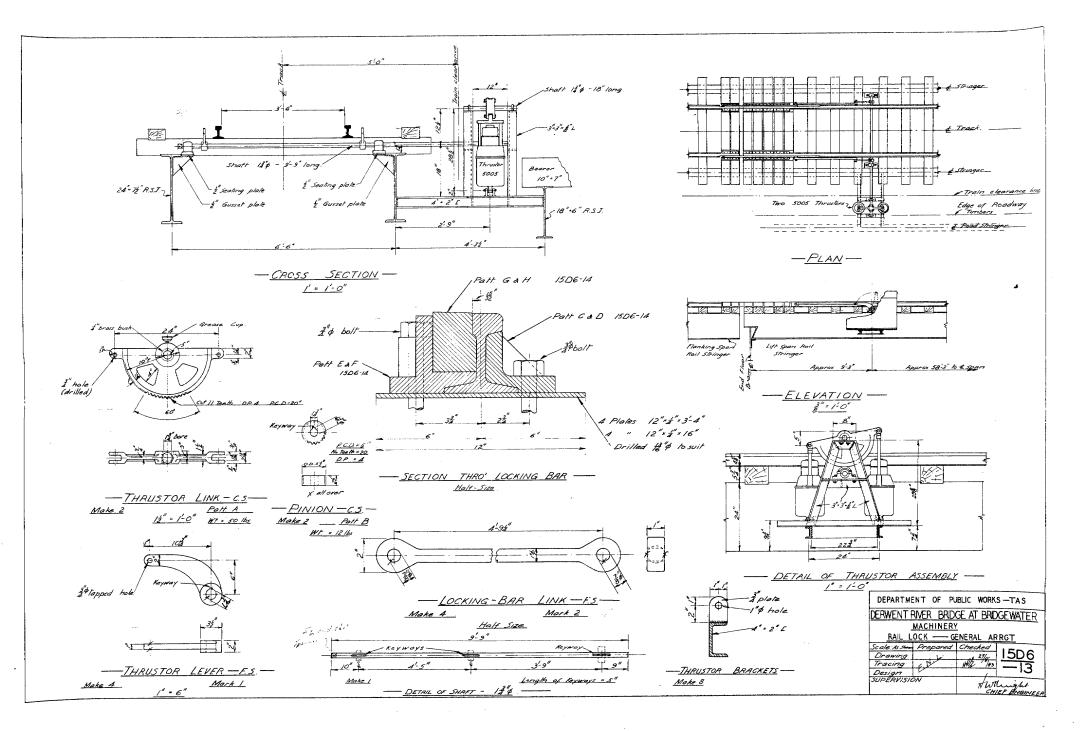
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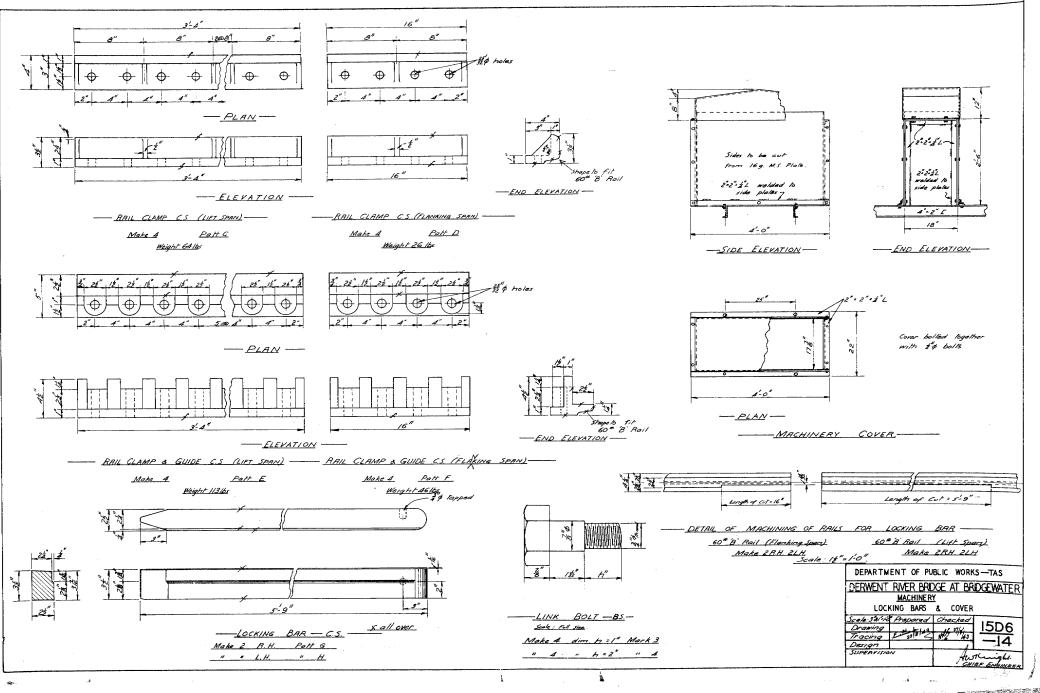
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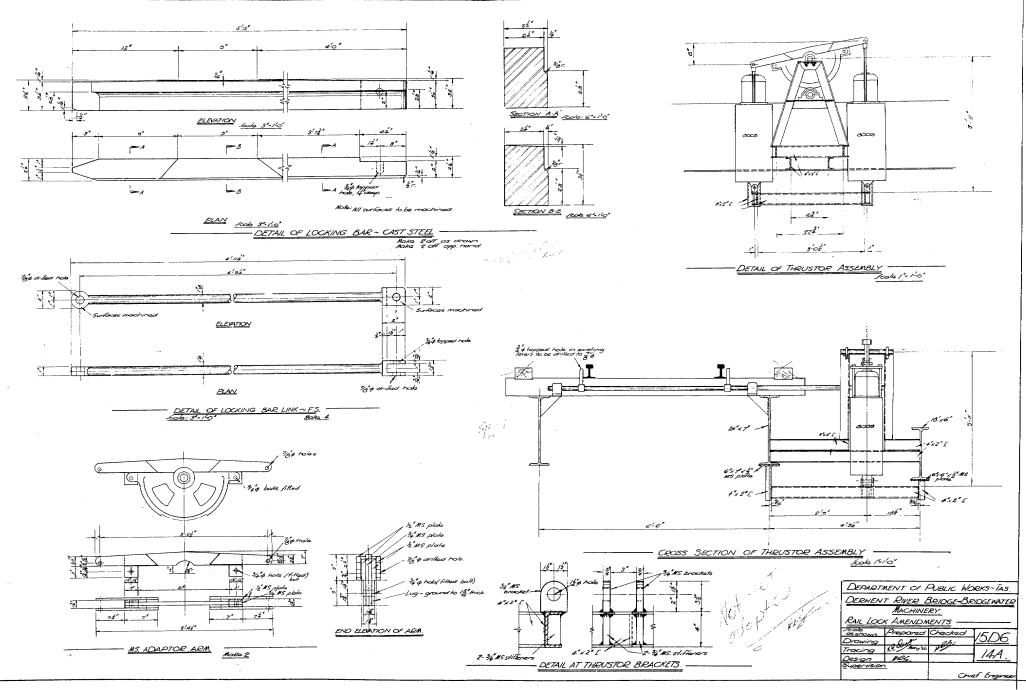


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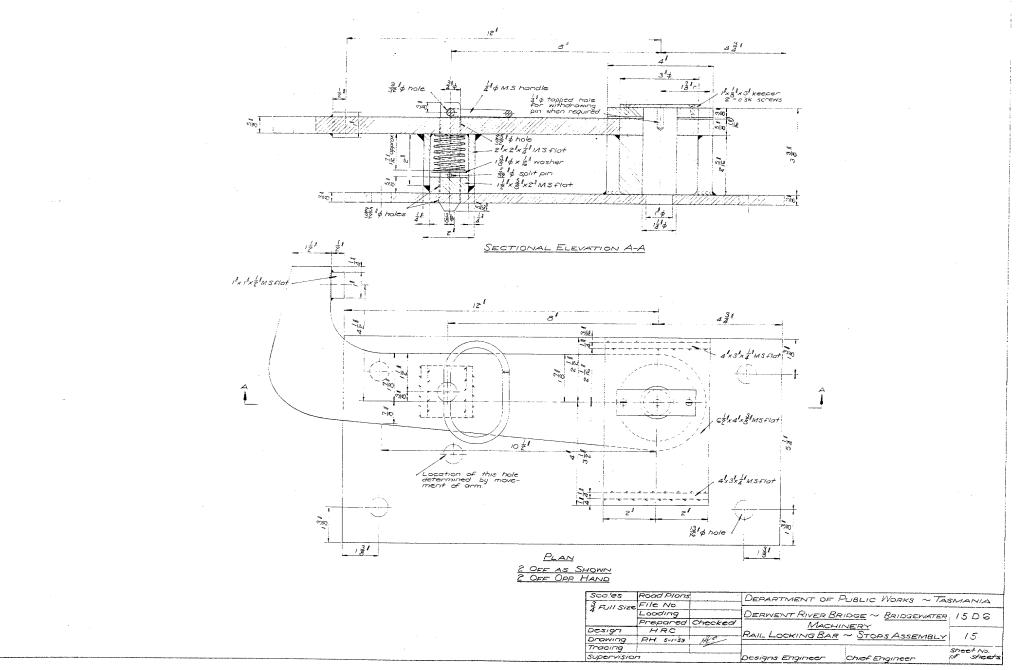
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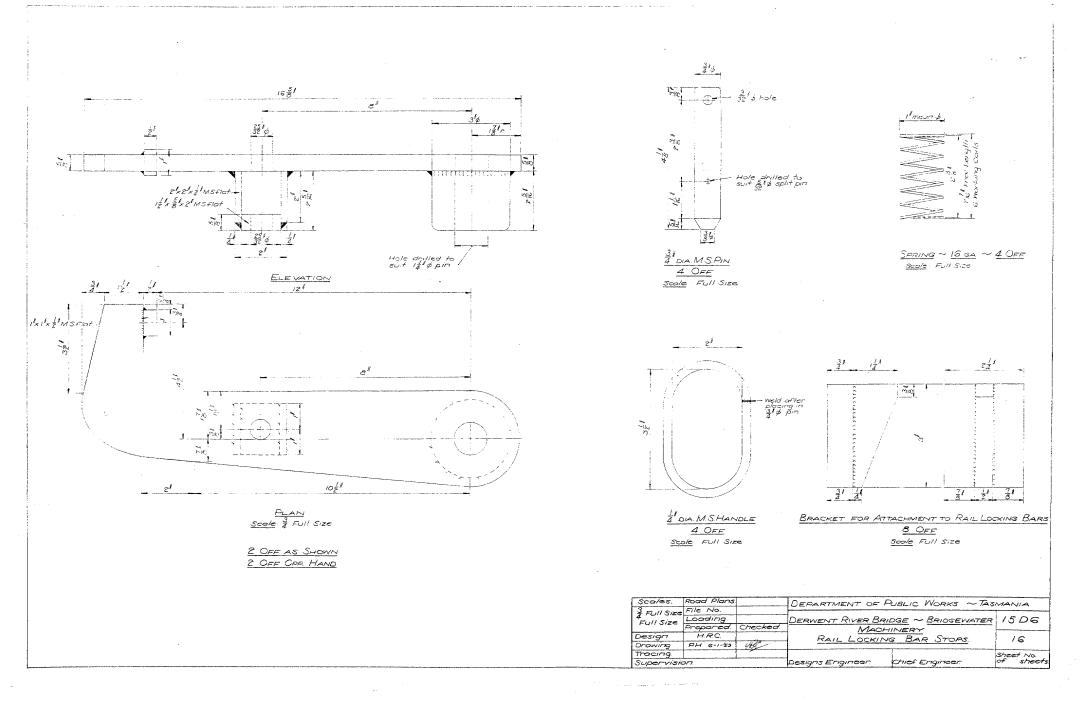
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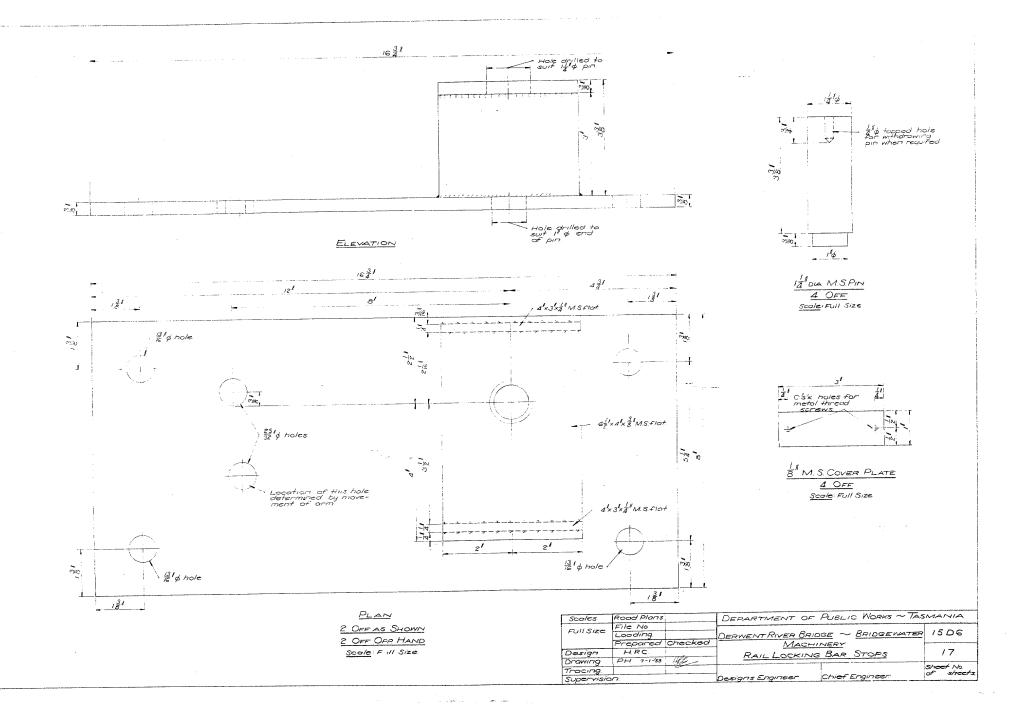
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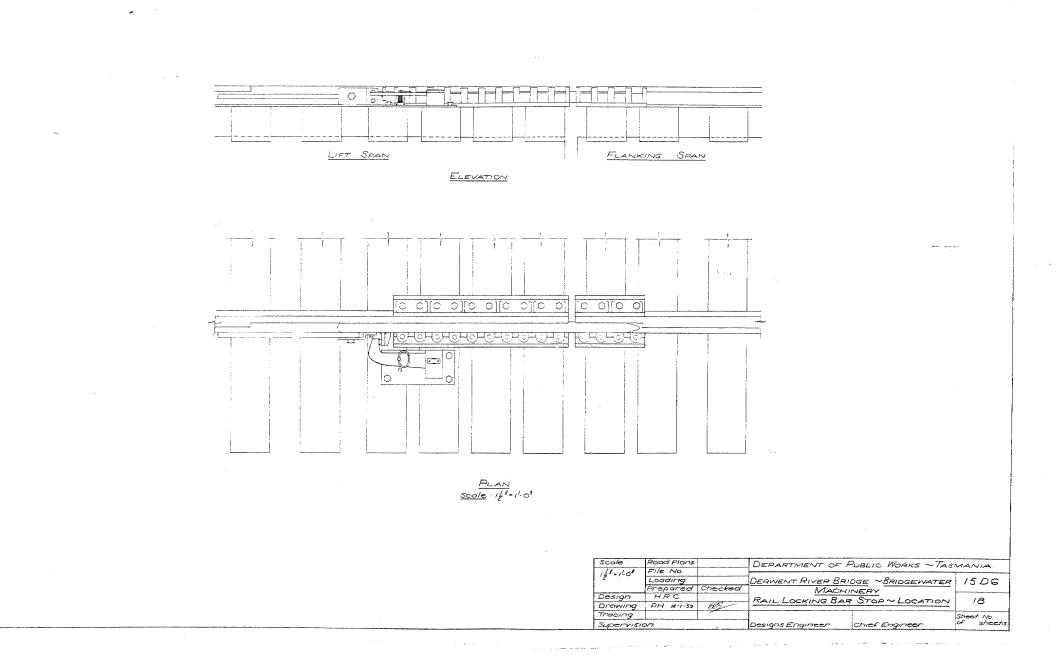
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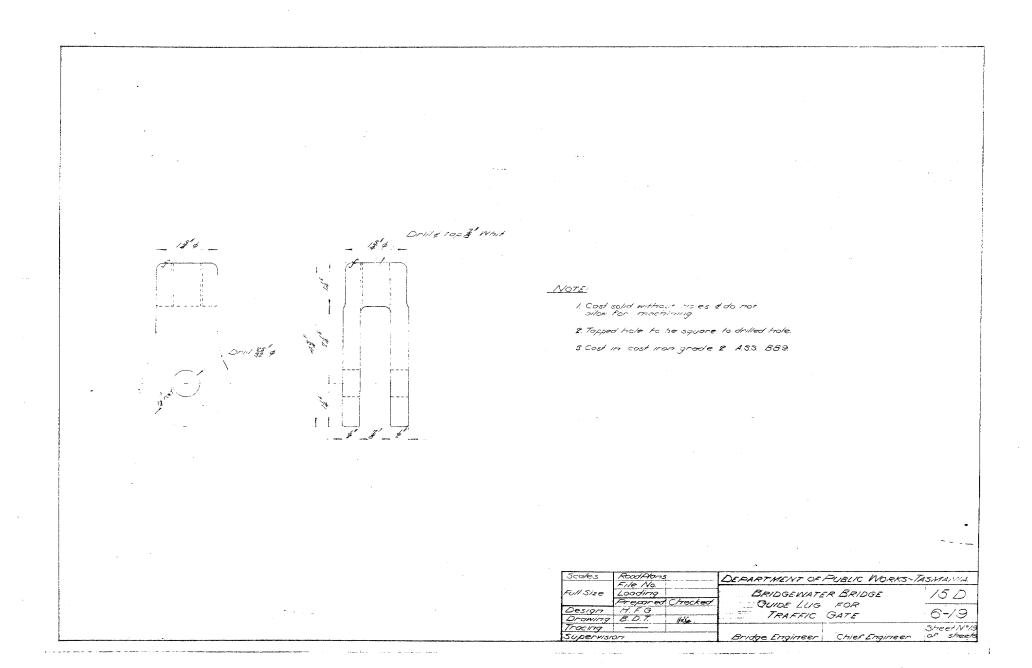


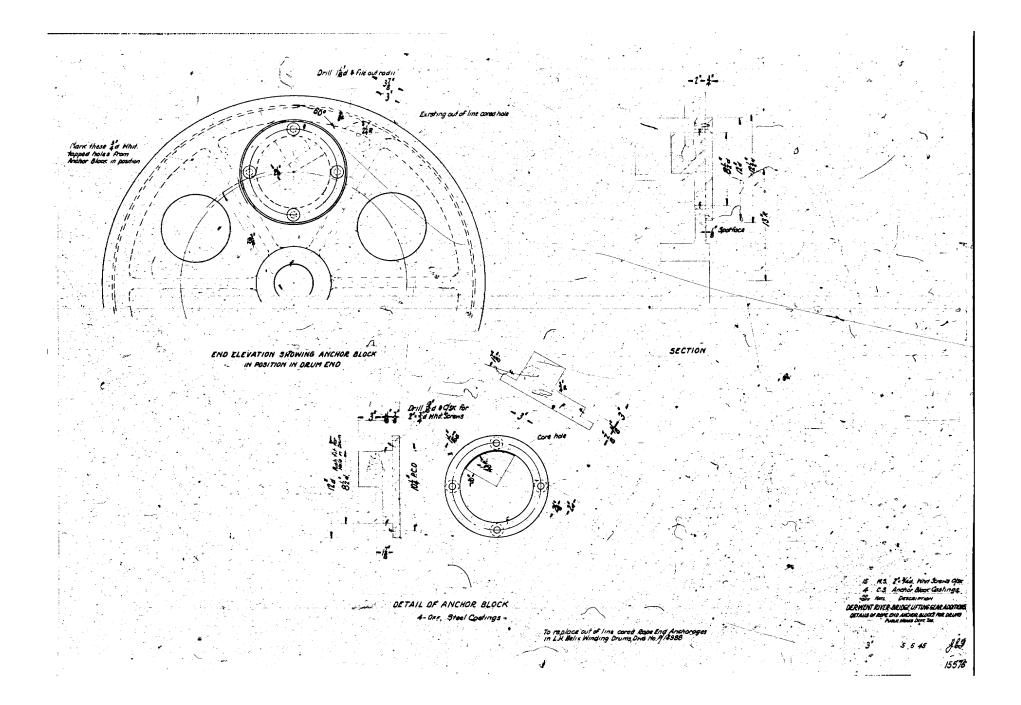
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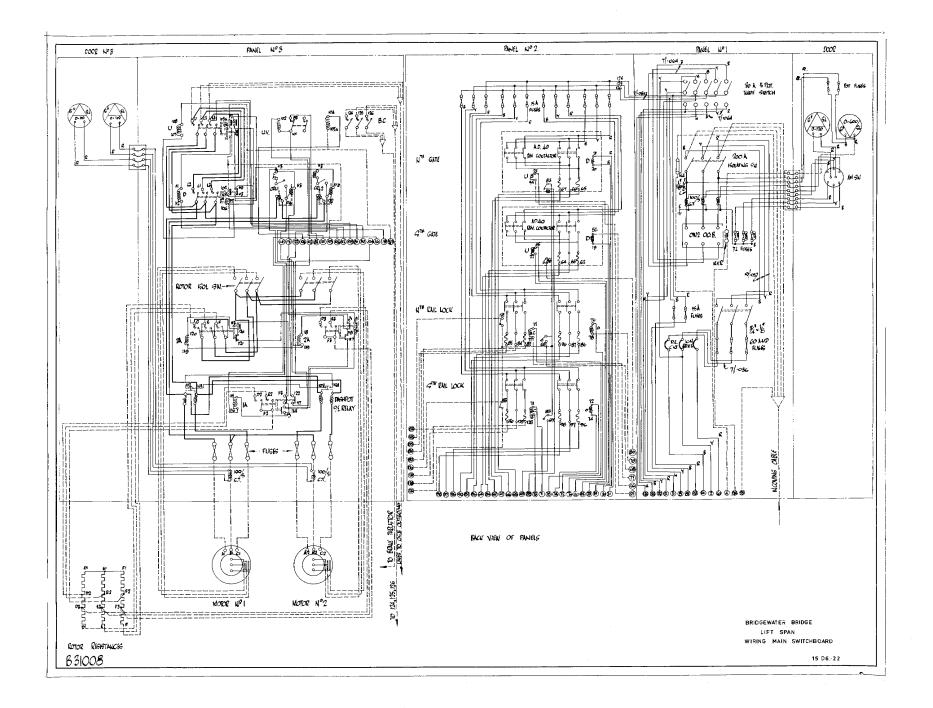


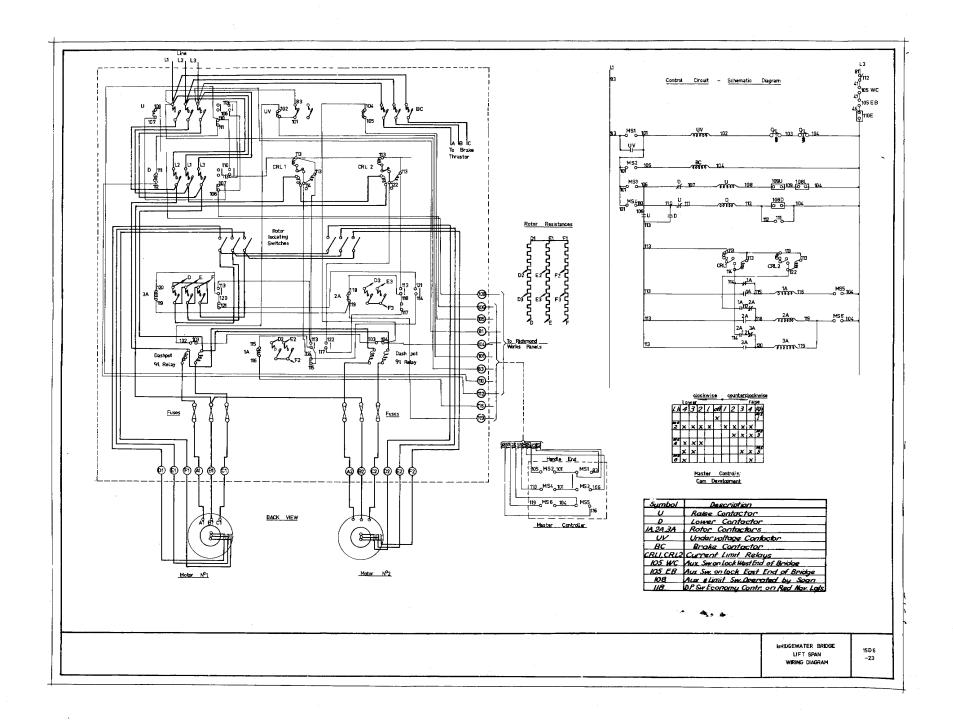


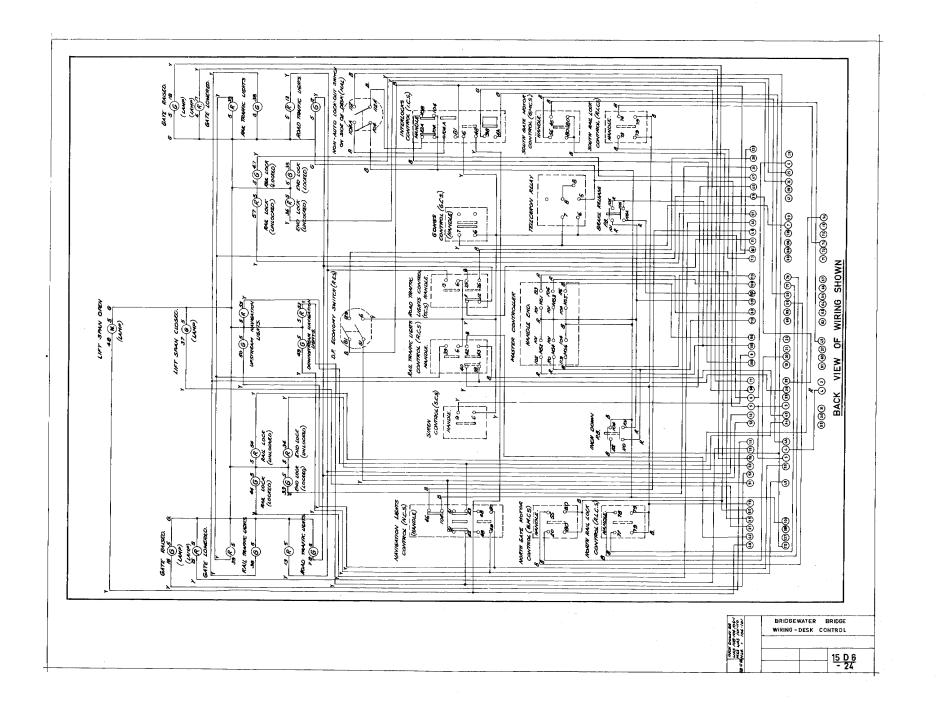


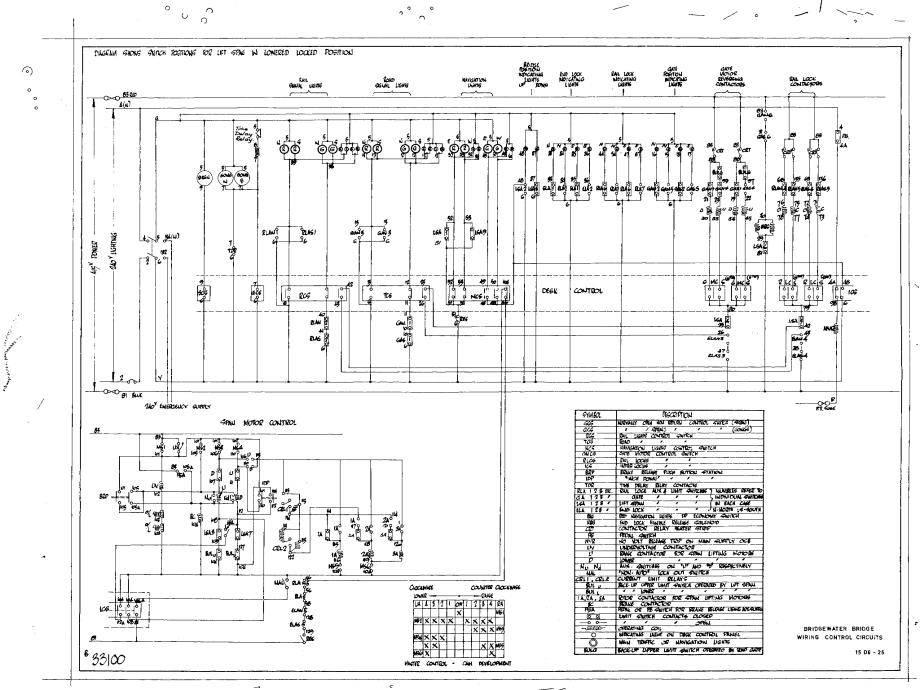












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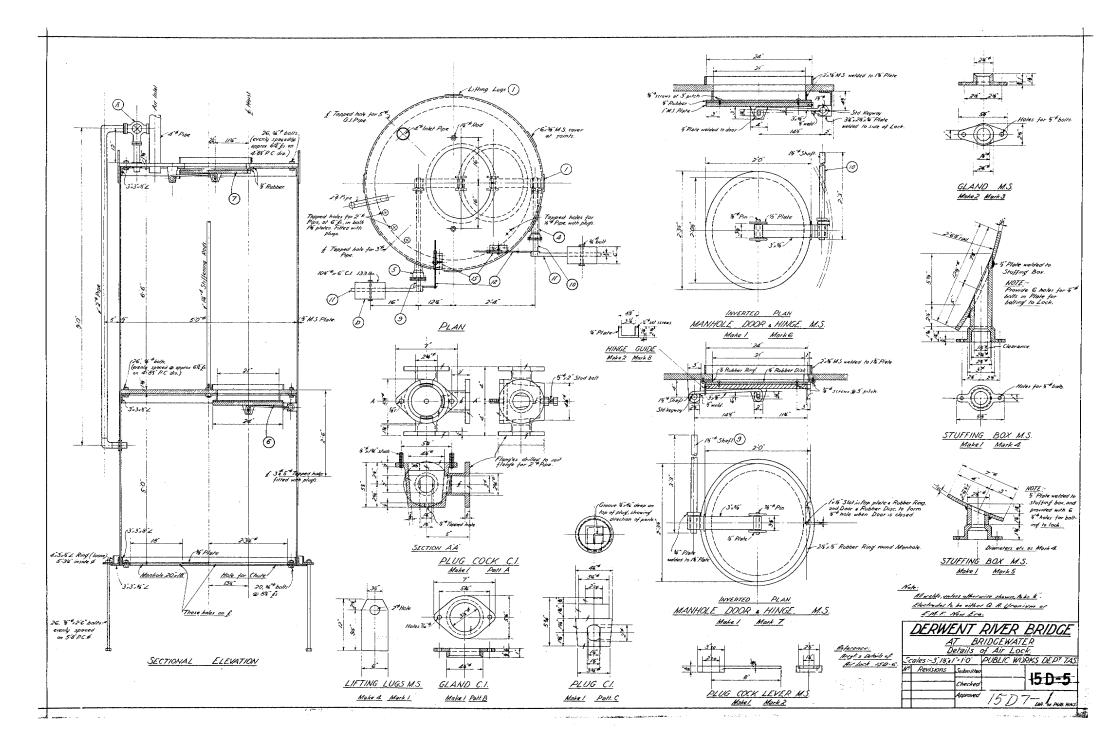
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3	D7-02	AIR LOCK ARRANGEMENT		
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	D7-16	FALSEWORK FOR TRUSSES		
	D7-16A	FALSEWORK ON PUNTS FOR	TRUSSES	
7	D7-17	CONCRETE BOTTOM DUMP BUCKET		
8	D7-18	GANTRY CRANE		
9	D7-19	GANTRY CRANE		
10	D7-20	GANTRY CRANE RAILWAY WHEELS		
11	D7-21	CRANE TRUCK		
12	D7-22	GANTRY CRANE BRAKING		
	D7-23	TIMBER PILE DRIVING FRAME		
13	D7-24	GANTRY HAULAGE WINCH		
	D7-25	GANTRY HAULAGE WINCH PULL	UP GROOVE	
	D7-26	LADDER, STEEL PIPE JOINT	FIELD AND MISCELLANEOUS	DRAWINGS
	D7-27	MULTIPLE WEIGHTS FOR	COUNTERPOISE	
	D7-28	NAVIGATION AND SYPHON SPAN	RIVER BED CROSS SECTION	1
	D7-29	NEW BAILWAY STATION LAY OUT	(SEE F.P.117)	
14	D7-30	MACHINERY HOUSE	ľ ,	
15	D7-31	TOWERS SHEAVE ERECTION		

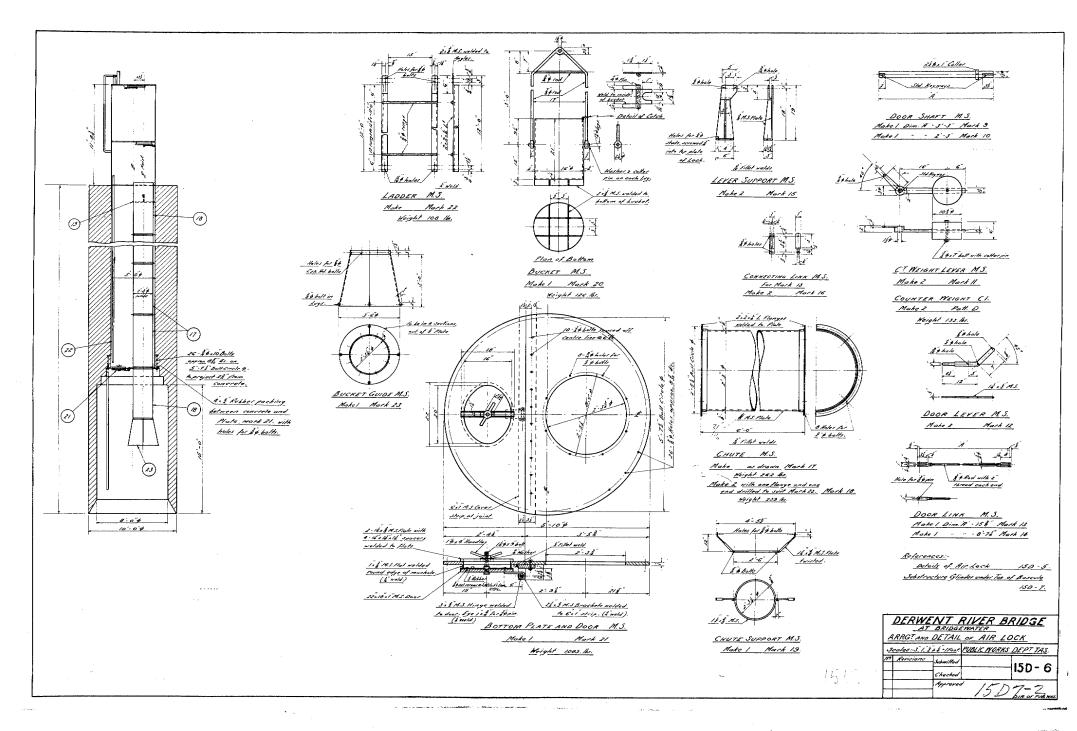
	Name2	Name3	Plan No	DrawingNo	Name1	Name2	Name3
			16	D7-31A	TOWERS SHEAVE ERECTION		
			17	D7-32	SOUTHERN ABUTMENT SETTLE-	MENT	
				D7-33A	OBSERVED SUBSTRUCTURE	LEVELS	
			19	D7-33B	OBSERVED SUBSTRUCTURE	LEVELS	
	VENTILATORS		20	D7-33B1	1986 OBSERVED SUBSTRUCTURE	LEVELS	
T			21	D7-33C	LEVELS ON PIN M		
			22	D7-33D	SOUTHERN ABUTMENT LEVELS	ON PINS H AND M (1986)	
	LAYOUT		23	D7-34	FENDERING RENEWAL	ARRANGEMENT (1981)	
	PILE RAILWAY LONGITUDINAL	SECTION	24	D7-35	PIERS AND PYLON	× /	
				D7-36	STEELWORK		
				D7-37	TRESTLE COMPONENTS (1987)		
	CLOSET		27	D7-38	MONORAIL AND BEAM		
				D7-39	MONORAIL AND TRESTLE	ASSEMBLY	
			29.30	D7-40	PIERS AND ABUTMENTS LEVELS	(1988)	
			31	D7-41	SOUTHERN ABUTMENT LEVELS	(1988)	
	OUT OF ERECTION BAY			D7-42	PIERS AND ABUTMENT LEVELS	(1988)	
			33	D7-43	PIER NO 1 LEVELS		
_	TRUSSES		34	D7-44	HEIGHT GANTRY ASSEMBLY	(1990)	
Т			35	D7-45	HEIGHT GANTRY (1990)		
				D7-46	NORTHERN HEIGHT GANTRY	ASSEMBLY (1990II)	
			37	D7-47	GENERAL ARRANGEMENT OF	SOUTHERN END RAISING	(1991)
:				D7-48	SECTIONS		
				D7-49	FENCES AND RETAINING WALLS		
				D7-50	ABUTMENT ALTERATIONS AND	JACKING SEQUENCE	
			41	D7-51	BEARINGS AND STEELWORK		
			42	D7-52	POLYSTYRENE FILL		
_	UP GROOVE		43	D7-53	TEMPORARY ROAD SIGNS		
	FIELD AND MISCELLANEOUS	DRAWINGS	44	D7-54	Auxiliary Power	Engine Bed,Alternator Drive	
_	COUNTERPOISE			D7-55	Rail Locking Bar	& Slop Mechanism	Hydraulic Conversion
-	RIVER BED CROSS SECTION		46		Rail Locking Bar	& Stop Mechanism	Hydraulic Circuit Deta
	(SEE F.P.117)				Rail Locking Bar	& Slop Mechanism	Details
			48	D7-58	Rail Locking Bar	& Slop Mechanism	Details
			49		Rail Locking Bar	& Slop Mechanism	Details-Hydraulic Ta
					Additional Traffic Signals		

BRIDGEWATER BRIDGE

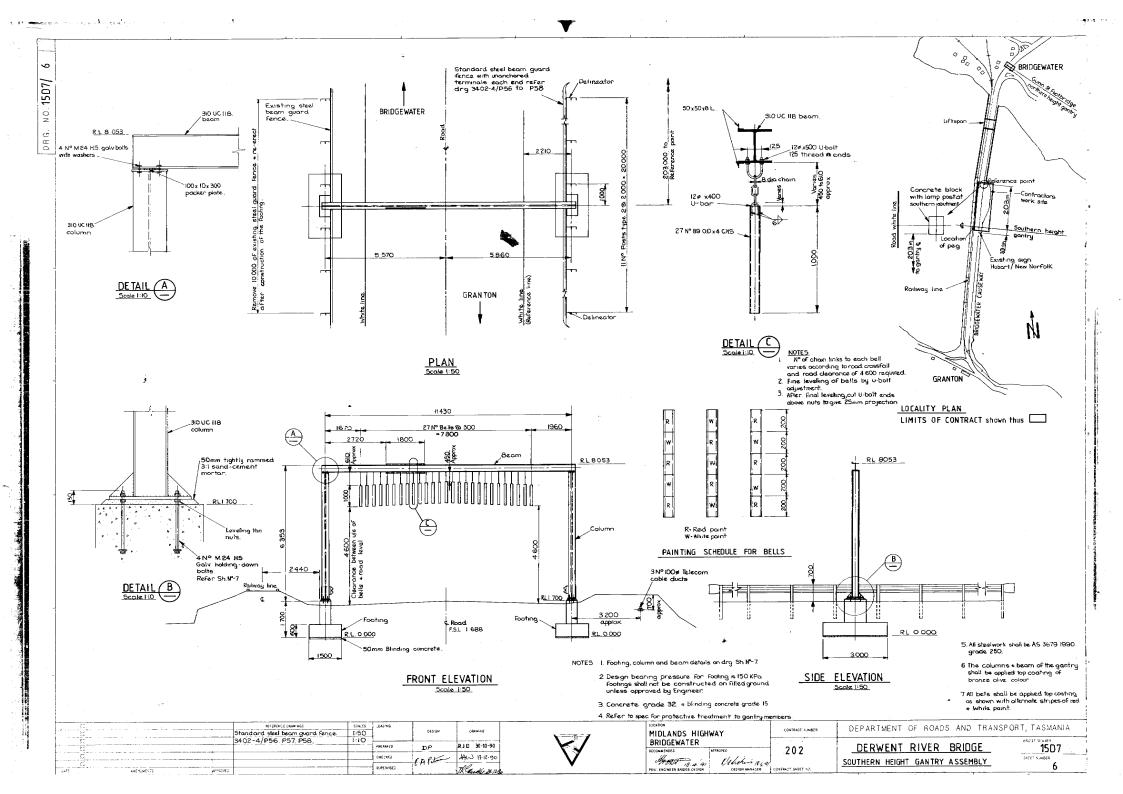
D7- MISCELLANEOUS

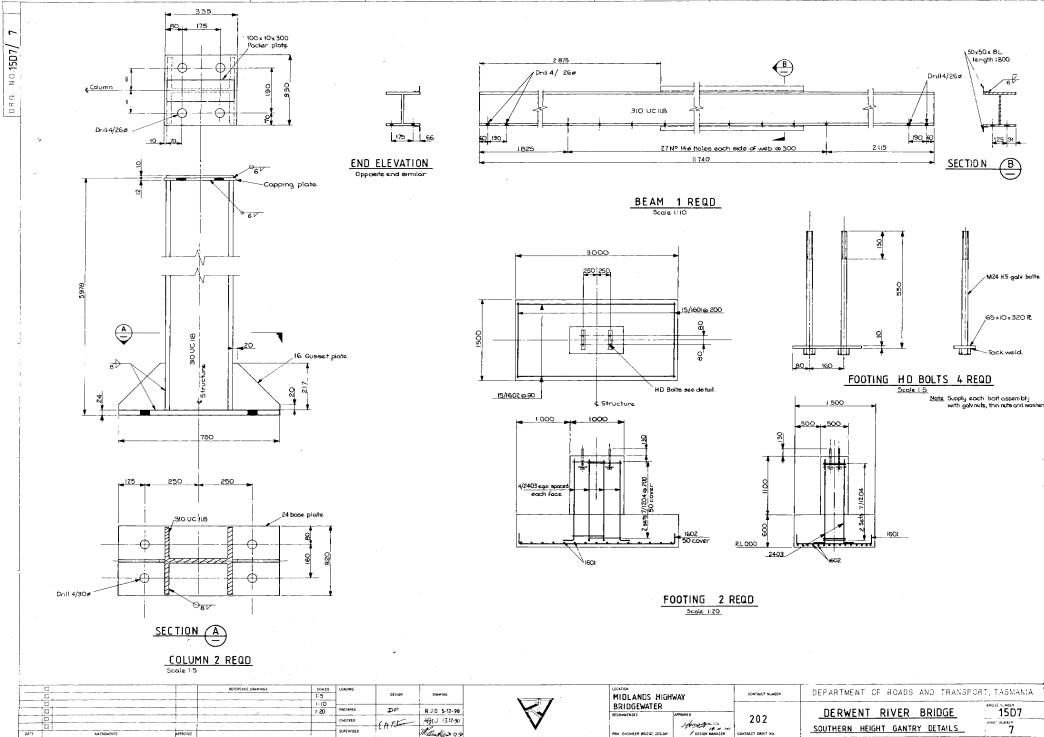
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M24 H.5 galv bolts.

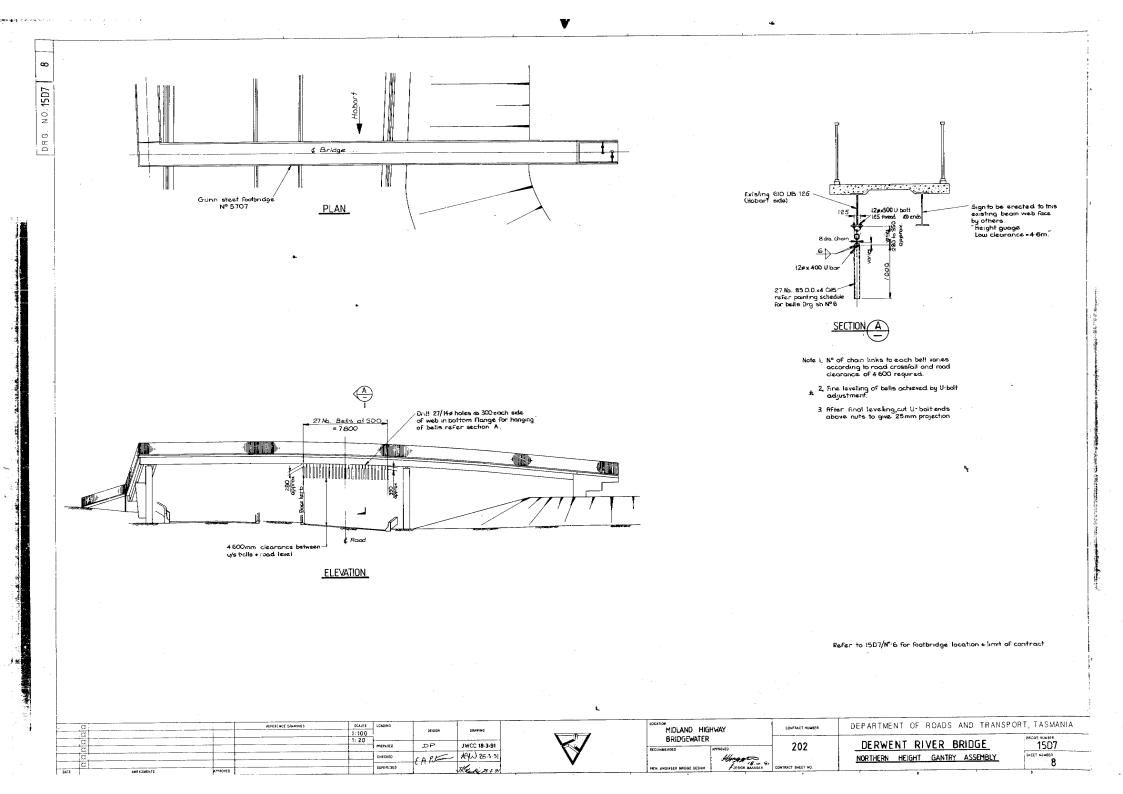
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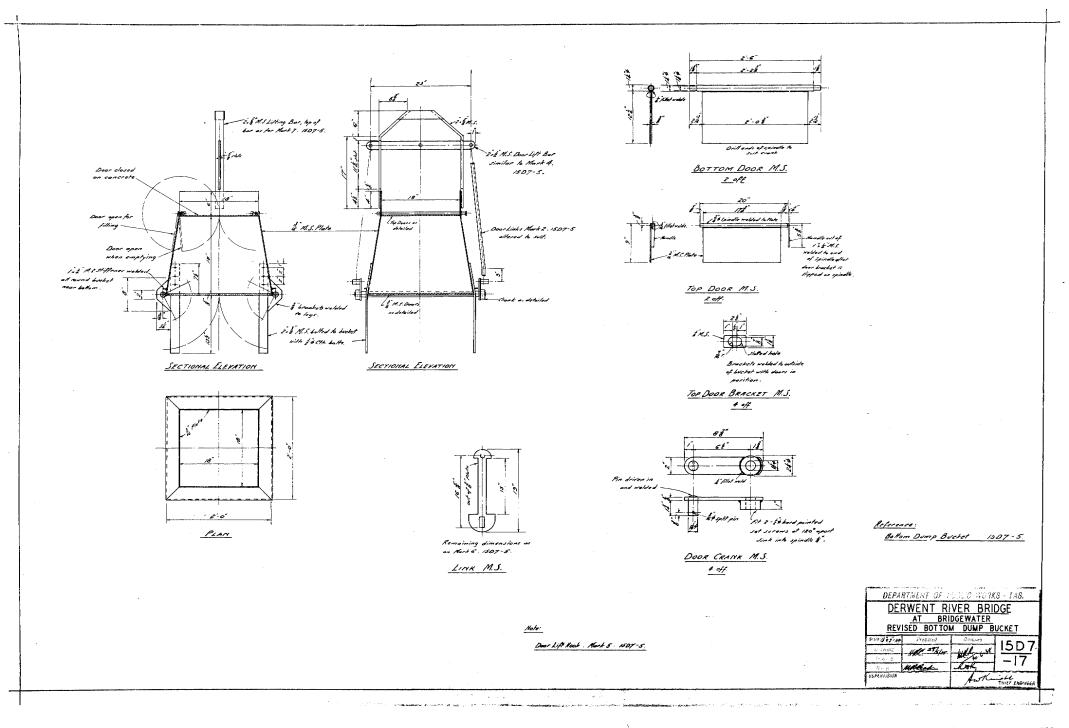
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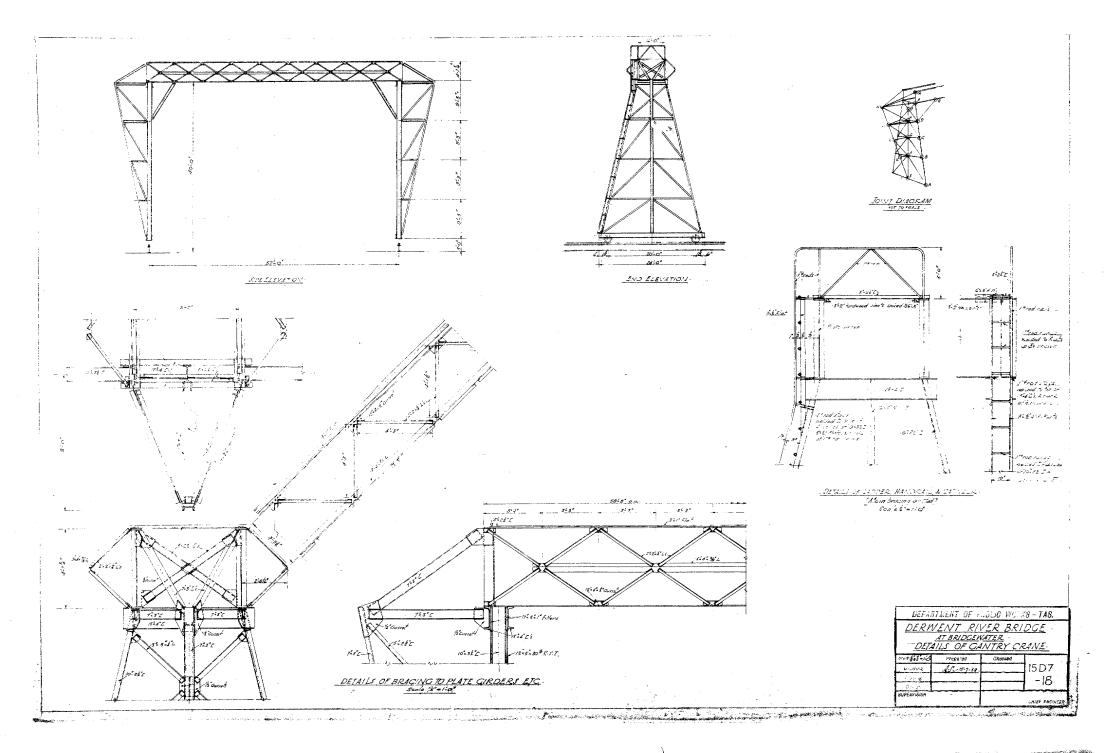
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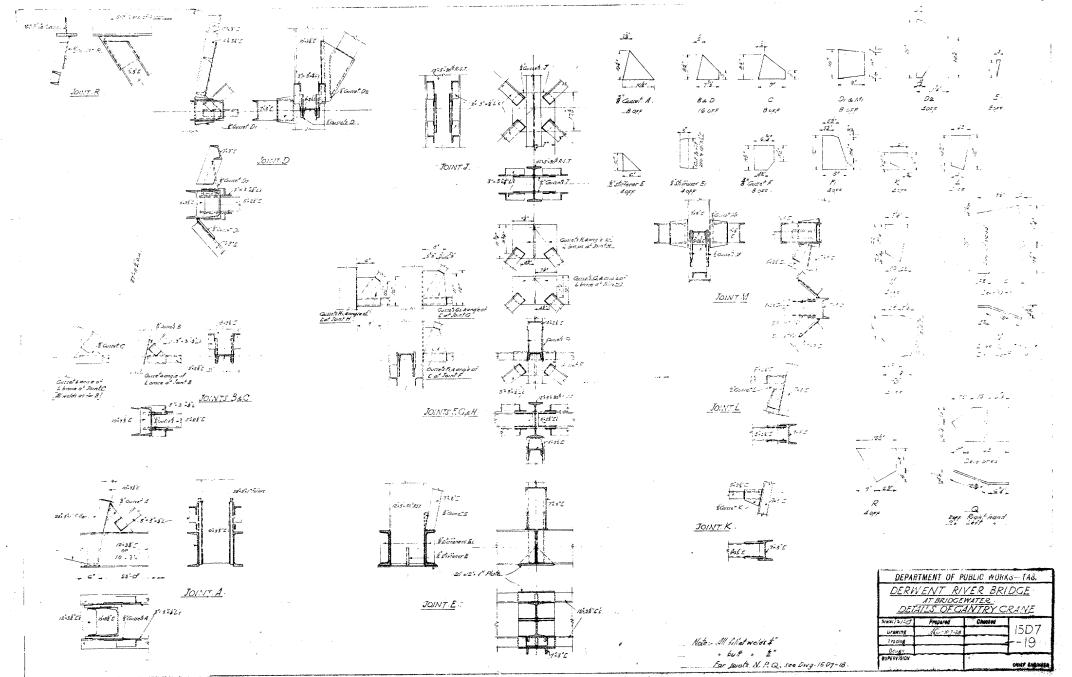
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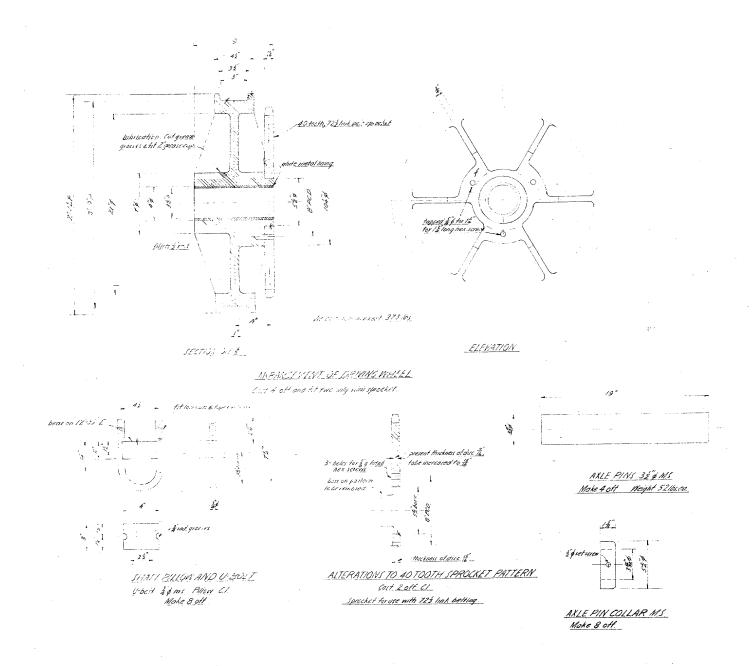


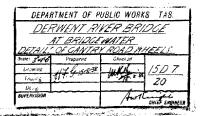


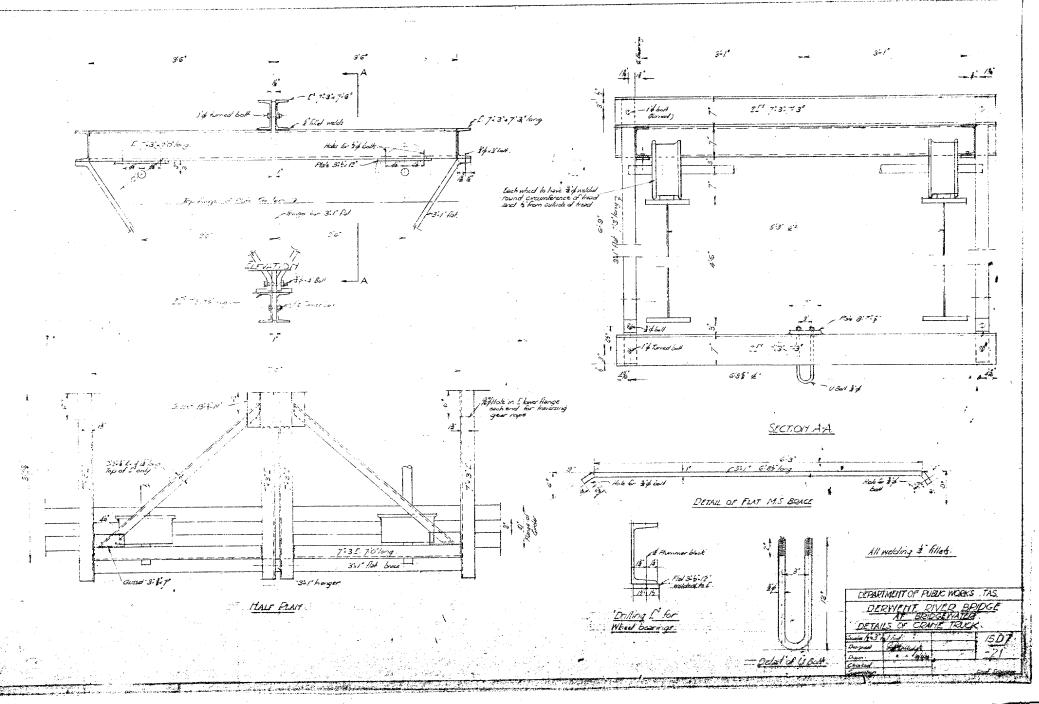


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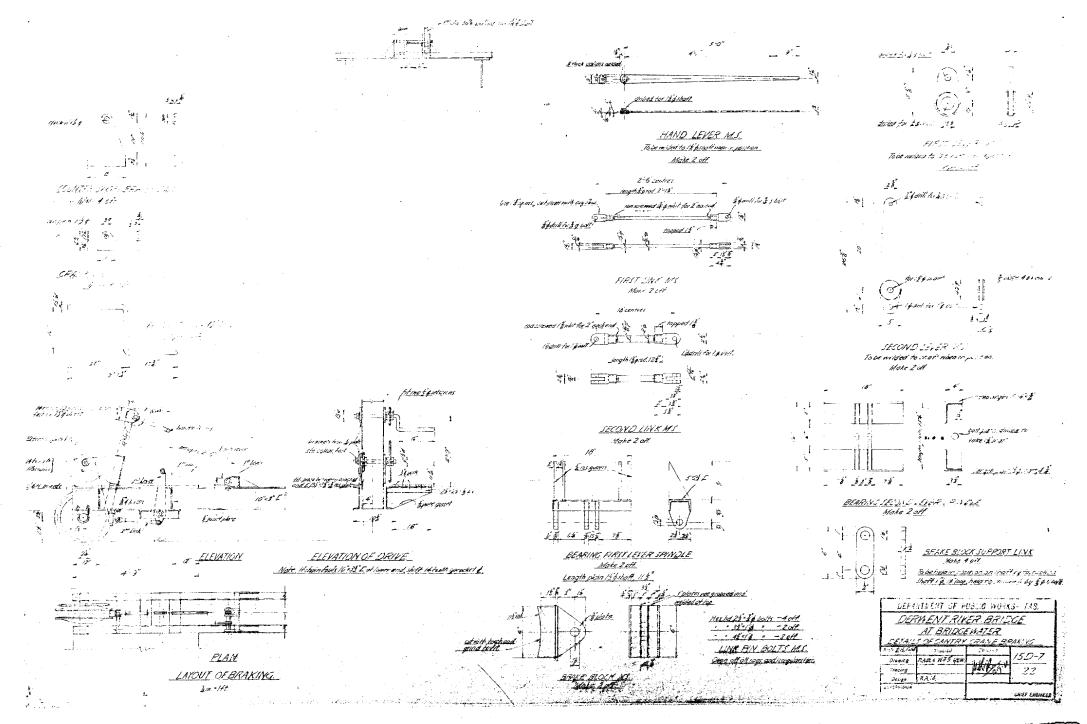
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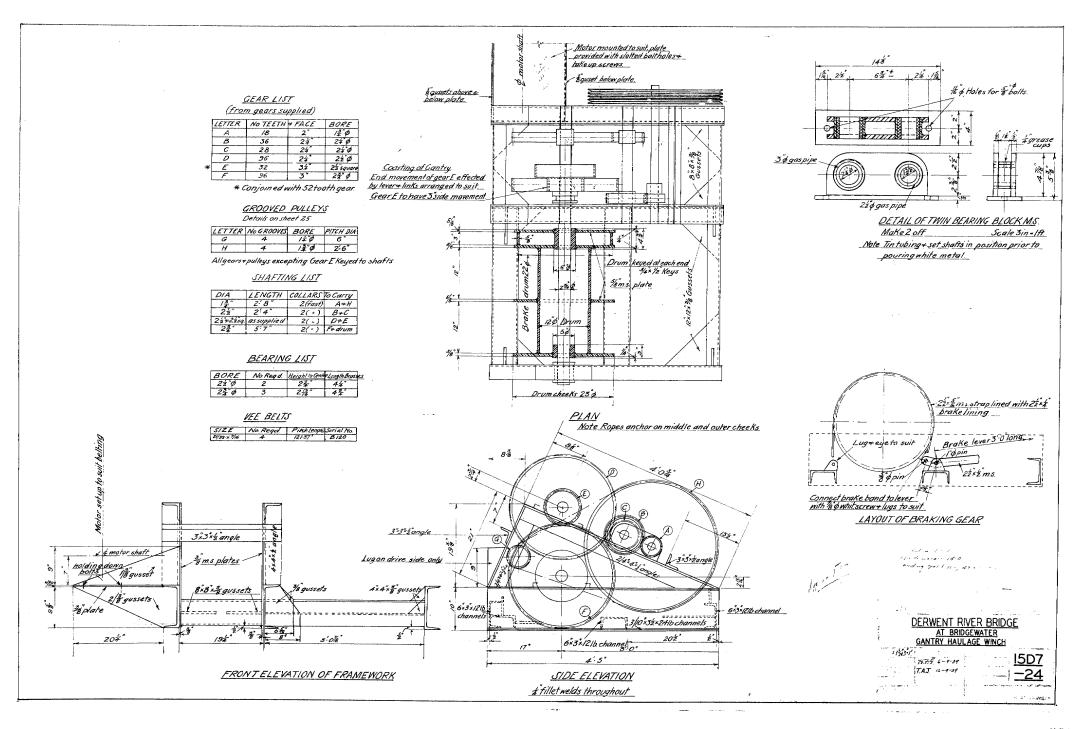




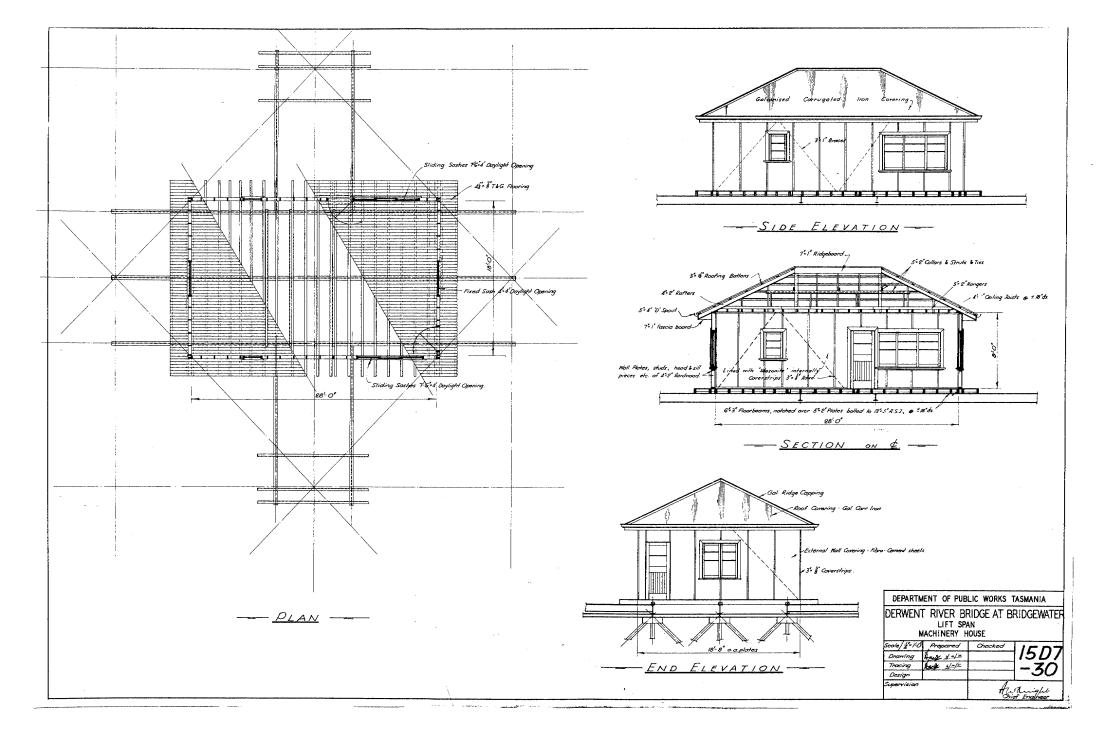


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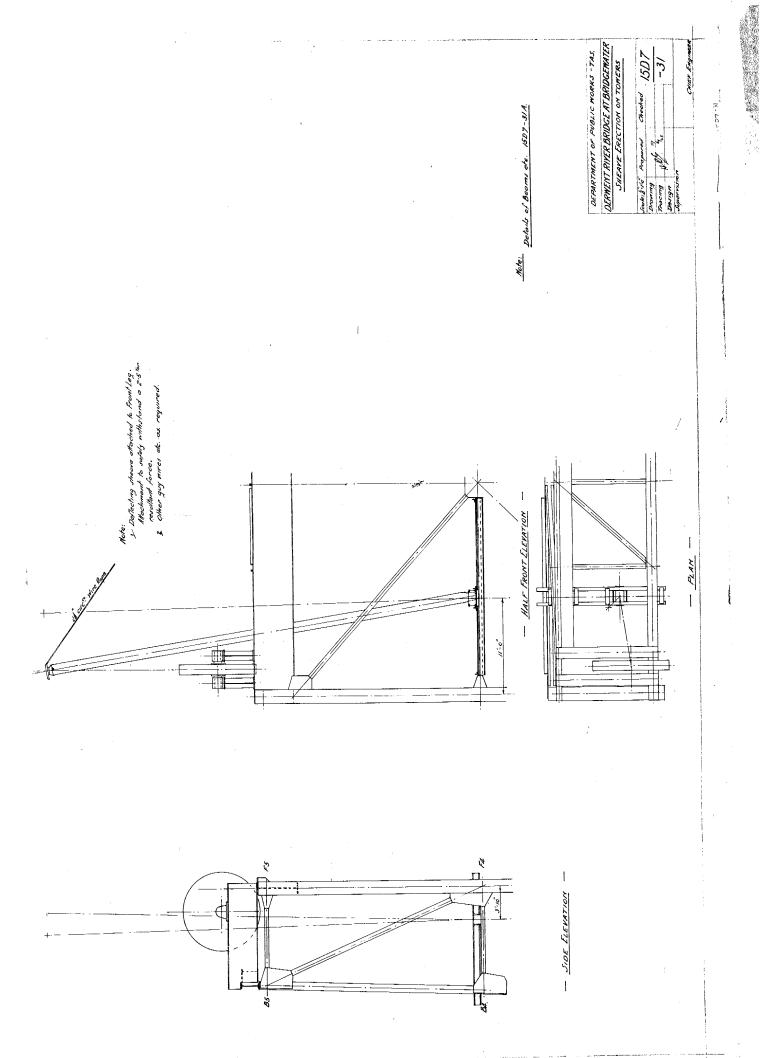


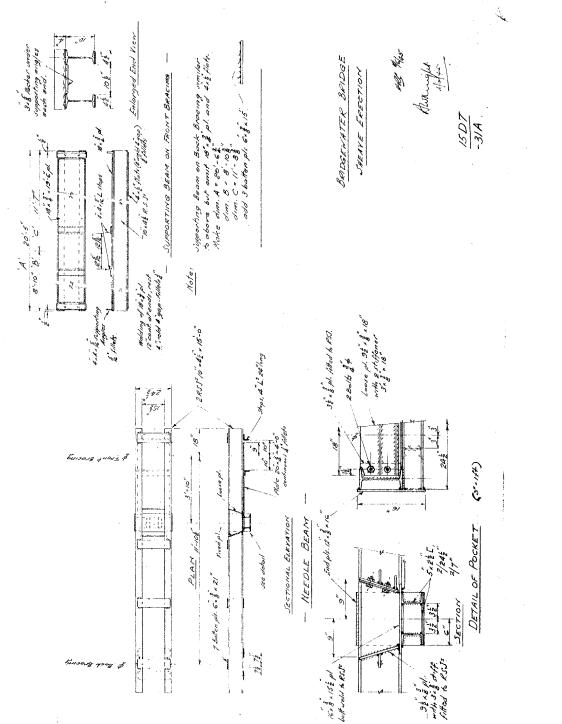


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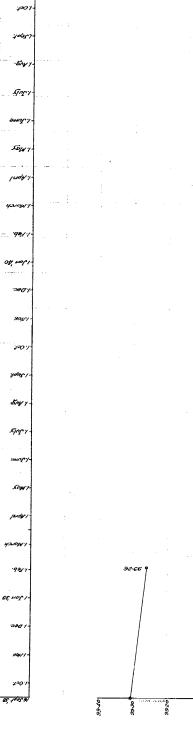
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CHIEFÉNGINEER OERMENT RIVER BRIDGE AT BRIDGENATER Prepared Checked 1507 -32 DEPARTMENT OF PUBLIC WORKS - TAS. SETTLEMENT OF SOUTH ABUTMENT as observed on N.W. seating bolt Scale: -Drawing Tracing Dasign Supervision Settle . . .

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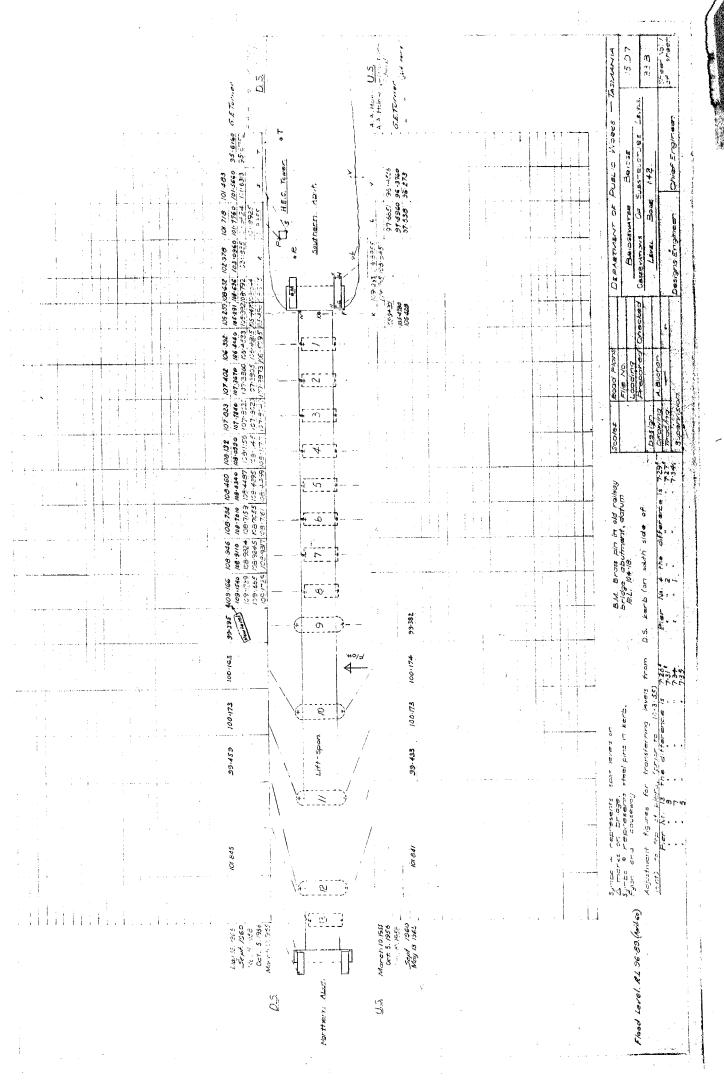
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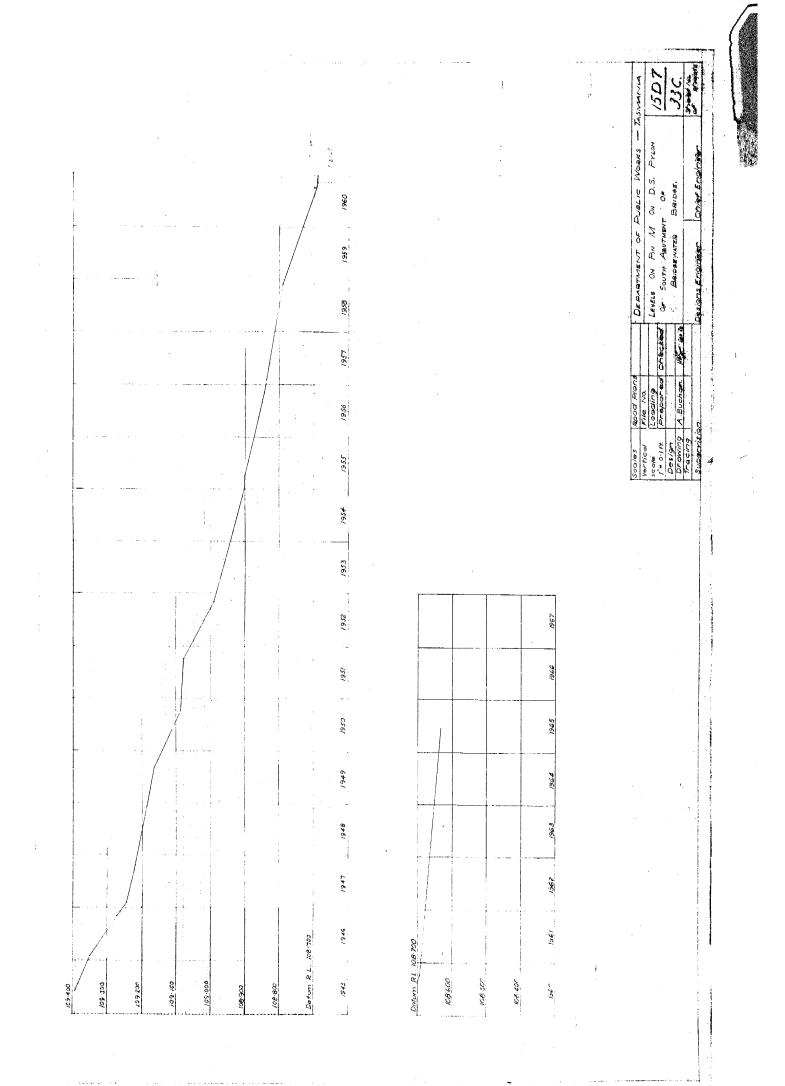
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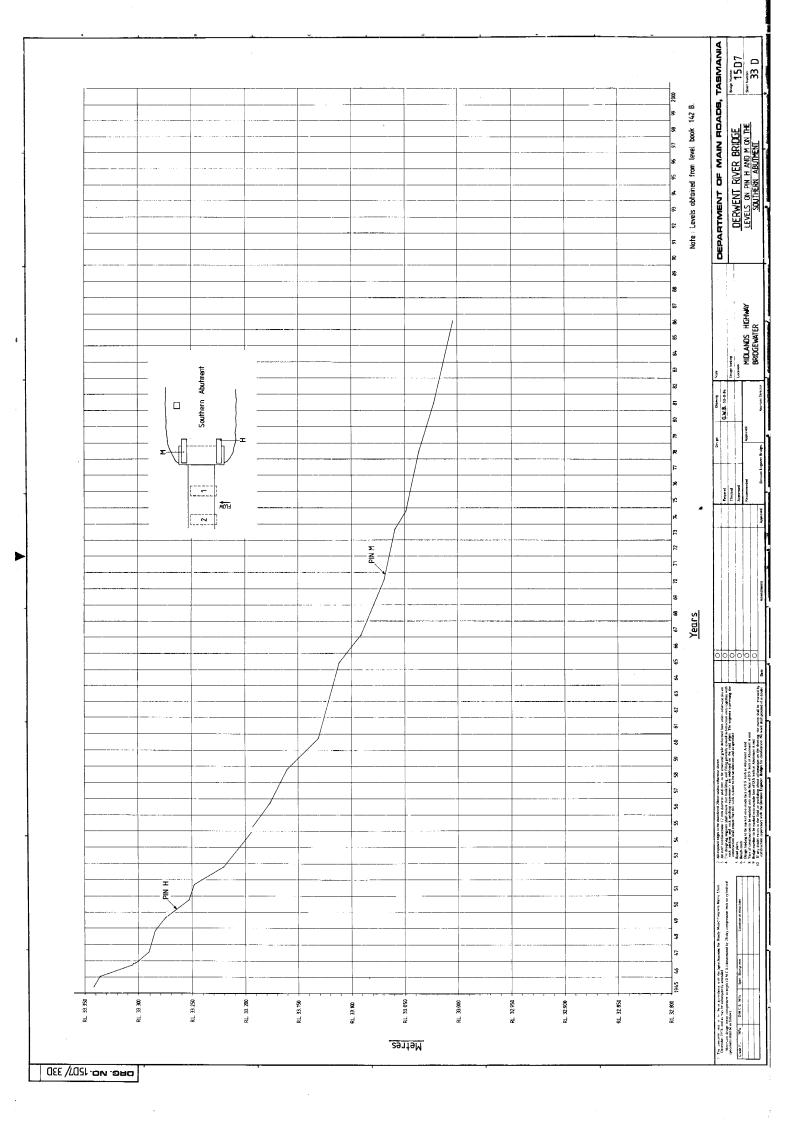
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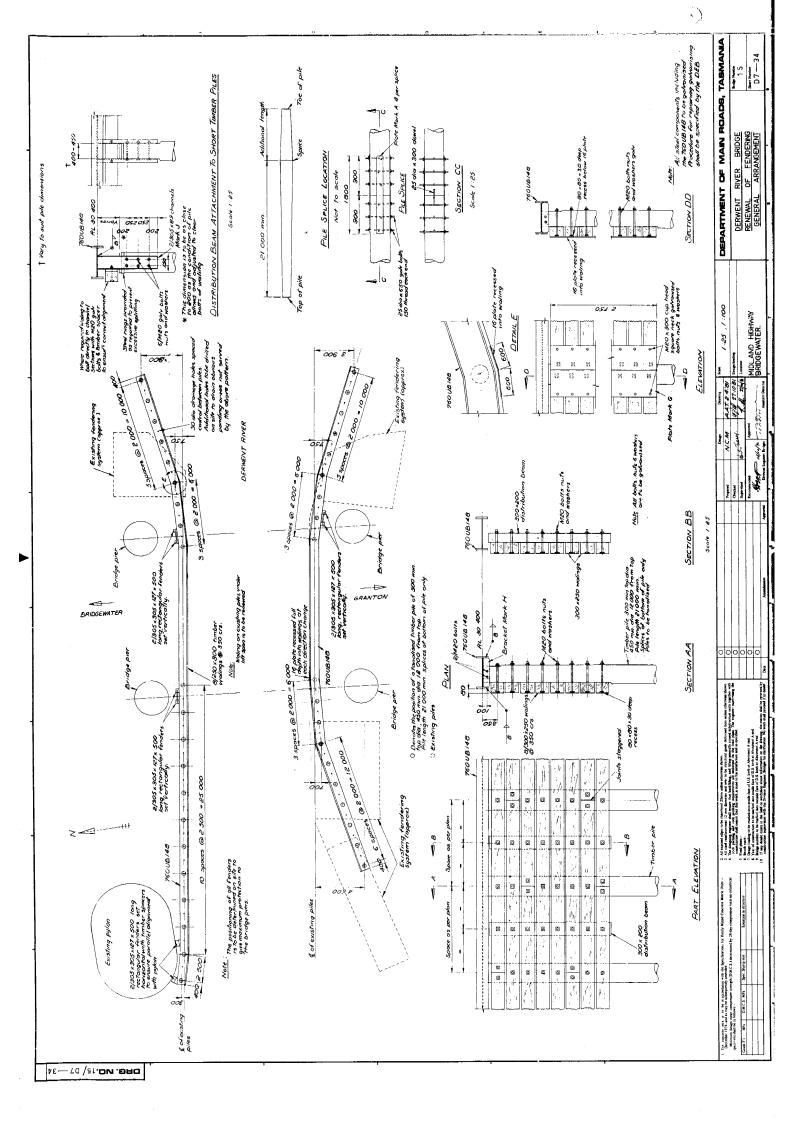
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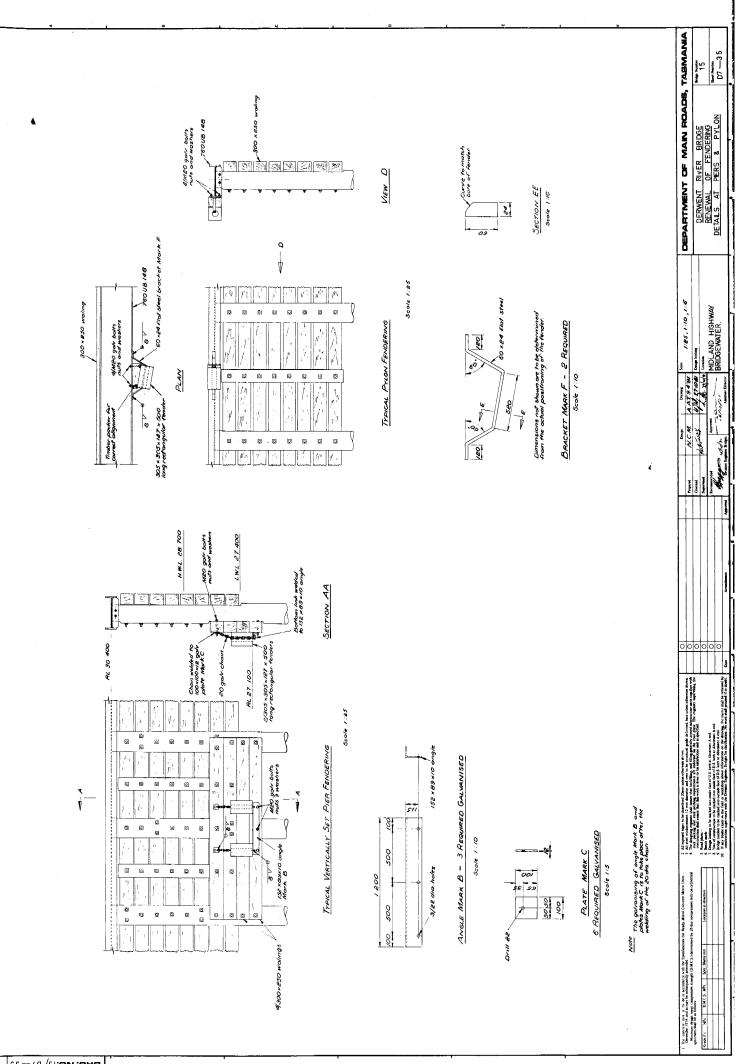
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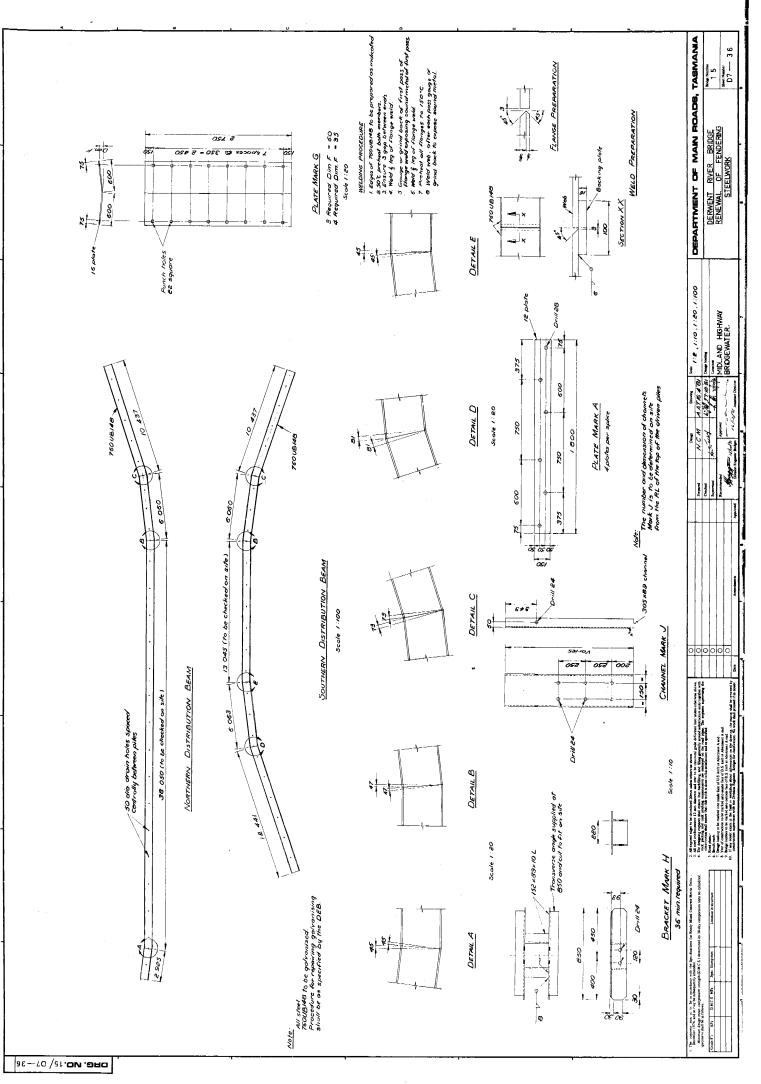




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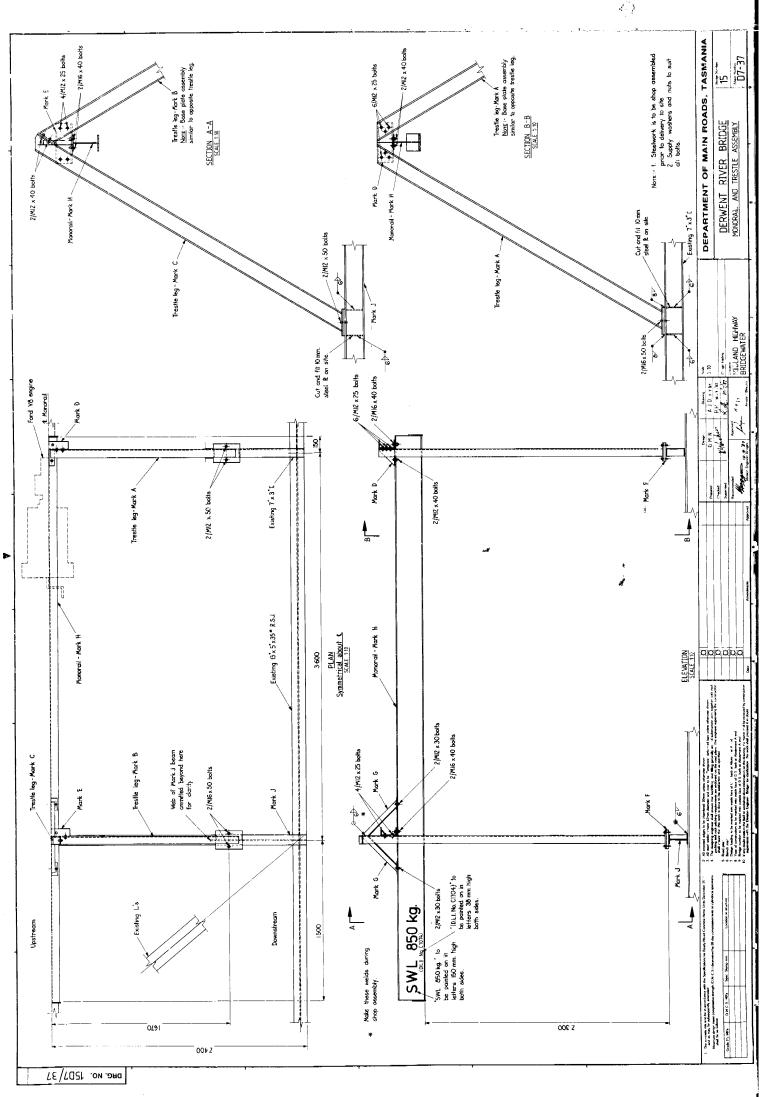
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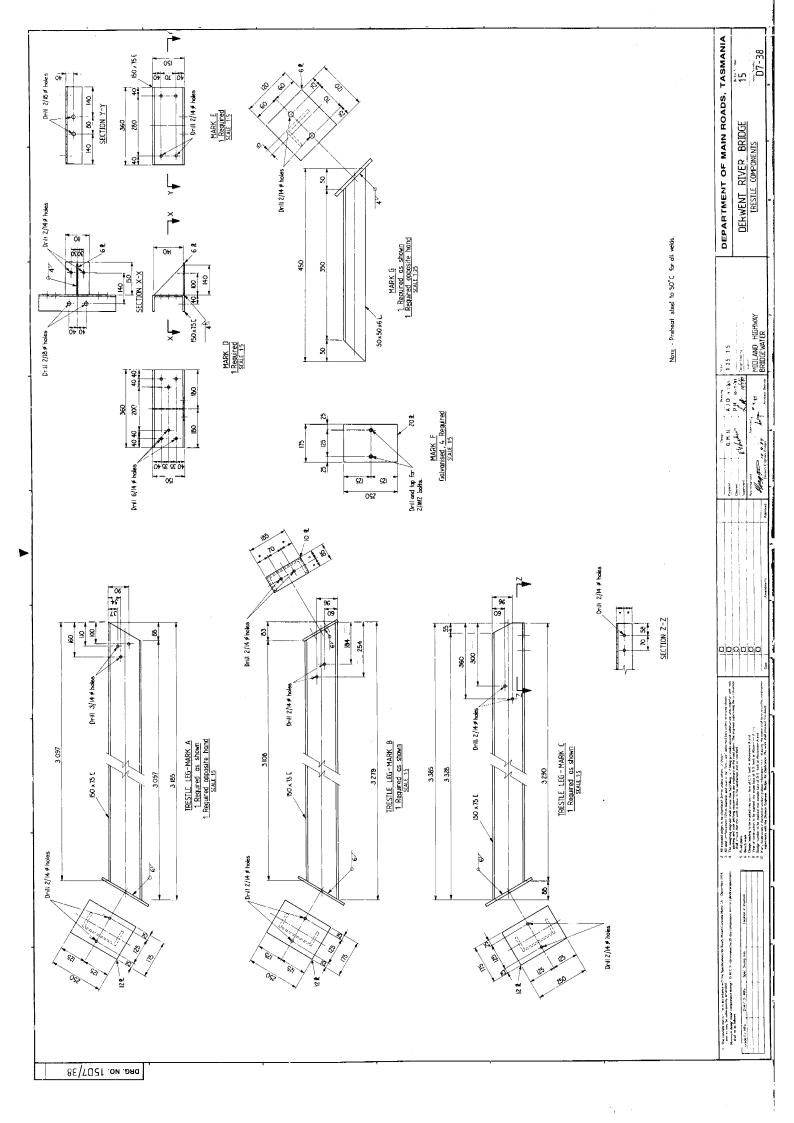
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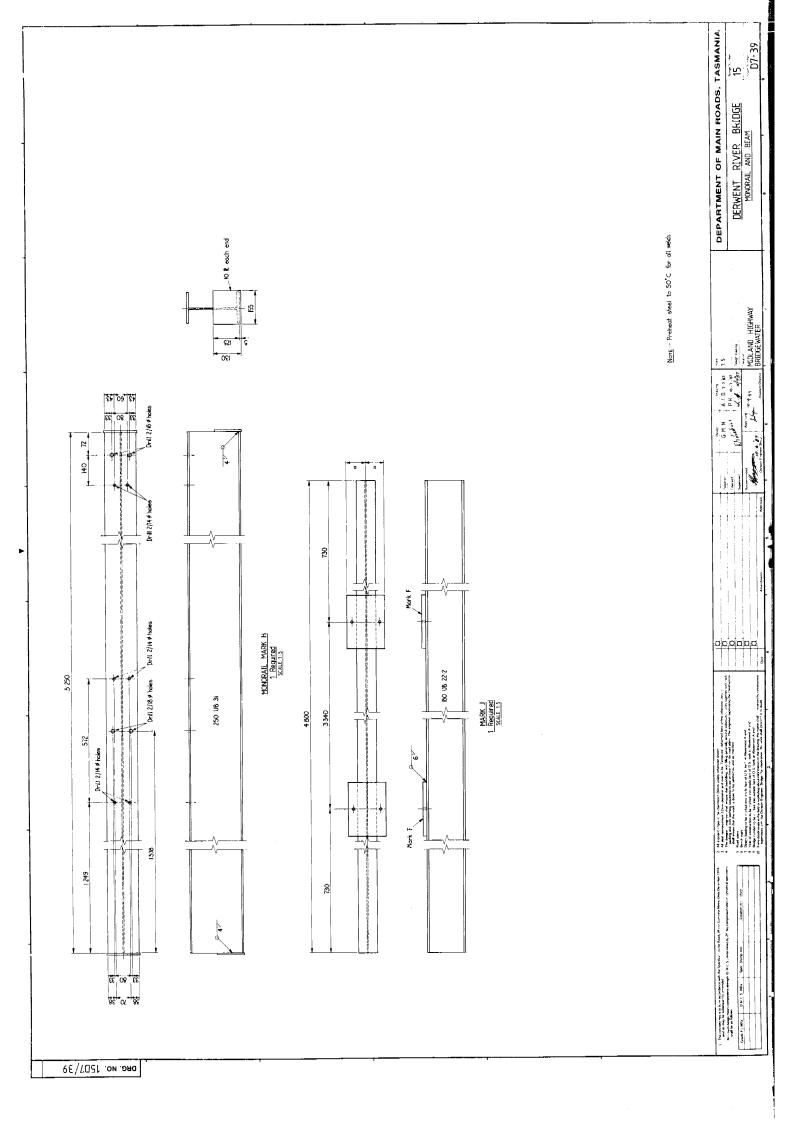
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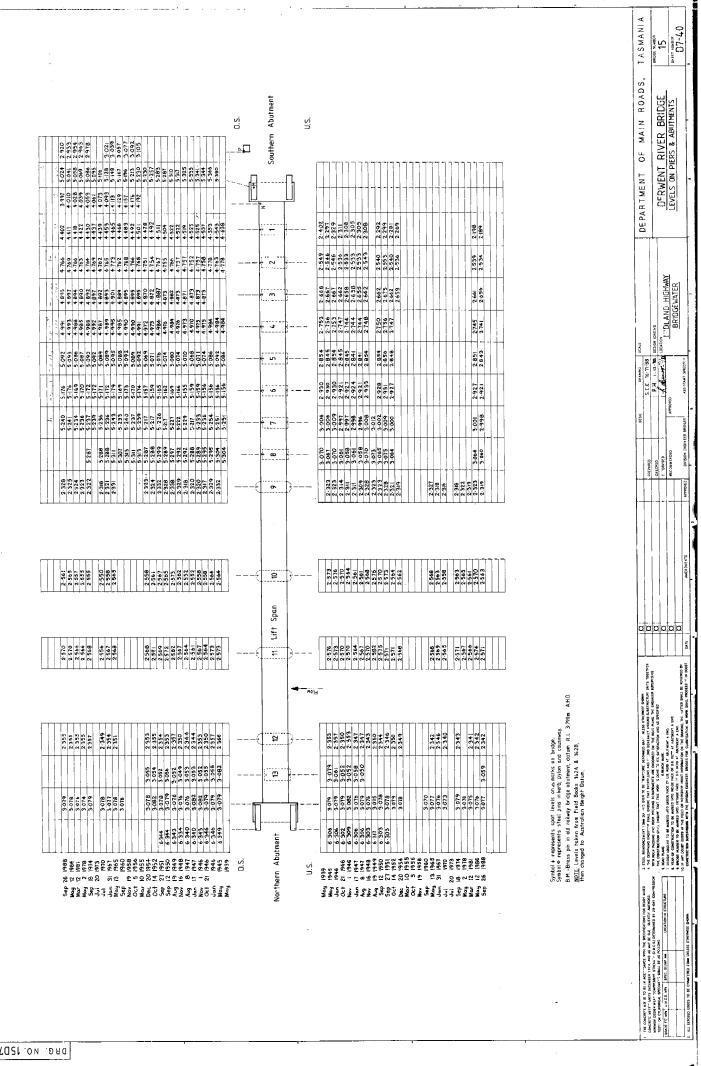


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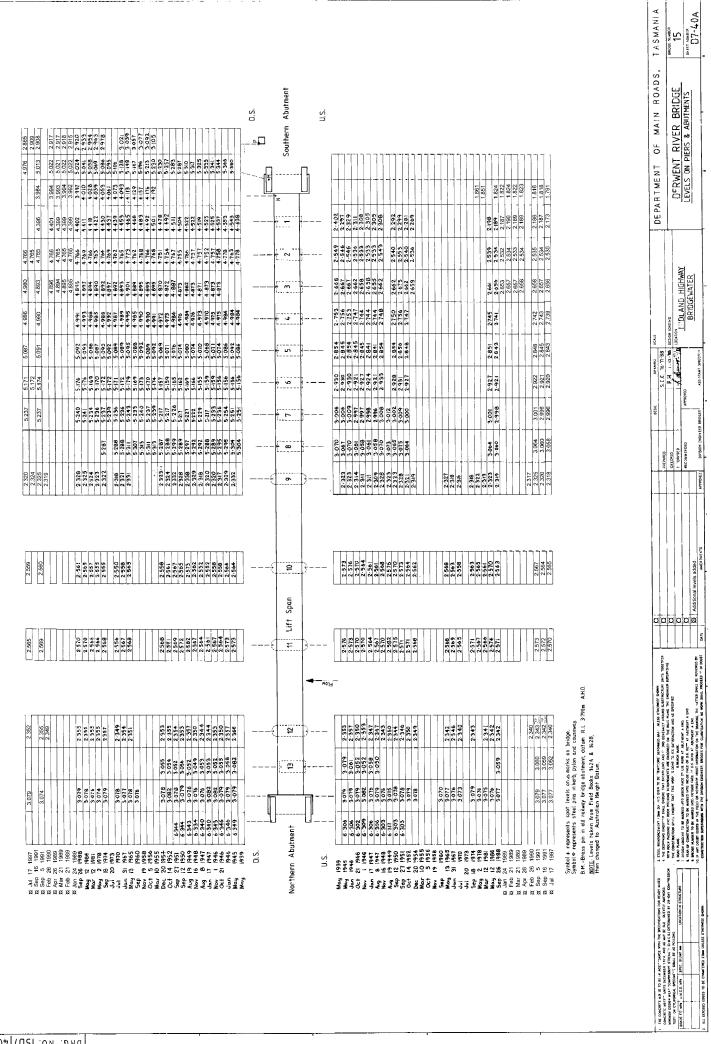




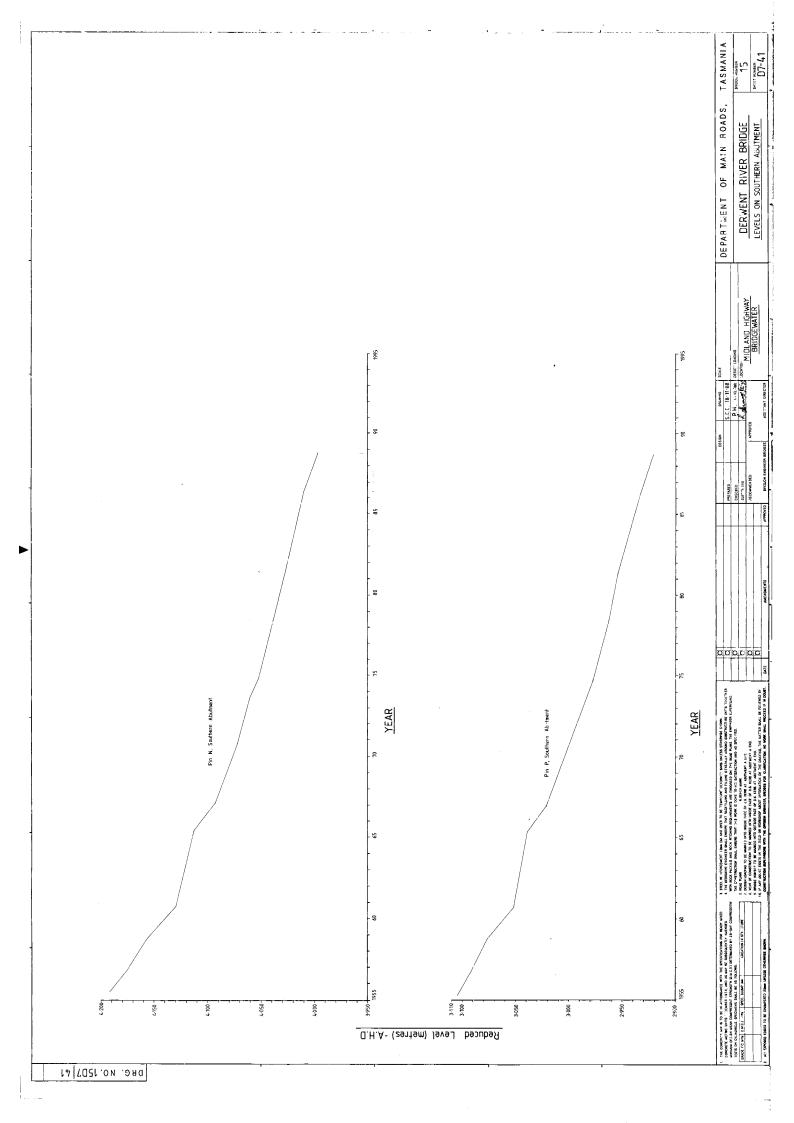


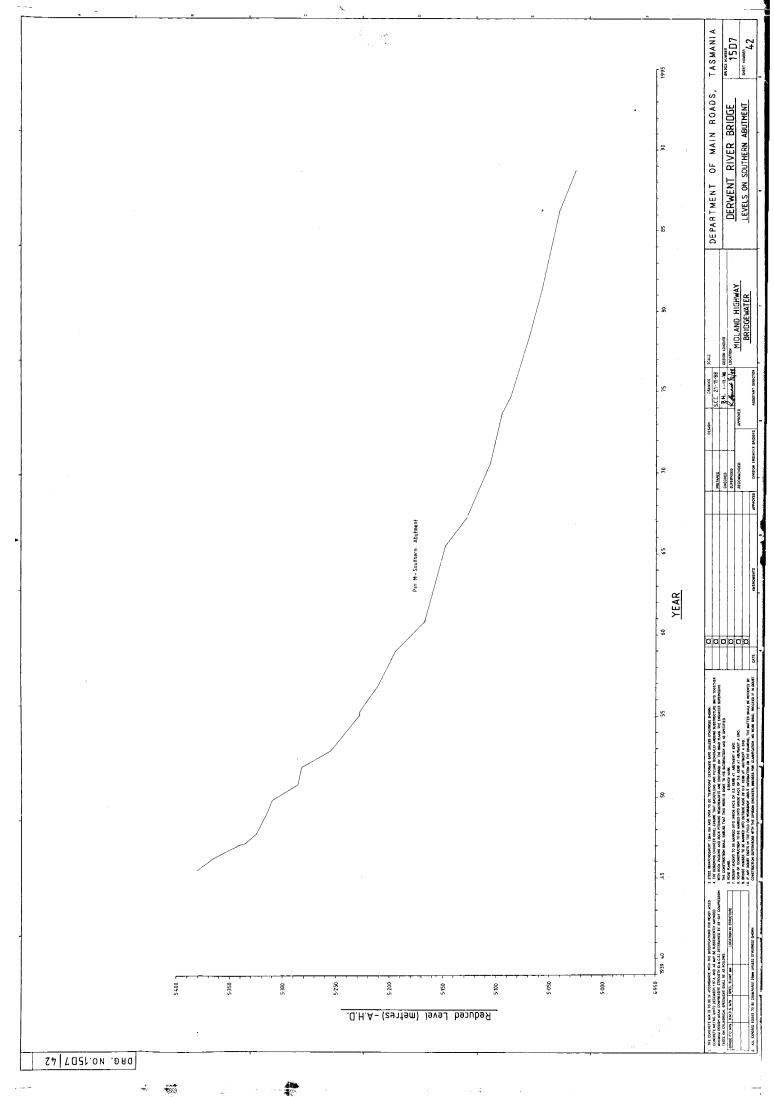
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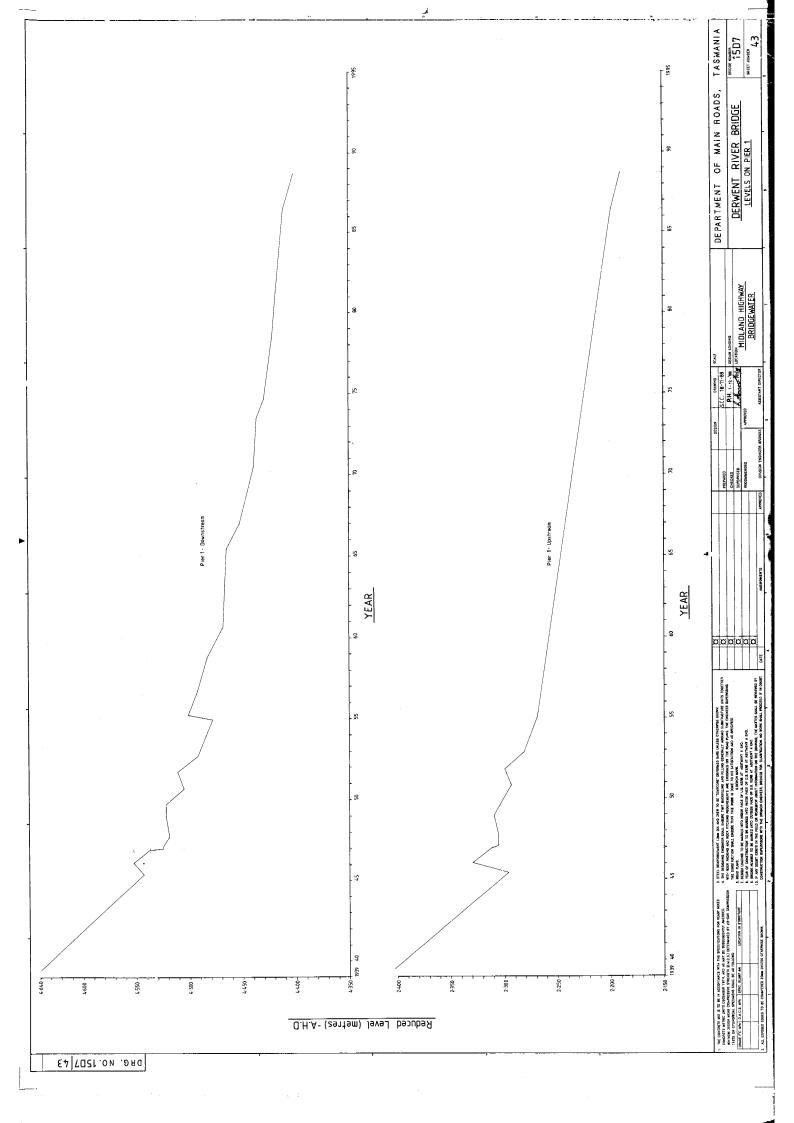
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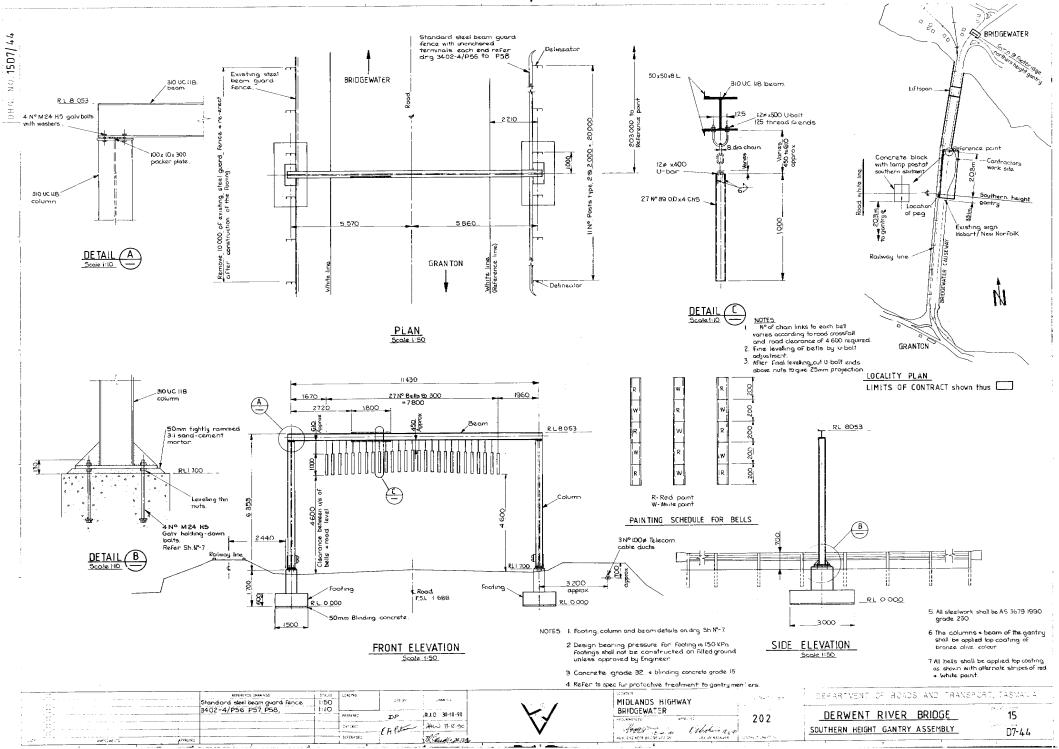


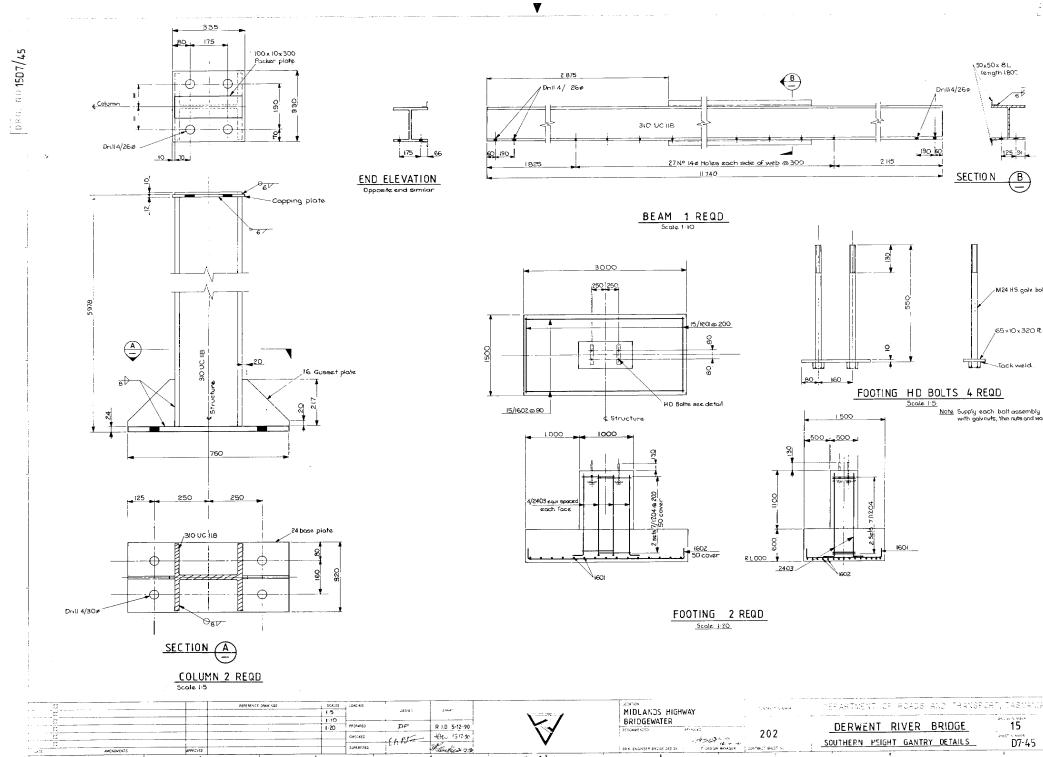
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APPROVED

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AMENDMENTS

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D7-45

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/M24 H.S. galv bolts.

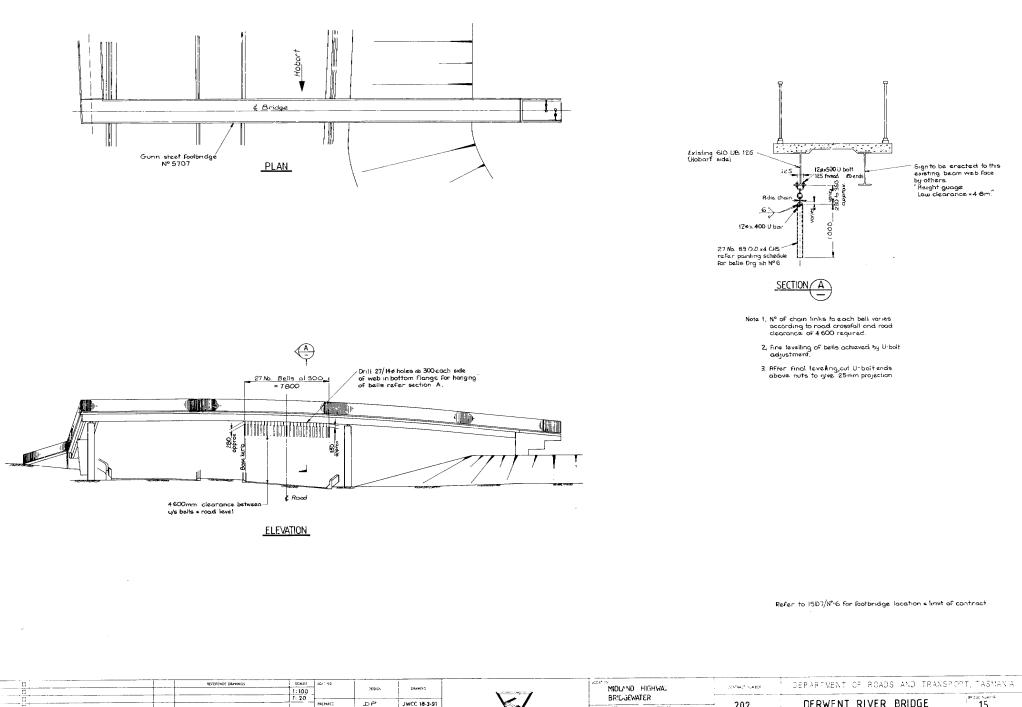
65×10×320 PL

-Tack weld

-<u>Note</u> Supply each balt assembly with galvinuts, thin nuts and washer

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DERWENT RIVER BRIDGE NORTHERN HEIGHT GANTRY ASSEMBLY

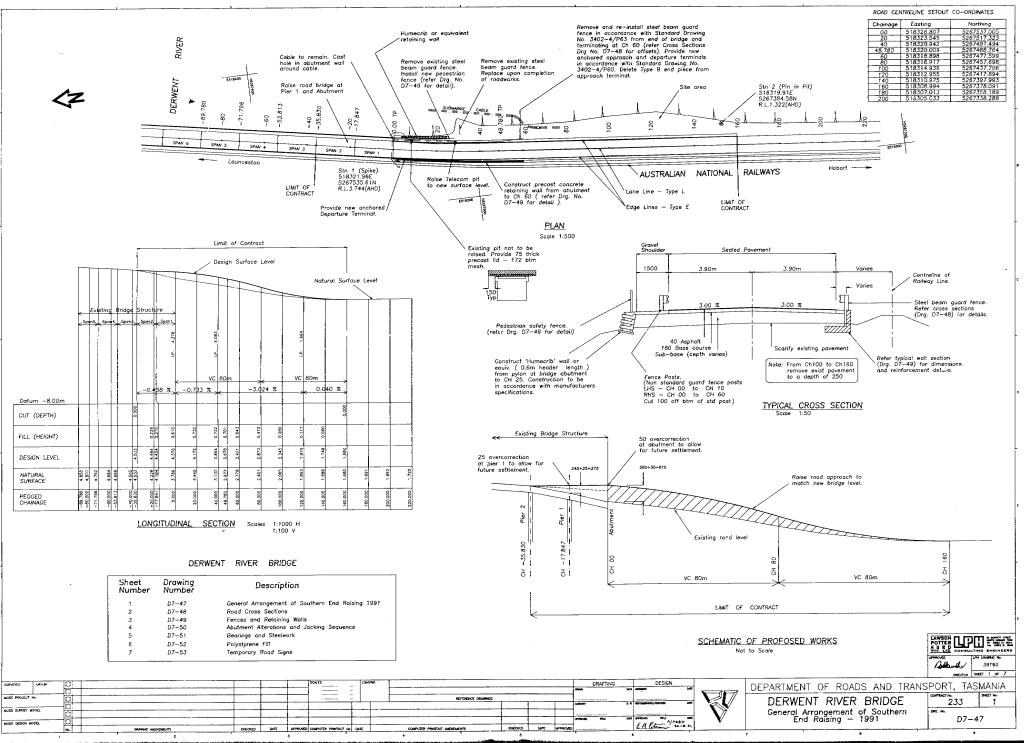


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DRG. NO. 15D7 46

AMENDMENTS

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LAWSON POTTER

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DRG. No.

39190 DIRECTOR SHEET 2 OF 7

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D7-48

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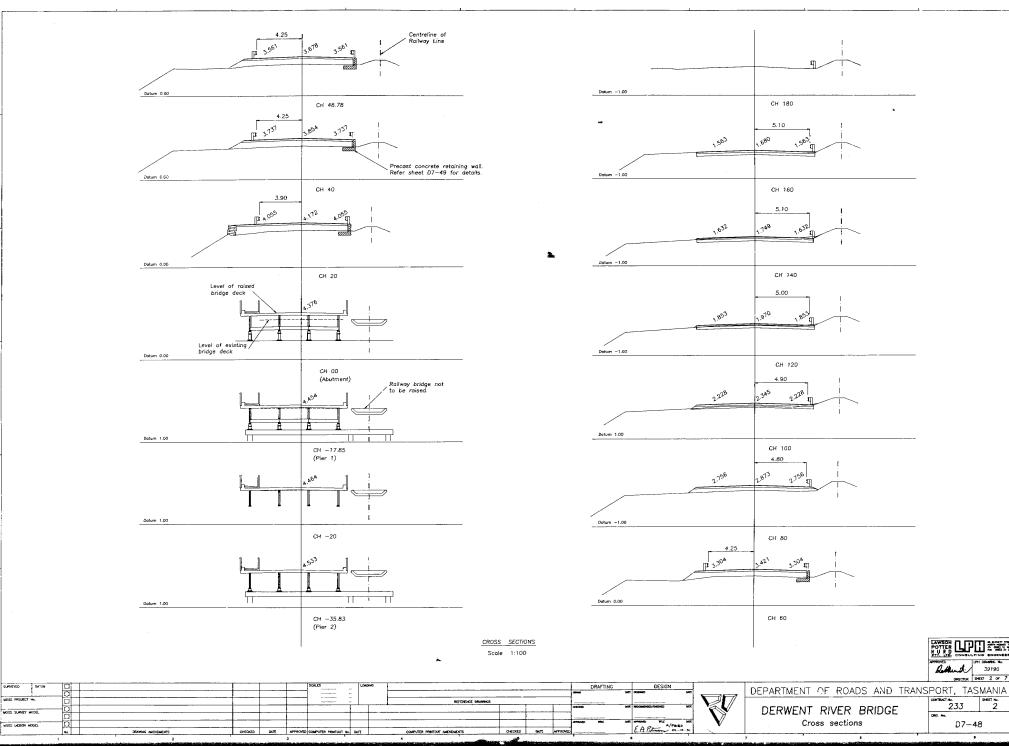
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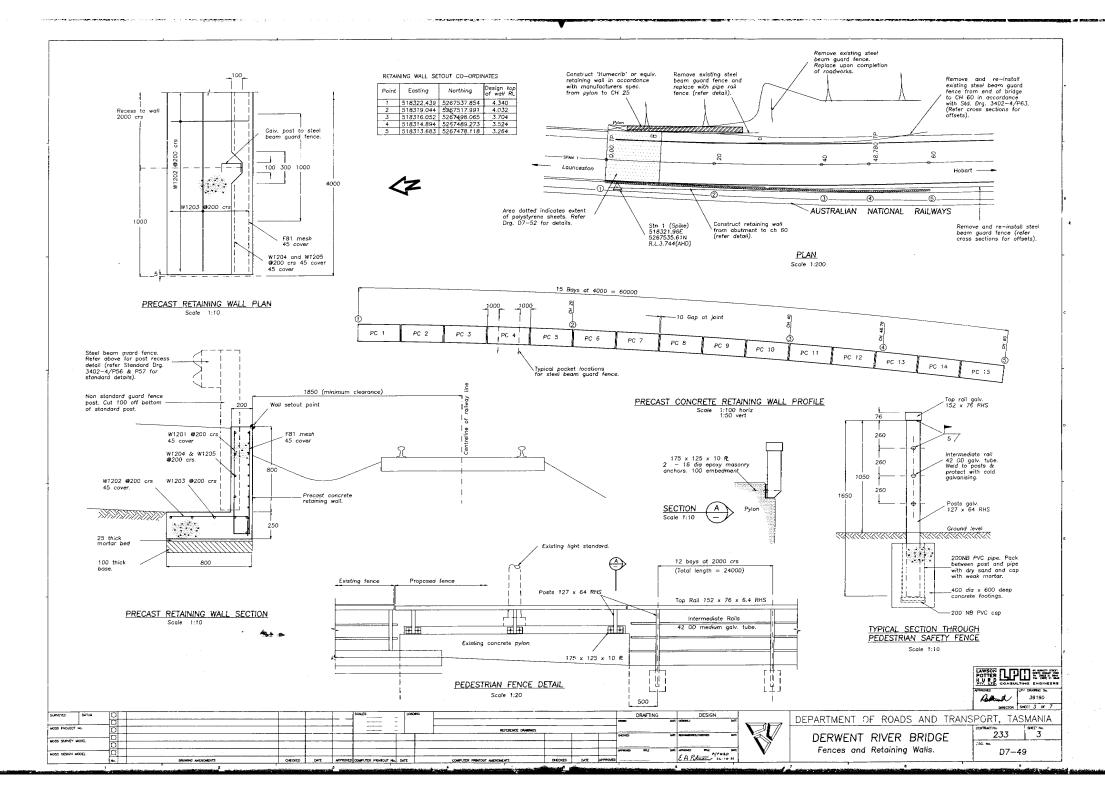
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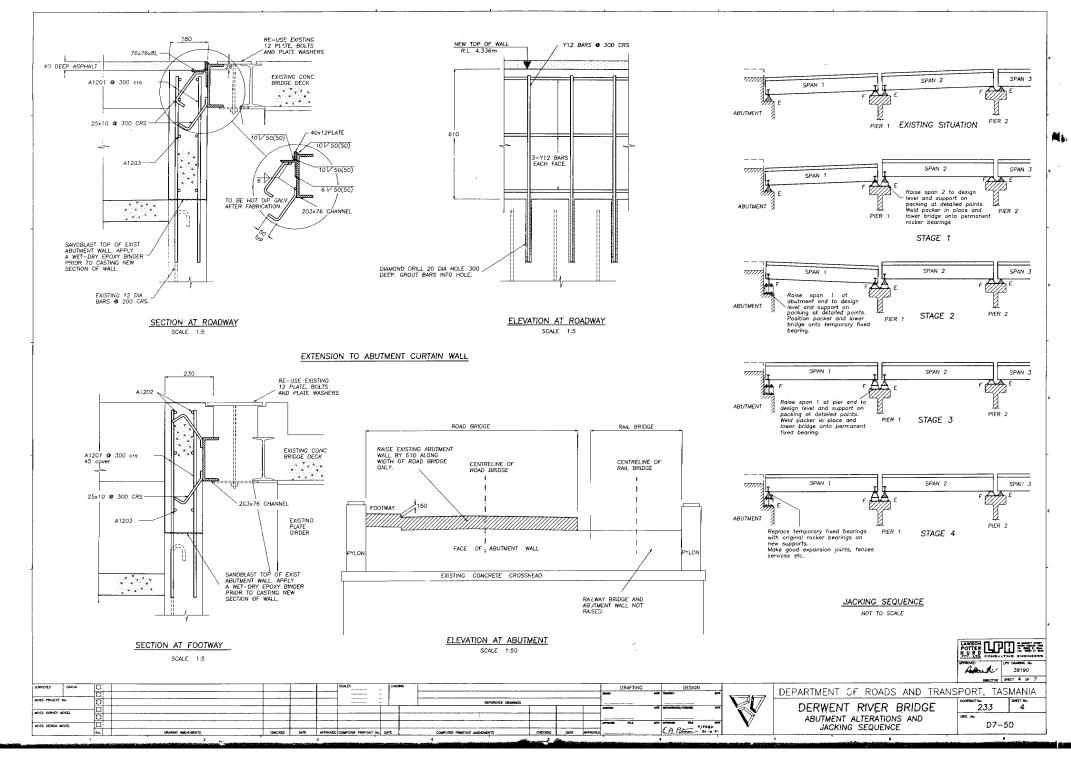
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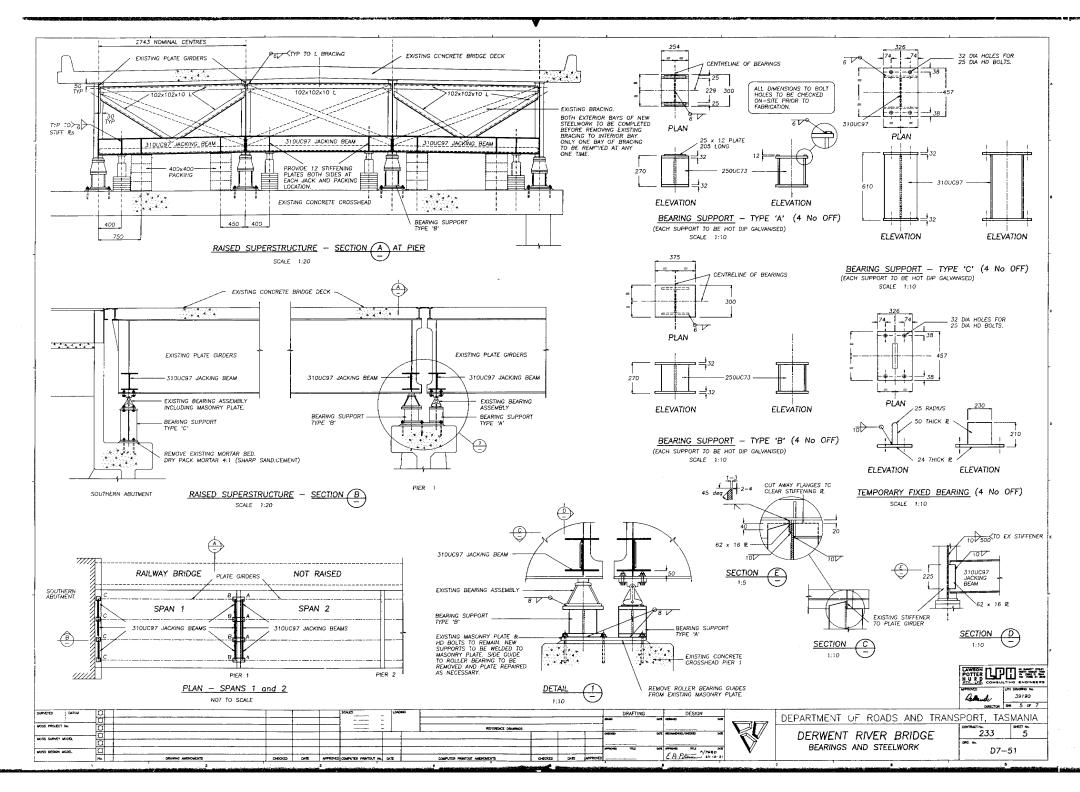
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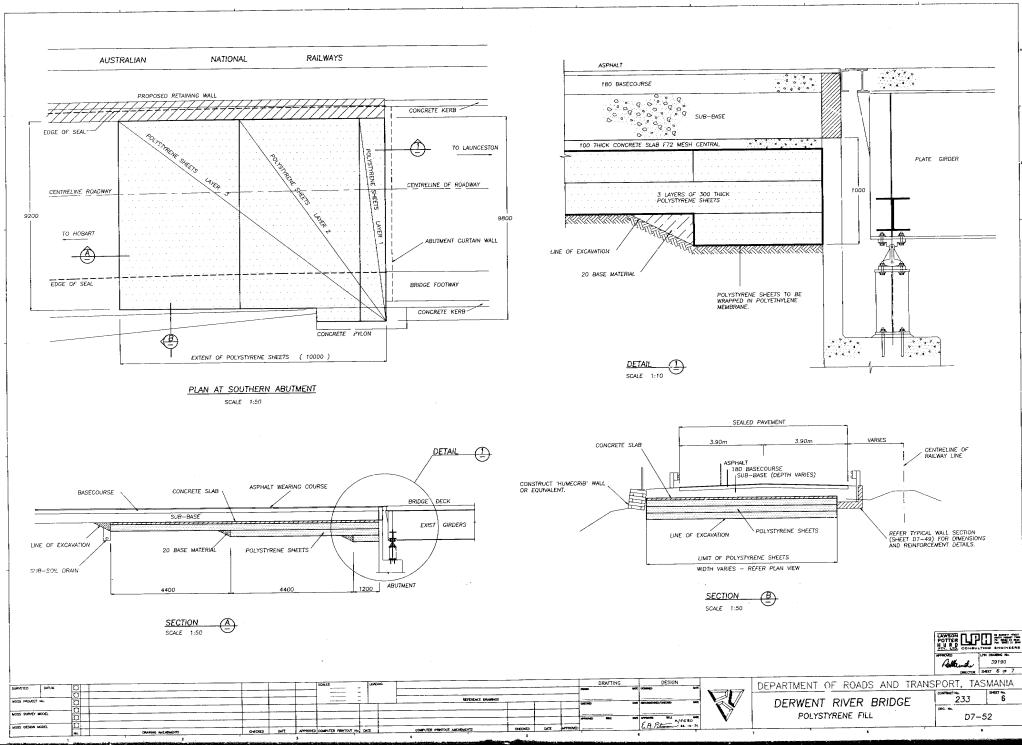




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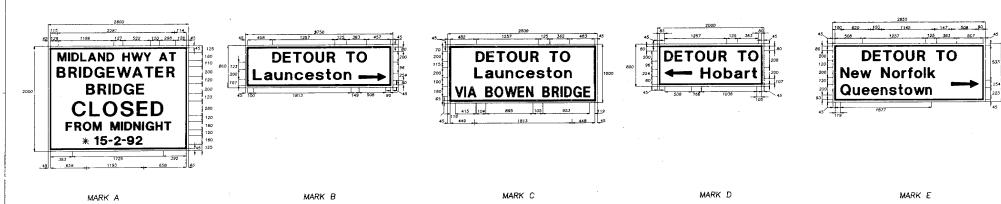






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* DATE AND TIME TO BE CONFIRMED AT AWARD OF CONTRACT

TEMPORARY SIGNS

MARK	No. REQUIRED	LOCATION		
A B – Left	1	Glenora Road – Lyelf Highway (Glenora Approach) 300m north of Blair Street Junction at New Norfolk.		
A B — Ahead	1 7	Boyer SR – Lyell Highway (Gretna Approach) 50m north of Sackriver Road Junction at New Norfolk.		
A	1	Lyell Highway — Midland Highway (New Norfolk Approach) 300m north west of Junction or 50m north west of existing AD.		
A	1	Brooker Highway – Lyelt Highway (Hobart Approach) 400m south of Black Snoke Lane Underpass.		
E – Right	1	Boyer SR — Midland Highway (Brighton Approach) 200m north east of junction.		
D – Left	1	Midland Highway – East Derwent Highway (Brighton Approach) North entrance to "Parkholme".		
A C	1	Brooker Avenue — Howard Road Roundabout (Hobart Approach) 200m south of pedestrian overpass bridge.		
ы — Right	1	Brooker Highway - Goodwood Road (Hobart Approach) North of Howard Road Roundabout.		
B – Left	1	Brooker Highway – Goodwood Road 700m north of Elwick Road.		
A	1	Brooker Highway 400m north cf Euston Street Overposs.		

0475

ED COMPUTER PRINTDUT No. DATE

COMPUTER PRIMTOUT AMENDMENTS

SIGNS TO BE COVERED

LOCATION	PART OF SIGN TO BE COVERED	No. OF SIGN
LUCATION	TART OF SIGN TO BE COULD	COVERED
Lyell Highway – Midiand Hwy: (New Norfolk)	Cover existing "Launceston " AD, route marker shield and "Launceston" 10.	3
Brooker Highway — Lyeil Hwy:— (Hobart Approach)	Cover existing "Launceston" AD and route marker shield.	2
Brooker SR – Midland Hwy:- (Boyer Approach)	Cover. "Hobart" FB.	t
Boyer SR — Midland Hwy:	Cover route marker shield and existing "Hobart" ID.	2
Boyer SR – Midland Hwy:- (Brighton Approach) Cover route marker shield		t
Midloria Highway — East Derwent Hwy:— (Old Beach Approach)	Cover existing "Hobart" FB, route marker shield, "Hobart" AD	3
Brooker Highway — Coodwood Roundobout (Hobart Approach)	Cover "Launceston" AD and route marker shield.	2
Brooker Highway — Goodwood Rd Jon:- (Hobart Approach)	Cover existing "Launceston" AD and route marker shield.	2
Brooker Hwy – Goodwood Rd Jon:– (Bowen Bridge Approach)	Cover "Launceston" AD and route marker shield. Cover "Launceston" FB.	3
Brooker Hwy, Claremont Link Rd:-	Cover existing "Launceston" ID (2 signs).	2

AD = Advanced Direction Sign, white on green. ID = Intersection Direction Sign, white on green FB = Fingerboard Sign, black on white.

TEMPORARY, ROAD SIGNS

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D7-53

TOTAL No. OF SIGNS = 14

WOSS SURVEY MODEL

WOSS DESIGN WODE

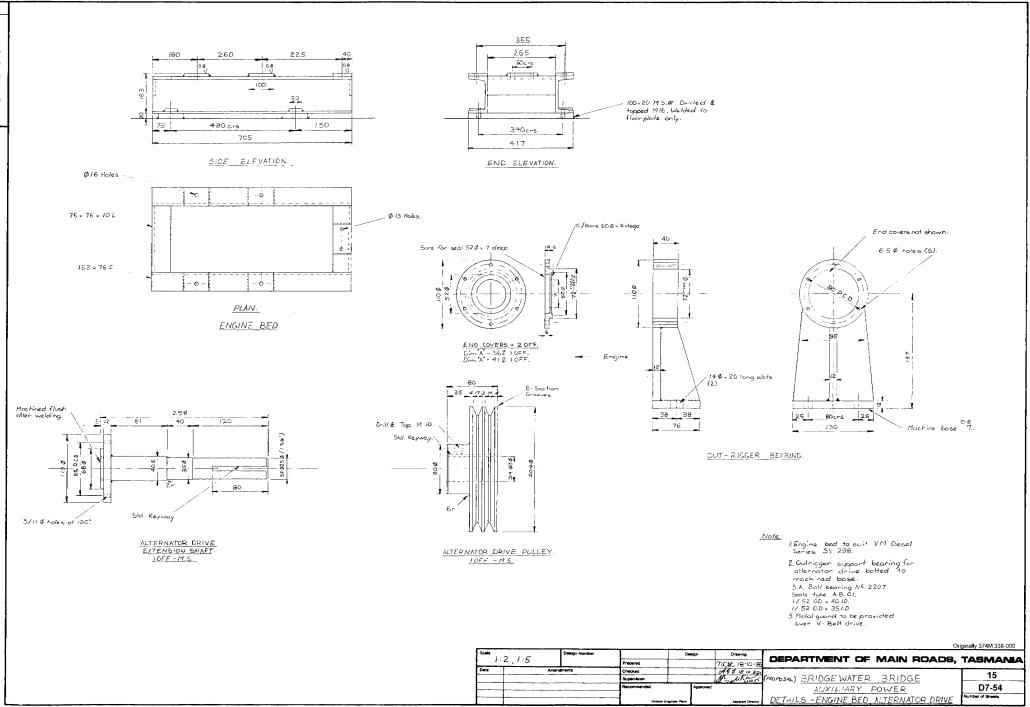
LETTERING TO AS 1743 160, 200, AND 280 HIGH UPPER CASE LETTERING SERIES E ş 200/150 LETTERING - SERIES E MODIFIED ₽₽₽₽₽₽ Q4 39190 HEET 7 OF 7 DESIGN DEPARTMENT OF ROADS AND TRANSPORT, TASMANIA 20 знеет №. 7 REFERENCE ORANIN 233 DERWENT RIVER BRIDGE DRG. No.

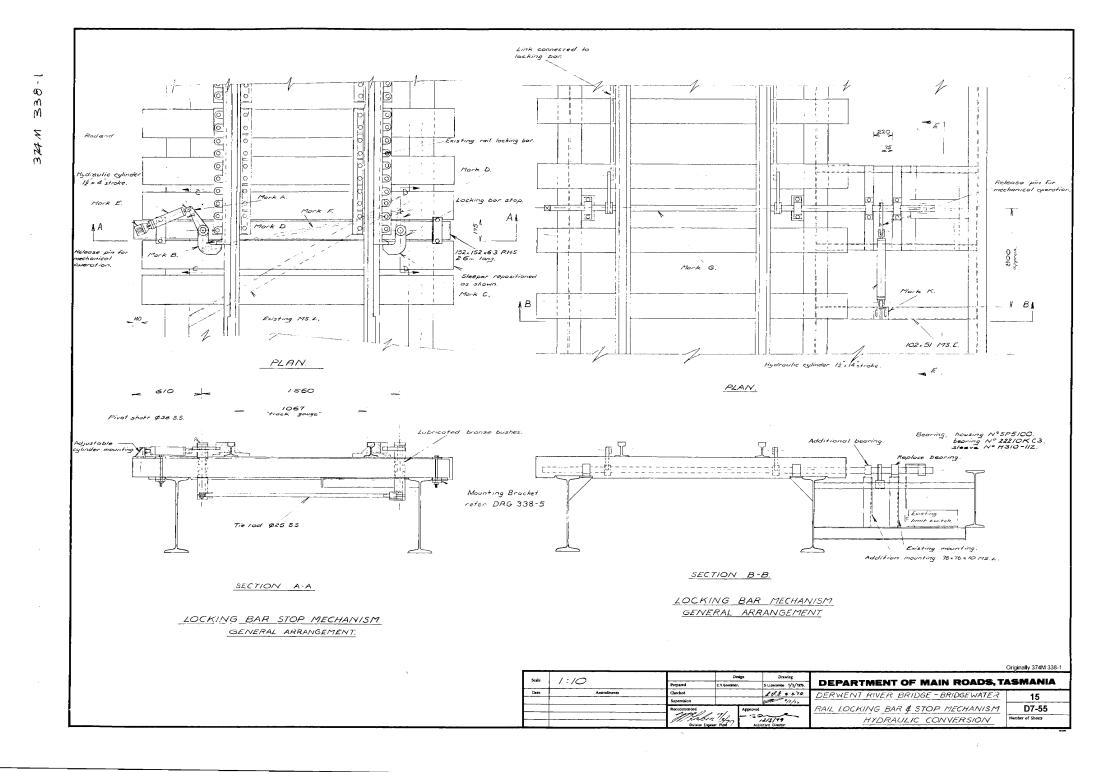
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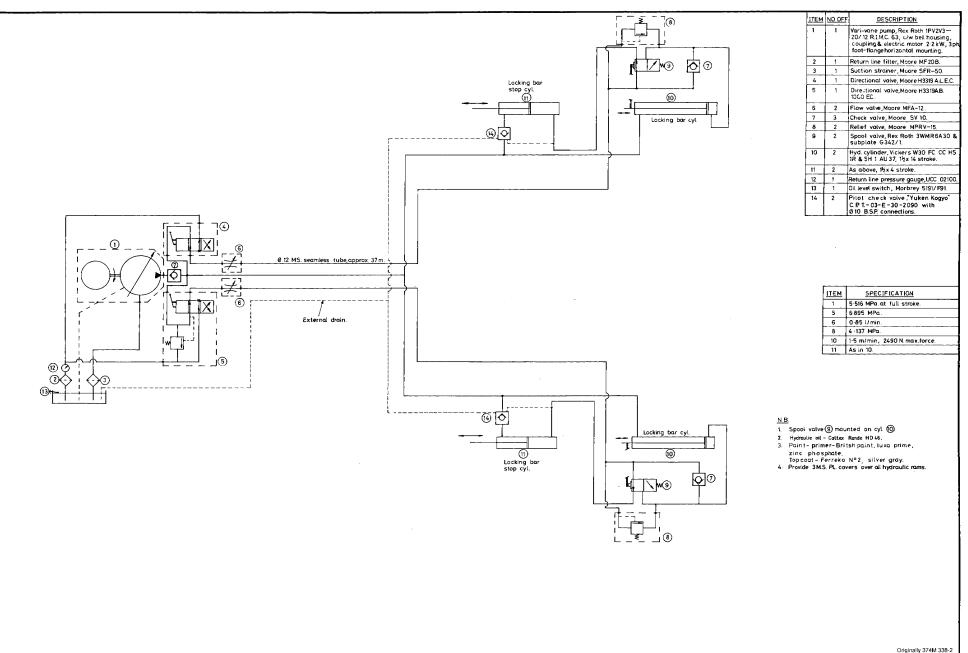




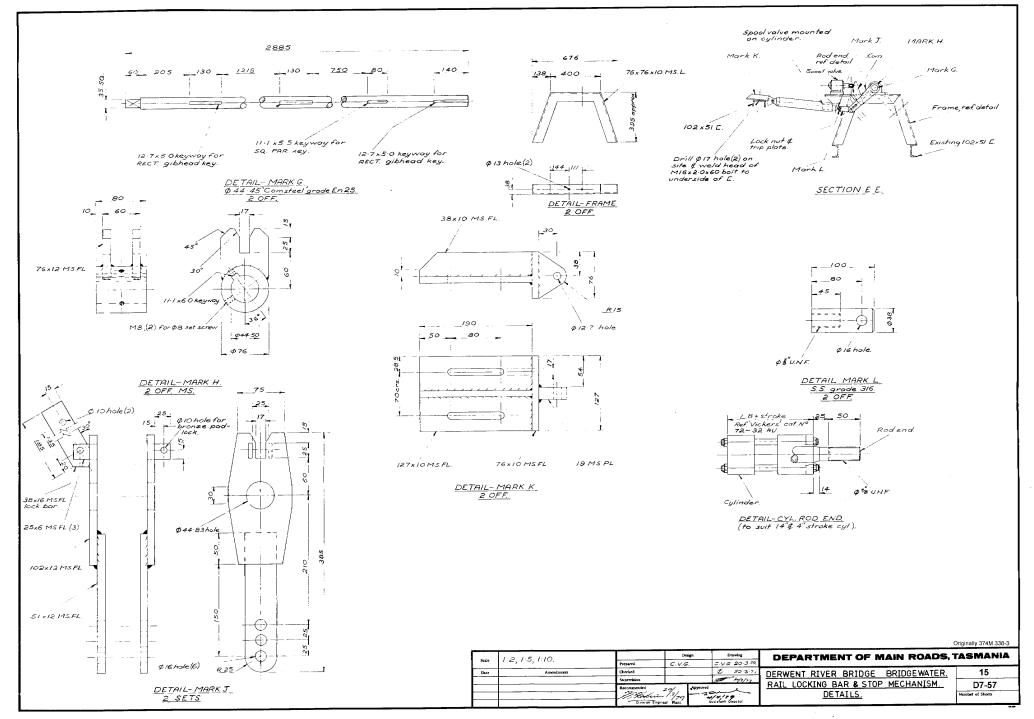




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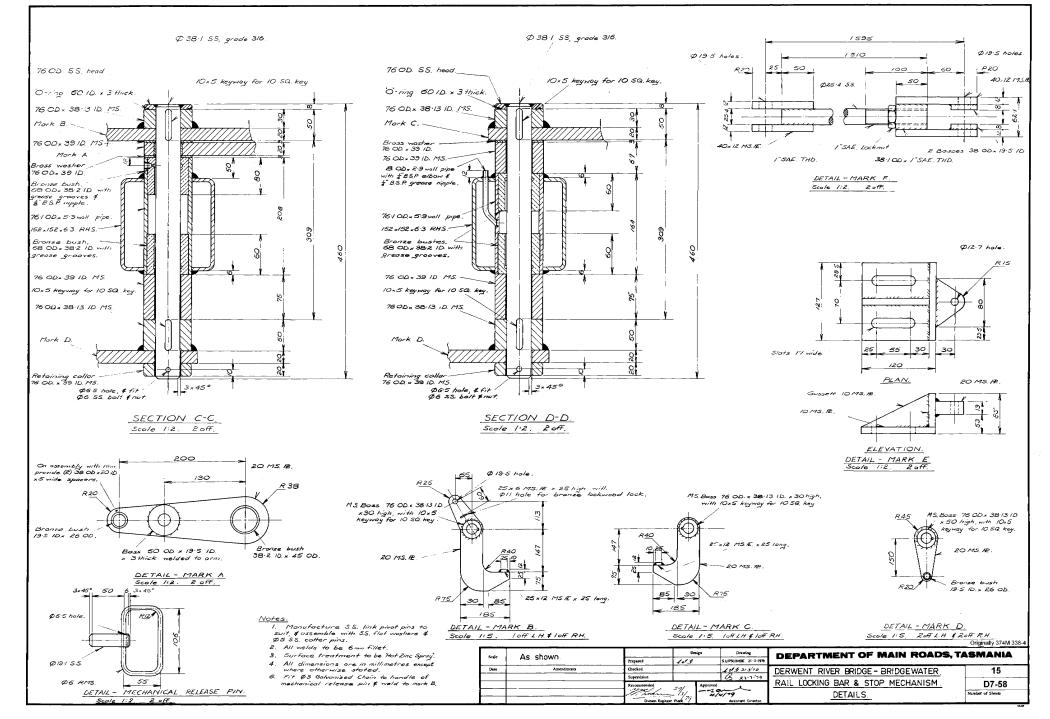
Scale	N.T.S.		Design	Drawing	DEPARTMENT OF MAIN BOADS TASMAN		
		N. I. S.	Prepared	C.V.G.	V.G. C.V.G. 8:379. SRL 6/9/79. DEPARTMENT OF MAIN ROADS, TASMANIA DERWENT RIVER BRIDGE - BRIDGEWATER. TABLE LOCKING BAR & STOP MECHANISM. DZ-56		
Ľ	Date	Amendments	Checked		SRL 8/3/79.	DERWENT RIVER BRIDGE - BRIDGEWATER	15
			Supervision		Fr 1/3/29		
-			Recommended	3/29 50	a/J/7 9 start Drester,		



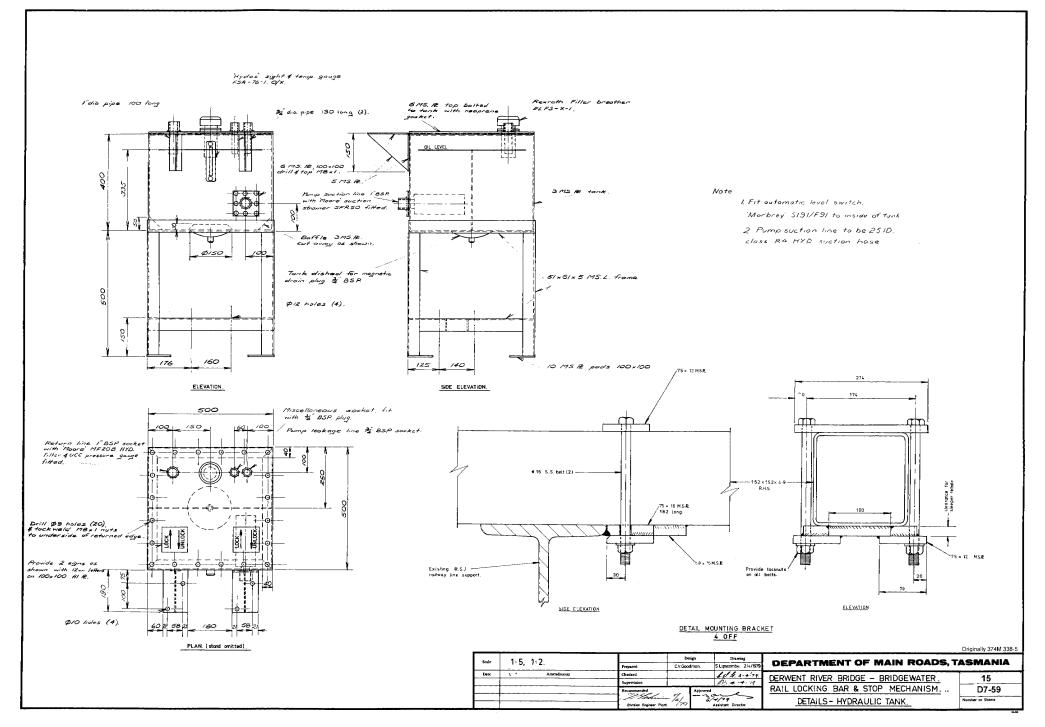
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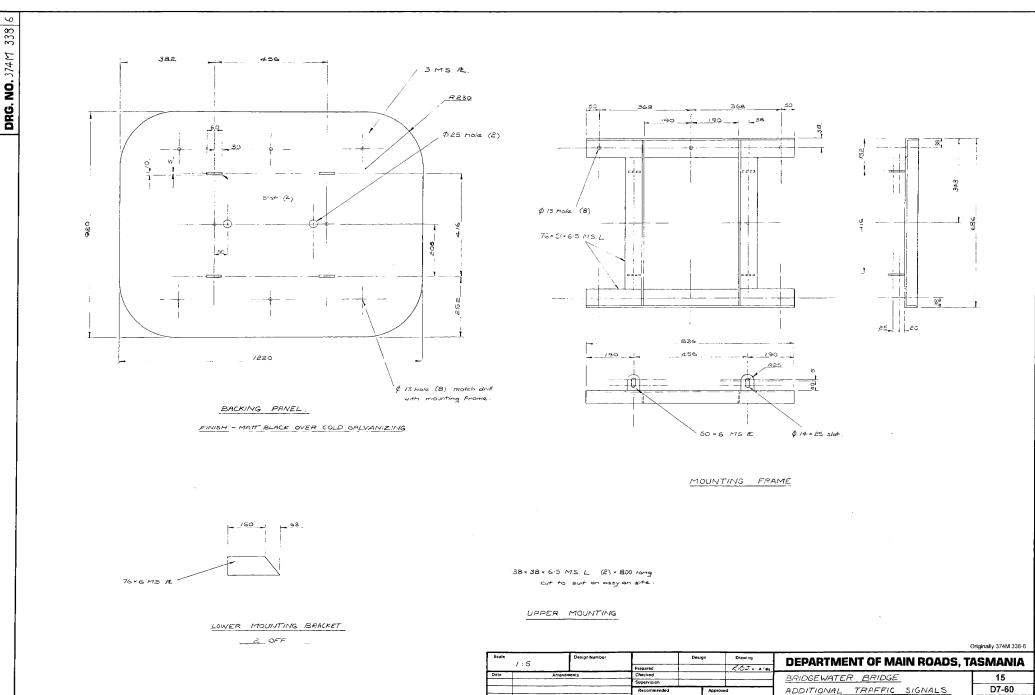
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≻age No	DrawingNo		Name2	Name3	Comment
	D8	LIFT SPAN REDECKING & CONTROL	+ CATHODIC PROTECTION		
2	D8-01	Redecking of Lift Span	Cover Sheet		
3	D8-02	Redecking of the Lift Span	General Arrangement		
4	D8-03	Redecking of the Lift Span	Stress Laminated Timber Deck	General	
5	D8-04	Redecking of the Lift Span	Stress Laminated Timber Deck	Steel Fabrication	
6	D8-05	Redecking of the Lift Span	Stress Laminated Timber Deck	Option A	
7	D8-06	Redecking of the Lift Span	Stress Laminaled Timber Deck	Option 8	
8	D8-07	Redecking of the Lift Span	Stress Laminated Timber Deck	Option C	
9	D8-08	Redecking of the Lift Span	Stress Laminated Timber Deck	Option D	
10	D8-09	Redecking of the Lift Span	Stress Laminaled Timber Deck	Options C & D	
11	D8-10	Redecking of the Lift Span	Deck Tie Downs	Sheet 1	
12	D8-11	Redecking of the Lift Span	Deck Tie Downs	Sheet 2	
13	D8-12	Redecking of the Lift Span	End Deck Joints	Sheet1	
14	D8-13	Redecking of the Lift Span	End Deck Joints	Sheel 2	
15	D8-14	Redecking of the Lift Span	Cross Beam Modifications	Sheet 1	
16	D8-15	Redecking of the Lift Span	Cross Beam Modifications	Sheet 2	
17	D8-16	Redecking of the Lift Span	Cross Beam Modifications	Sheel 3	
18	D8-17	Redecking of the Lift Span	Railway Side Kerb, Railing and	Drains - Sheel 1	
19	D8-18	Redecking of the Lift Span	Railway Side Kerb, Railing and	Drains - Sheel 1	
20	D8-19	Redecking of the lift Span	Railway Side Kerb, Railing and	Drains - Sheet 3	
21	D8-20	Redecking of the Lift Span	Footway Modifications and	Drains - Sheel 1	
22	D8-21	Redecking of the Lift Span	Footway Modifications and	Drains - Sheet 2	
23	D8-22	Redecking of the Lift Span	Temporary Support of the	Footway - Sheet 1	
24	D8-23	Redecking of the Lift Span	Temporary Support of the	Footway - Sheet 2	
25	D8-24	Redecking of the Lift Span	Launching and Installation	Sheet 1	
26	D8-25	Redecking of the Lift Span	Launching and Installation	Sheet 2	
27	D8-26	Redecking of the Lift Span	Launching and Installation	Sheet 3	
28	D8-27	Redecking of the Lift Span	Launching and Installation	Sheel 4	
29	D8-28	Redecking of the Lift Span	Table of Materials and	Construction Notes	
30	D8-29	LIFT SPAN CONTROL	240V AC PLC INPUT SCHEMATIC		
31	D8-30	LIFT SPAN CONTROL	240V AC PLC INPUT SCHEMATIC		
32	D8-31	LIFT SPAN CONTROL	240V AC PLC OUTPUT SCHEMATIC		
33	D8-32	LIFT SPAN CONTROL	240V PLC OUTPUT MODULE #7	SCHEMATIC DIAGRAM	
34	D8-33	LIFT SPAN CONTROL	240V AC CONTROL CIRCUITS	SCHEMATIC DIAGRAM	
35	D8-34	LIFT SPAN CONTROL	MAIN SUPPLIES	SCHEMATIC DIAGRAM	
36	D8-35	LIFT SPAN CONTROL	240V AC CONTROL CIRCUIT	SCHEMATIC DIAGRAM	
37	D8-36	LIFT SPAN CONTROL	240V AC CONTROL CIRCUIT	SCHEMATIC DIAGRAM	
38	D8-37	LIFT SPAN CONTROL	SPAN MOTORS	SCEMATIC DIAGRAM	
39	D8-38	LIFT SPAN CONTROL	415V AC AUXILIARY CIRCUITS	SCHEMATIC DIAGRAM	
40	D8-39	Calhodic Protection & Ass Work	Typical Arrangement	Piers 1 to 8 & 13	Contract 72
41	D8-40	Calhodic Protection & Ass Work	General Arrangement	Piers 9,10,11&12	Contract 72
42	D8-41	Calhodic Protection & Ass Work	Electrical Schematic	Buried Structure System	Contract 72
43	D8-42	Calhodic Protection & Ass Work	General Arrangements	For Abutments	Contract 72
44	D8-43	Calhodic Protection & Ass Work	Typical Transformer	Rectifiers Details	Contract 721
45	D8-44	Cathodic Protection & Ass Work	Below Water	Protection System Lay out	Contract720

BRIDGEWATER BRIDGE

D8- LIFT SPAN REDECKING & CONTROL & CATHODIC PROTECTION TABLE OF CONTENTS

DEPARTMENT OF INFRASTRUCTURE, ENERGY AND RESOURCES

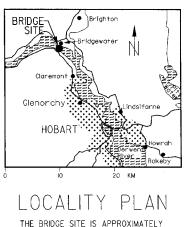
MIDLAND HIGHWAY

BRIDGEWATER

BRIDGE OVER THE DERWENT RIVER at bridgewater, tasmania NEW STRESS LAMINATED TIMBER DECKING AND CROSS BEAM STRENGTHENING

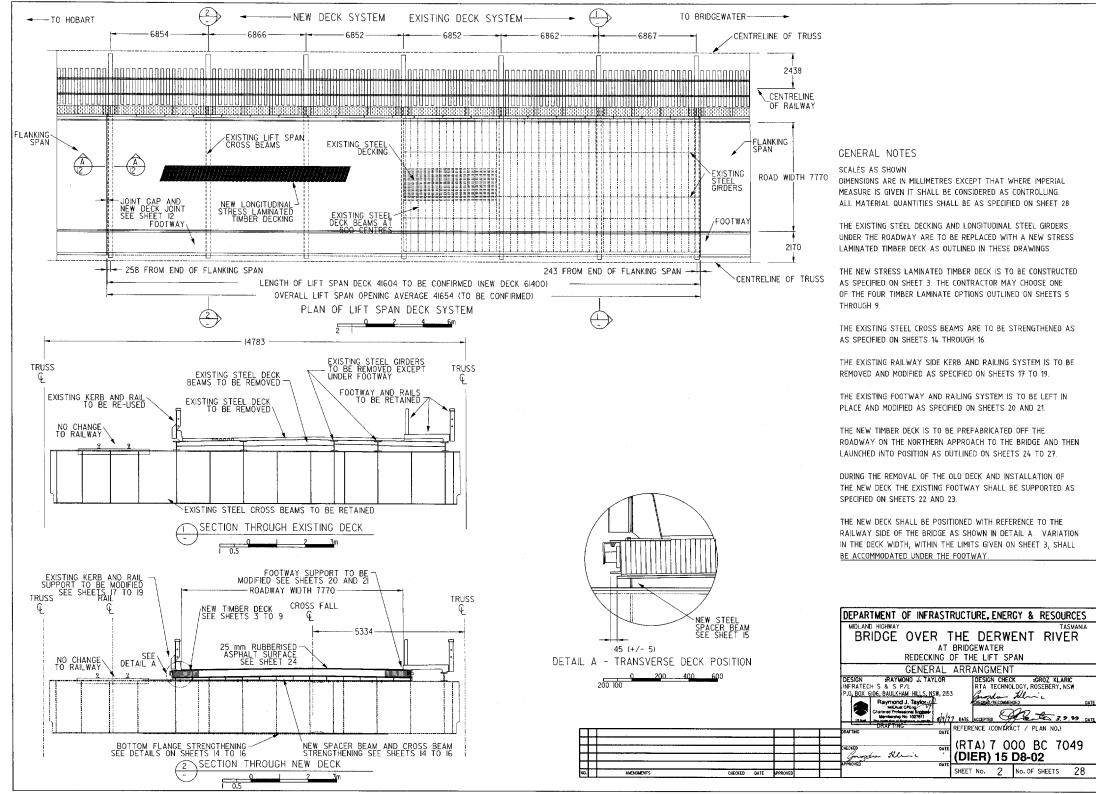
SCHEDULE OF DRAWINGS

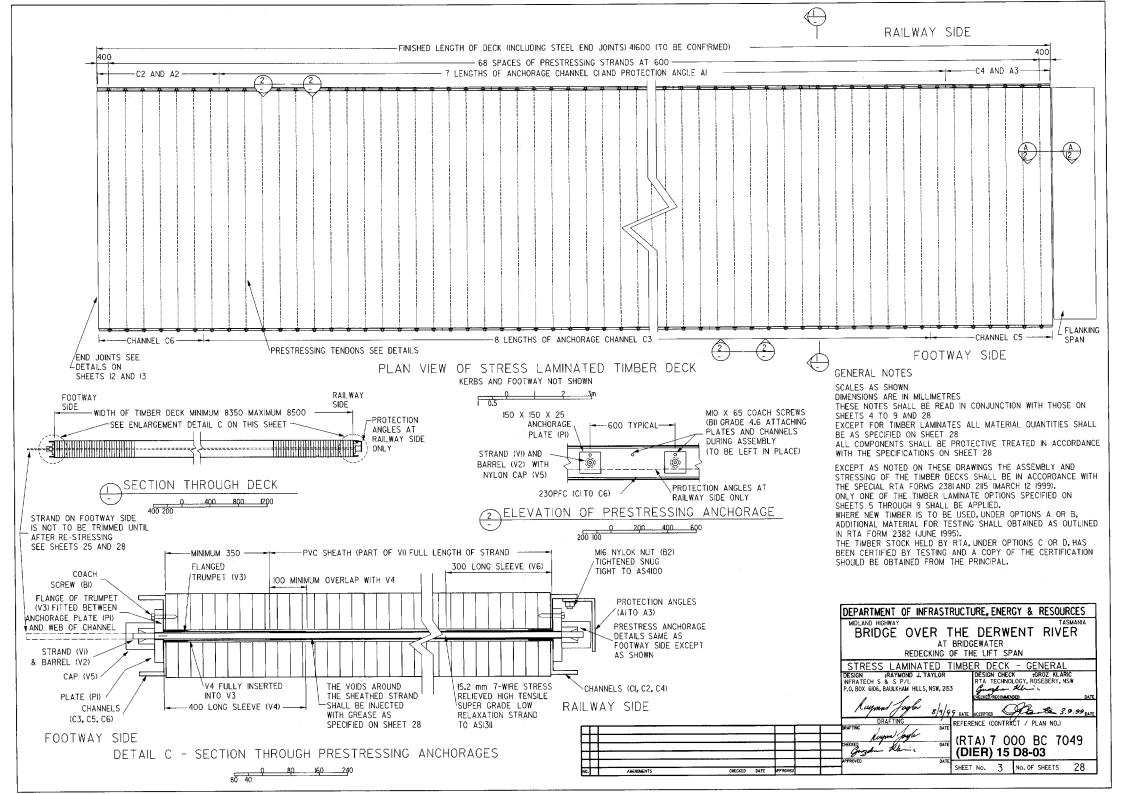
I. COVER SHEET

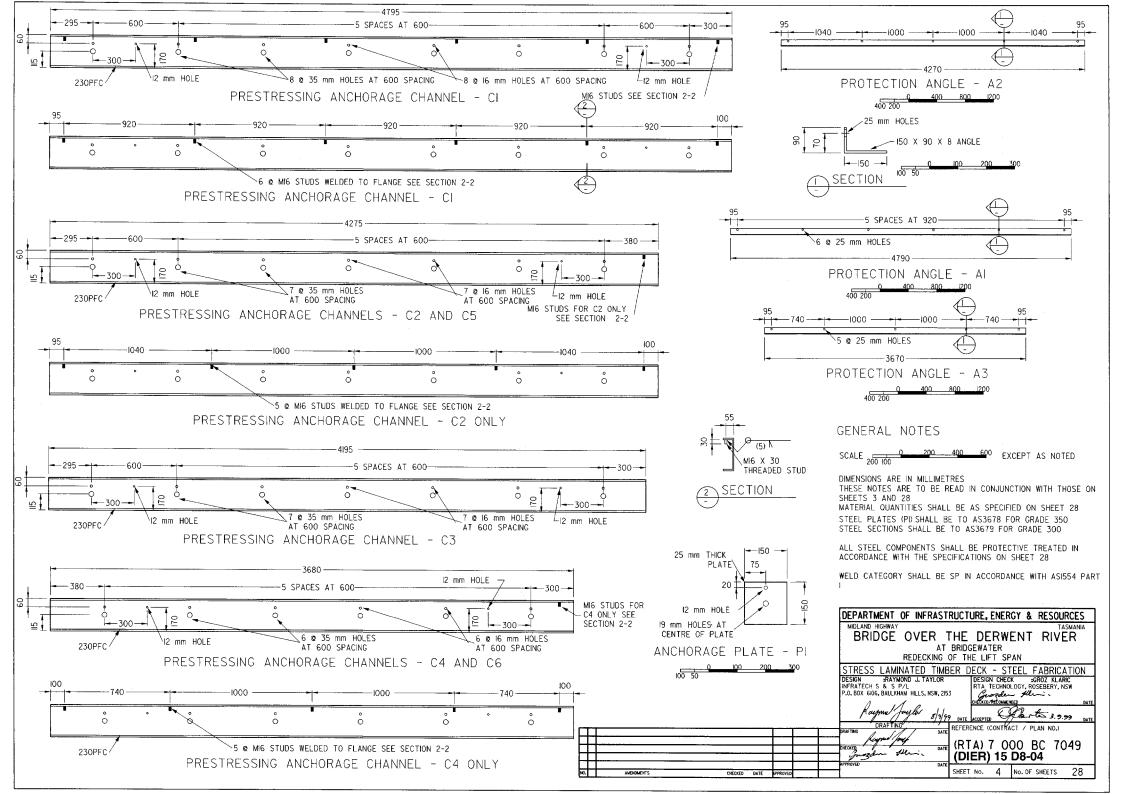


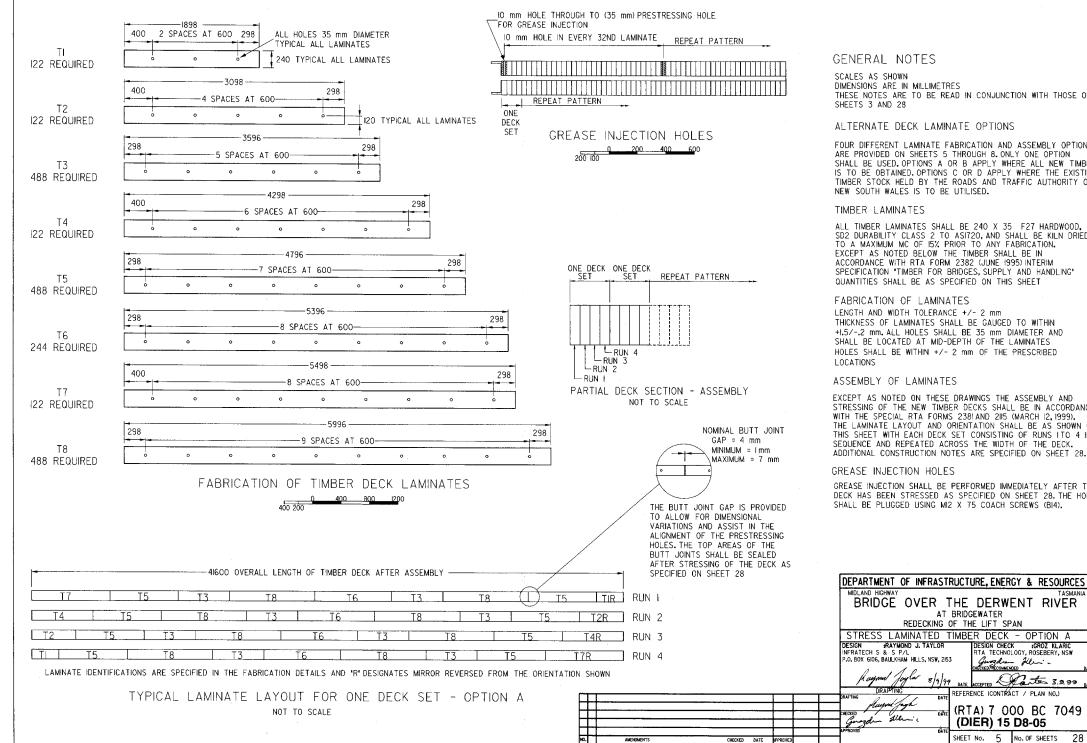
THE BRIDGE SITE IS APPROXIMATELY 20 Km FROM HOBART CITY CENTRE 2. GENERAL ARRANGEMENT 3. STRESS LAMINATED TIMBER DECK - GENERAL 4. STRESS LAMINATED TIMBER DECK - STEEL FABRICATION 5. STRESS LAMINATED TIMBER DECK - OPTION A 6. STRESS LAMINATED TIMBER DECK - OPTION B 7. STRESS LAMINATED TIMBER DECK - OPTION C 8. STRESS LAMINATED TIMBER DECK - OPTION D 9. STRESS LAMINATED TIMBER DECK - OPTIONS C AND D 10. DECK THE DOWNS - SHEET | IL DECK THE DOWNS - SHEET 2 12. END DECK JOINTS - SHEET I 13. END DECK JOINTS - SHEET 2 14. CROSS BEAM MODIFICATIONS - SHEET I 15. CROSS BEAM MODIFICATIONS - SHEET 2 16. CROSS BEAM MODIFICATIONS - SHEET 3 17. RAILWAY SIDE KERB, RAILING AND DRAINS - SHEET I 18. RAILWAY SIDE KERB, RAILING AND DRAINS - SHEET 2 19. RAILWAY SIDE KERB. RAILING AND DRAINS - SHEET 3 20. FOOTWAY MODIFICATIONS AND DRAINS - SHEET I 21. FOOTWAY MODIFICATIONS AND DRAINS - SHEET 2 22. TEMPORARY SUPPORT OF THE FOOTWAY - SHEET I 23. TEMPORARY SUPPORT OF THE FOOTWAY - SHEET 2 24. LAUNCHING AND INSTALLATION - SHEET H 25. LAUNCHING AND INSTALLATION - SHEET 2 26, LAUNCHING AND INSTALLATION - SHEET 3 27. LAUNCHING AND INSTALLATION - SHEET 4 28. TABLE OF MATERIALS AND CONSTRUCTION NOTES

EXISTING BRIDGE ORIGINAL - 1938 PREVIOUS DECK REPLACEMENT - 1979 NEW TIMBER DECK AND CROSS BEAM STRENGTHENING- 1999 DESIGN LOADING: 92 AUSTROADS T44 LIVE LOAD BRAKING FORCES - NAASRA 1976 TRAFFIC BARRIERS: NOT UPGRADED REGISTRATION OF PLANS 7 000 BC 7049 SHEET No I NO. OF SHEETS 28 (DIER) 15 D8-01









DIMENSIONS ARE IN MILLIMETRES THESE NOTES ARE TO BE READ IN CONJUNCTION WITH THOSE ON

ALTERNATE DECK LAMINATE OPTIONS

FOUR DIFFERENT LAMINATE FABRICATION AND ASSEMBLY OPTIONS ARE PROVIDED ON SHEETS 5 THROUGH 8. ONLY ONE OPTION SHALL BE USED. OPTIONS A OR B APPLY WHERE ALL NEW TIMBER IS TO BE OBTAINED, OPTIONS C OR D APPLY WHERE THE EXISTING TIMBER STOCK HELD BY THE ROADS AND TRAFFIC AUTHORITY OF NEW SOUTH WALES IS TO BE UTILISED.

ALL TIMBER LAMINATES SHALL BE 240 X 35 F27 HARDWOOD. SD2 DURABILITY CLASS 2 TO ASI720, AND SHALL BE KILN DRIED TO A MAXIMUM MC OF 15% PRIOR TO ANY FABRICATION. EXCEPT AS NOTED BELOW THE TIMBER SHALL BE IN ACCORDANCE WITH RTA FORM 2382 (JUNE 1995) INTERIM SPECIFICATION "TIMBER FOR BRIDGES, SUPPLY AND HANDLING" QUANTITIES SHALL BE AS SPECIFIED ON THIS SHEET

FABRICATION OF LAMINATES

LENGTH AND WIDTH TOLERANCE +/- 2 mm THICKNESS OF LAMINATES SHALL BE GAUGED TO WITHIN +1.5/-.2 mm. ALL HOLES SHALL BE 35 mm DIAMETER AND SHALL BE LOCATED AT MID-DEPTH OF THE LAMINATES HOLES SHALL BE WITHIN +/- 2 mm OF THE PRESCRIBED

ASSEMBLY OF LAMINATES

EXCEPT AS NOTED ON THESE DRAWINGS THE ASSEMBLY AND STRESSING OF THE NEW TIMBER DECKS SHALL BE IN ACCORDANCE WITH THE SPECIAL RTA FORMS 238 AND 2115 (MARCH 12, 1999). THE LAMINATE LAYOUT AND ORIENTATION SHALL BE AS SHOWN ON THIS SHEET WITH EACH DECK SET CONSISTING OF RUNS I TO 4 IN SEQUENCE AND REPEATED ACROSS THE WIDTH OF THE DECK. ADDITIONAL CONSTRUCTION NOTES ARE SPECIFIED ON SHEET 28.

GREASE INJECTION SHALL BE PERFORMED IMMEDIATELY AFTER THE DECK HAS BEEN STRESSED AS SPECIFIED ON SHEET 28. THE HOLES SHALL BE PLUGGED USING MI2 X 75 COACH SCREWS (BI4).

AT BRIDGEWATER

DESIGN CHECK :GROZ KLARIC

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(RTA) 7 000 BC 7049

REFERENCE (CONTRACT / PLAN NO.)

(DIER) 15 D8-05

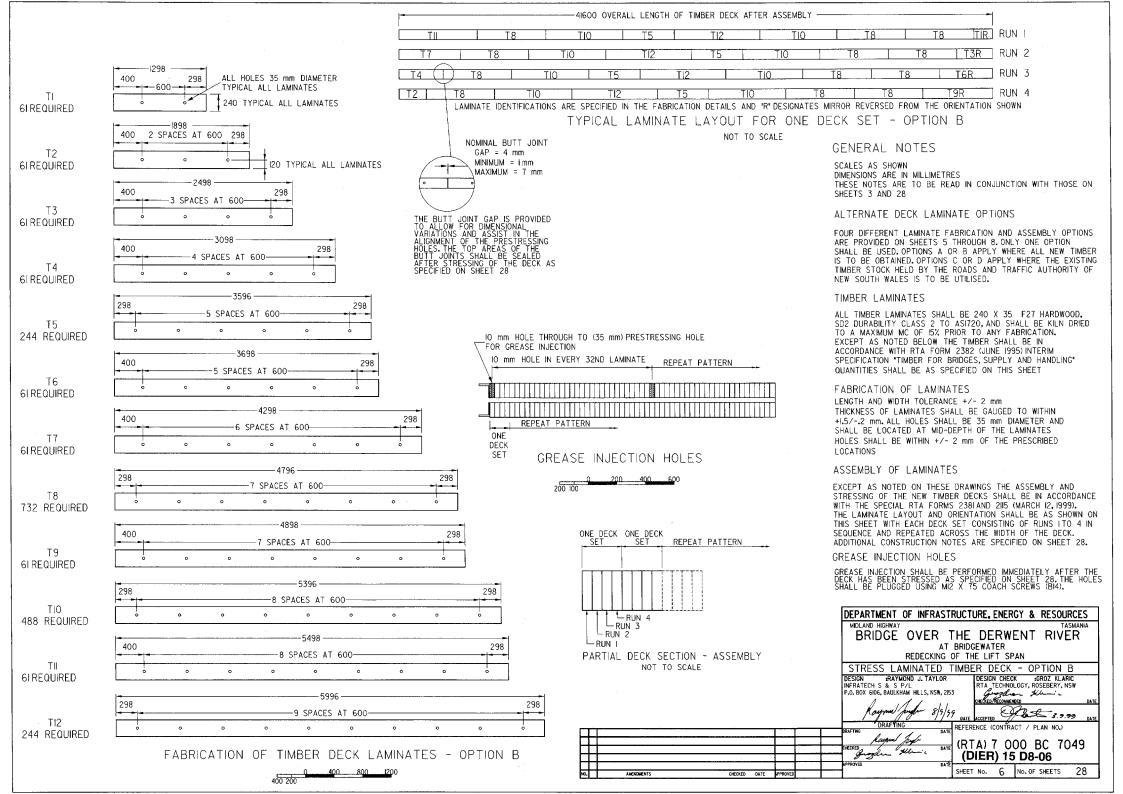
SHEET NO. 5 NO. OF SHEETS

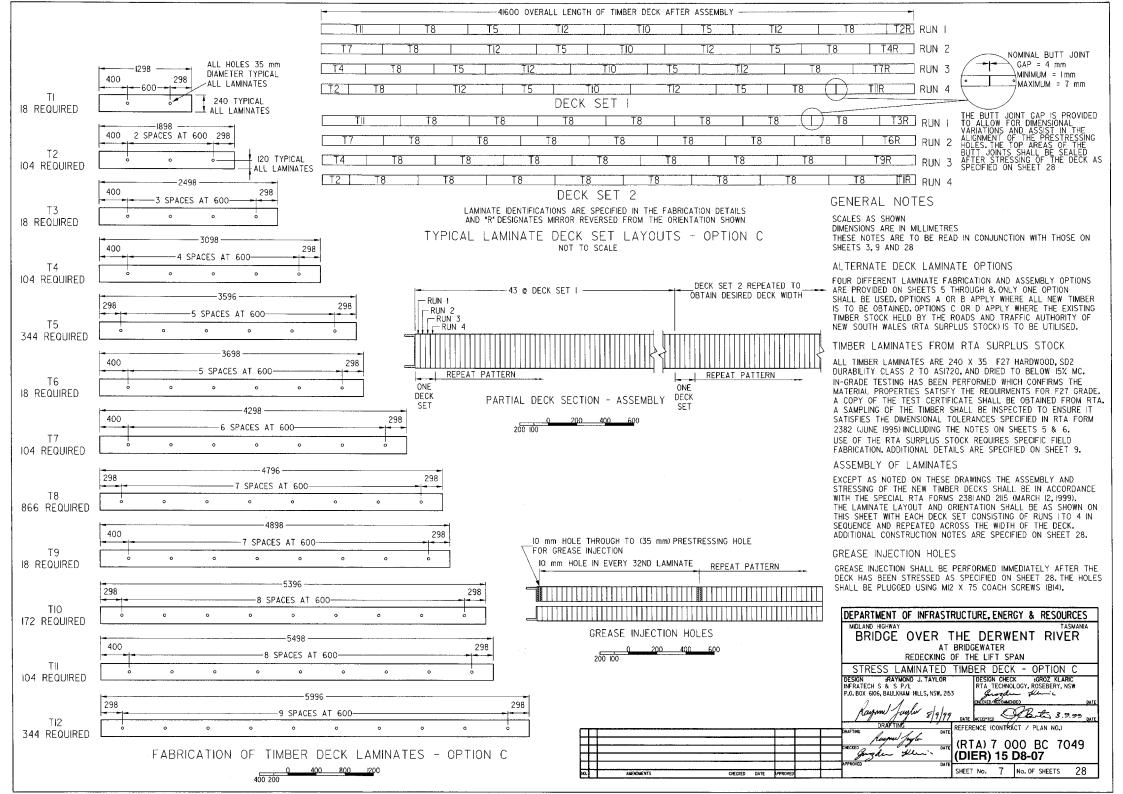
TA TECHNOLOGY, ROSEBERY, NSW

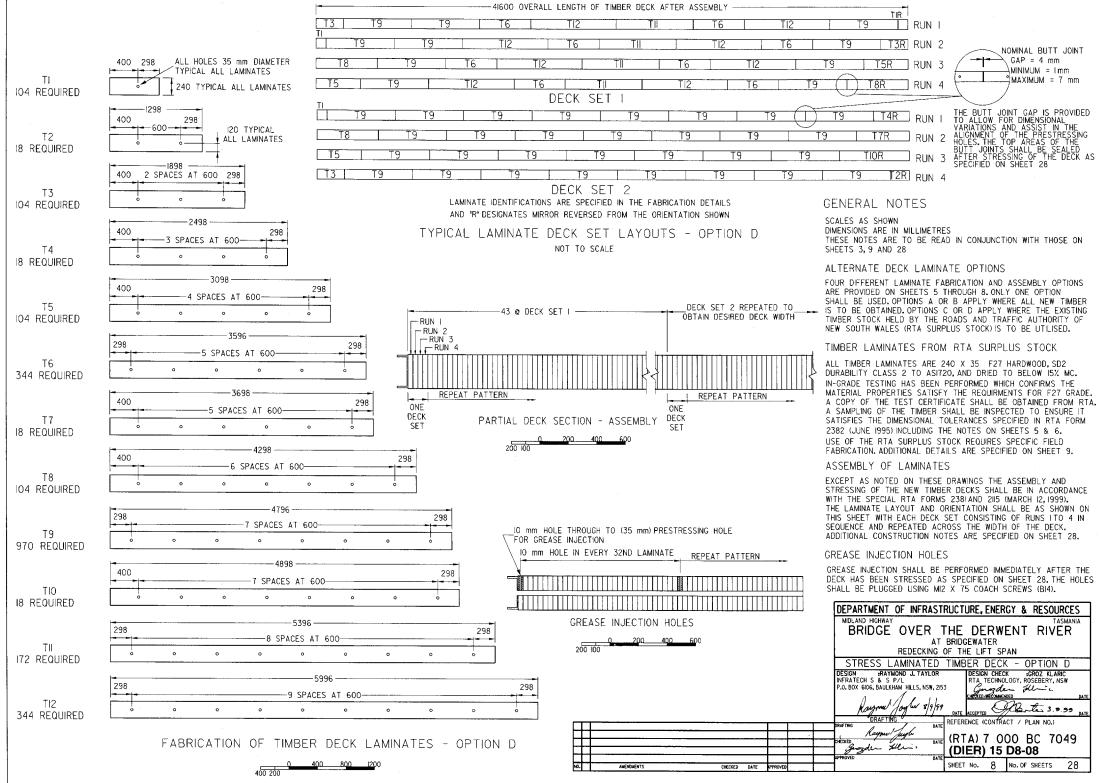
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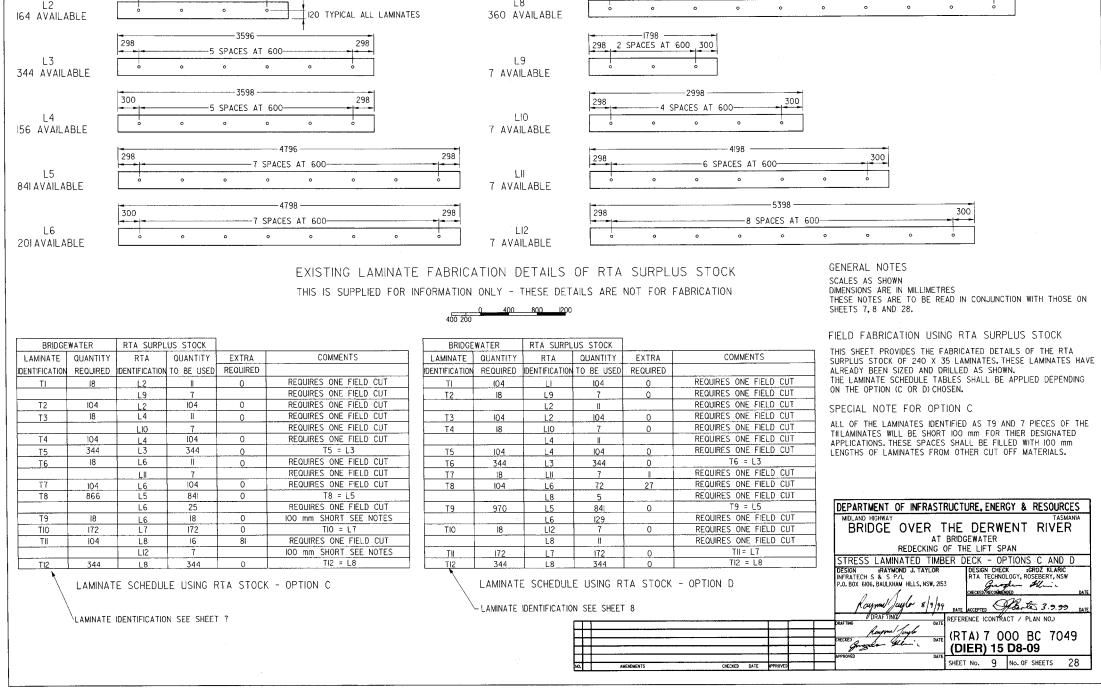
TASMANIA

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L7 172 AVAILABLE 298 L8

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8 SPACES AT 600-

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-3 SPACES AT 600-

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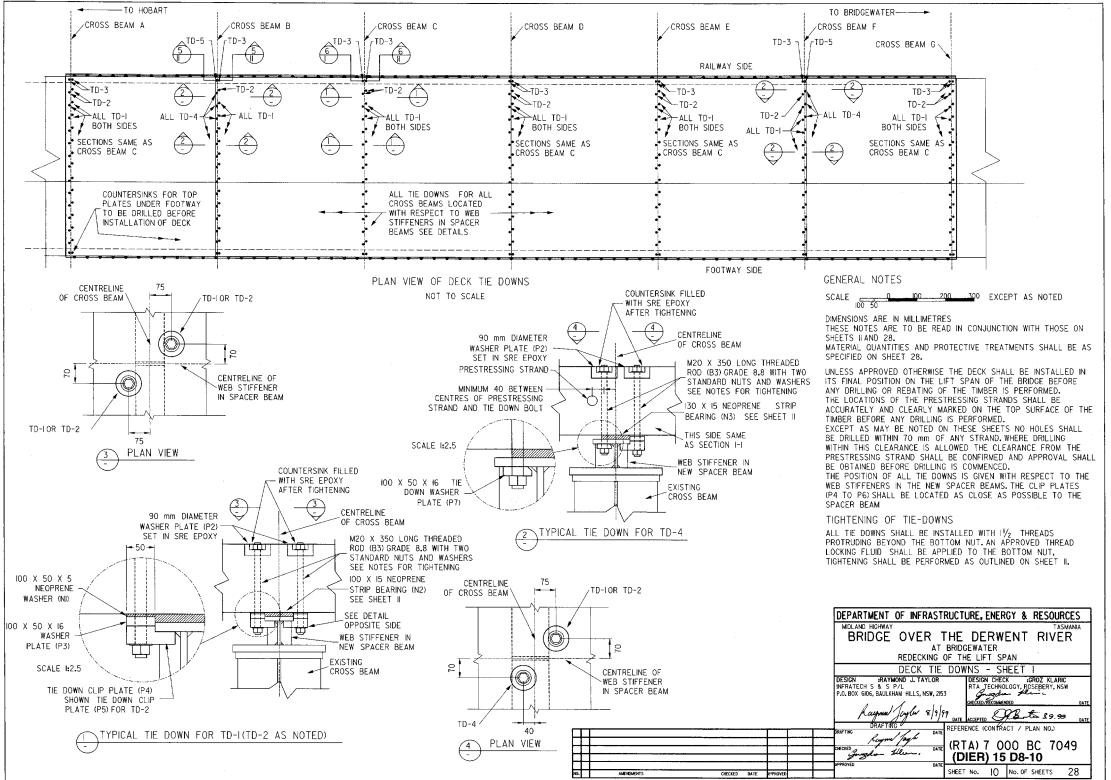
156 AVAILABLE

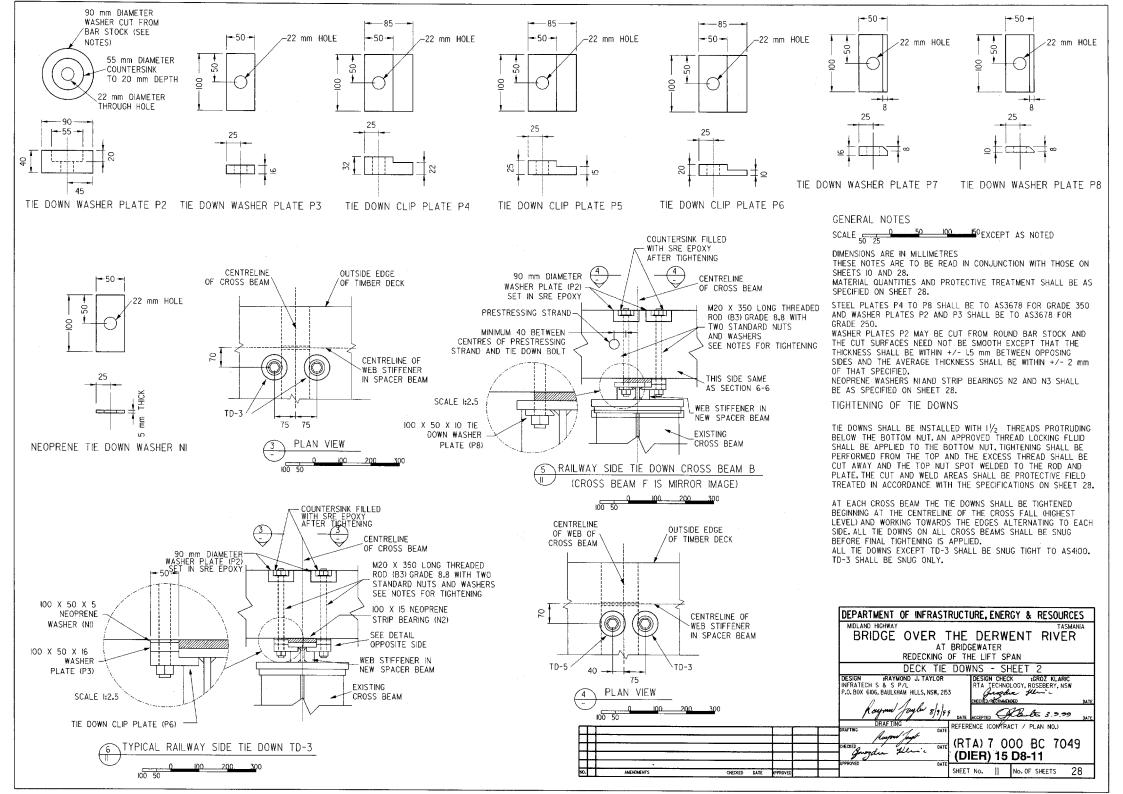
ALL HOLES 35 mm DIAMETER

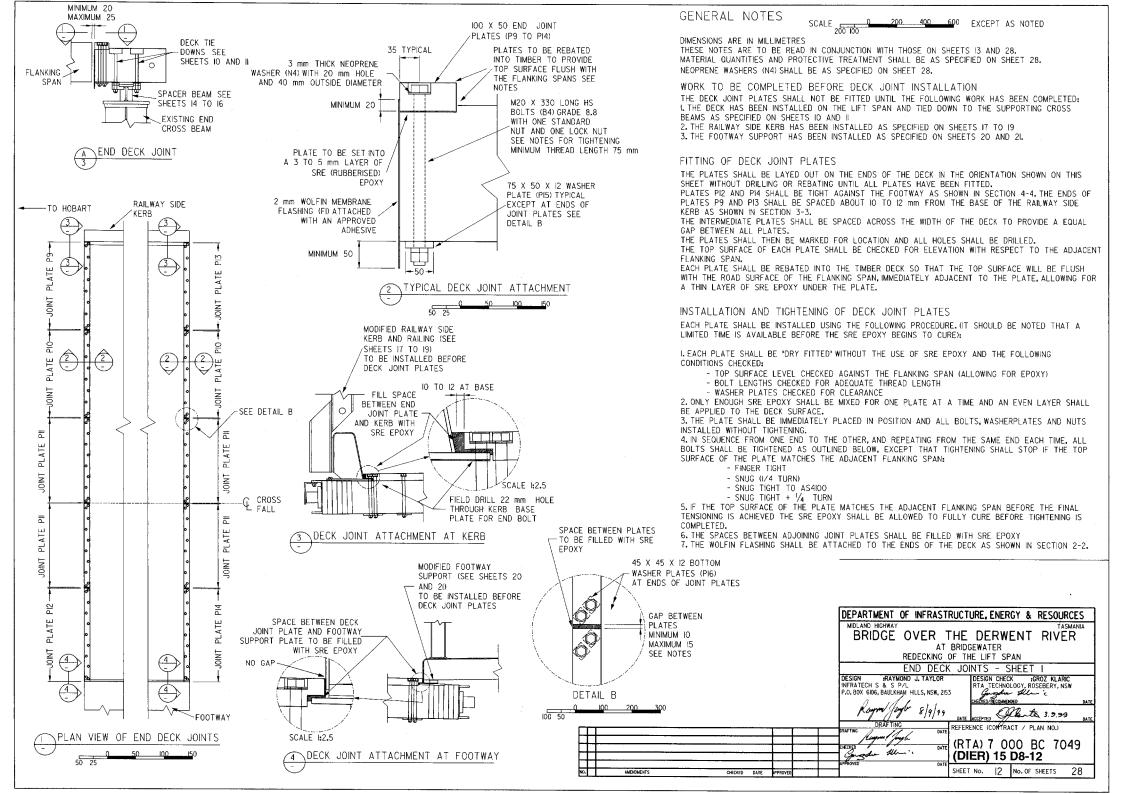
240 TYPICAL ALL LAMINATES

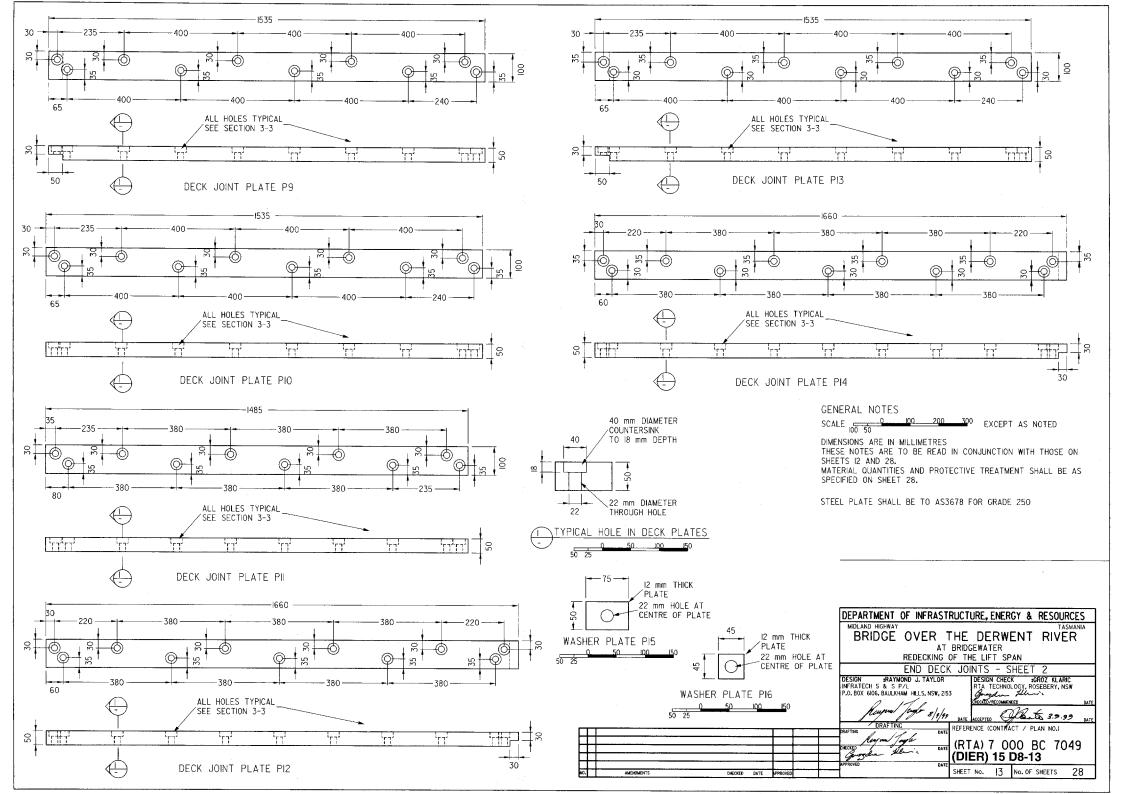
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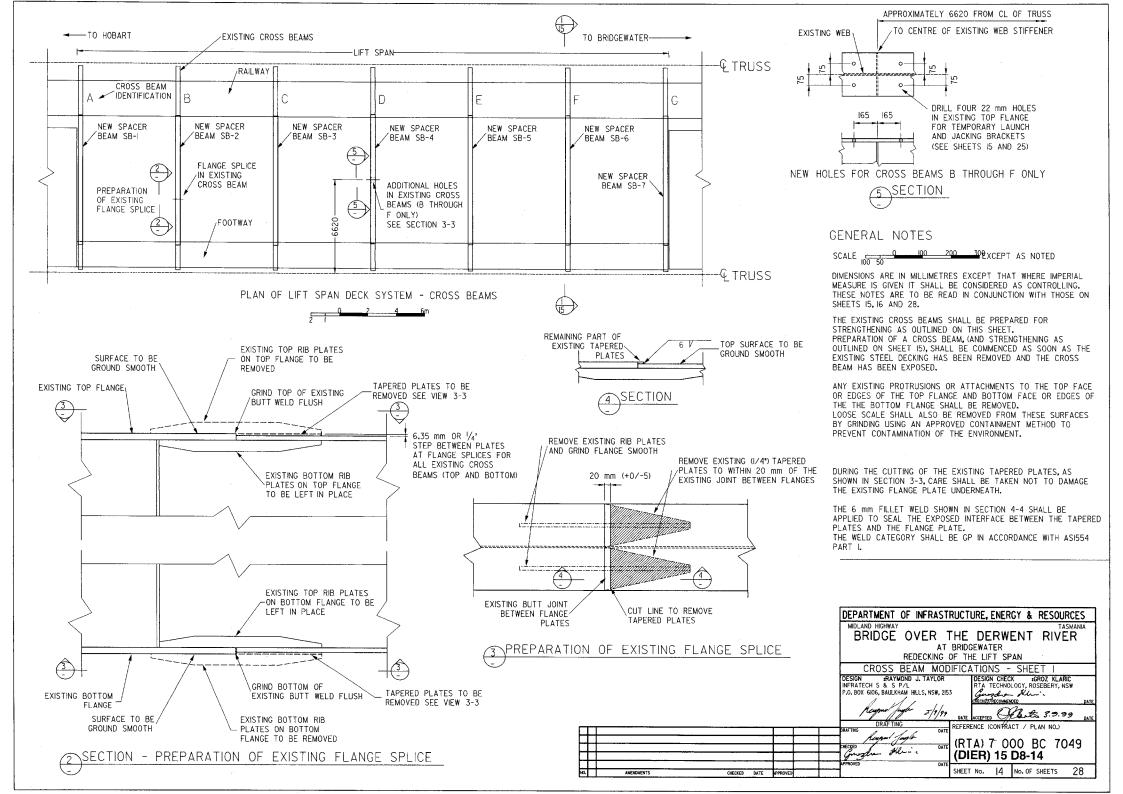
TYPICAL ALL LAMINATES

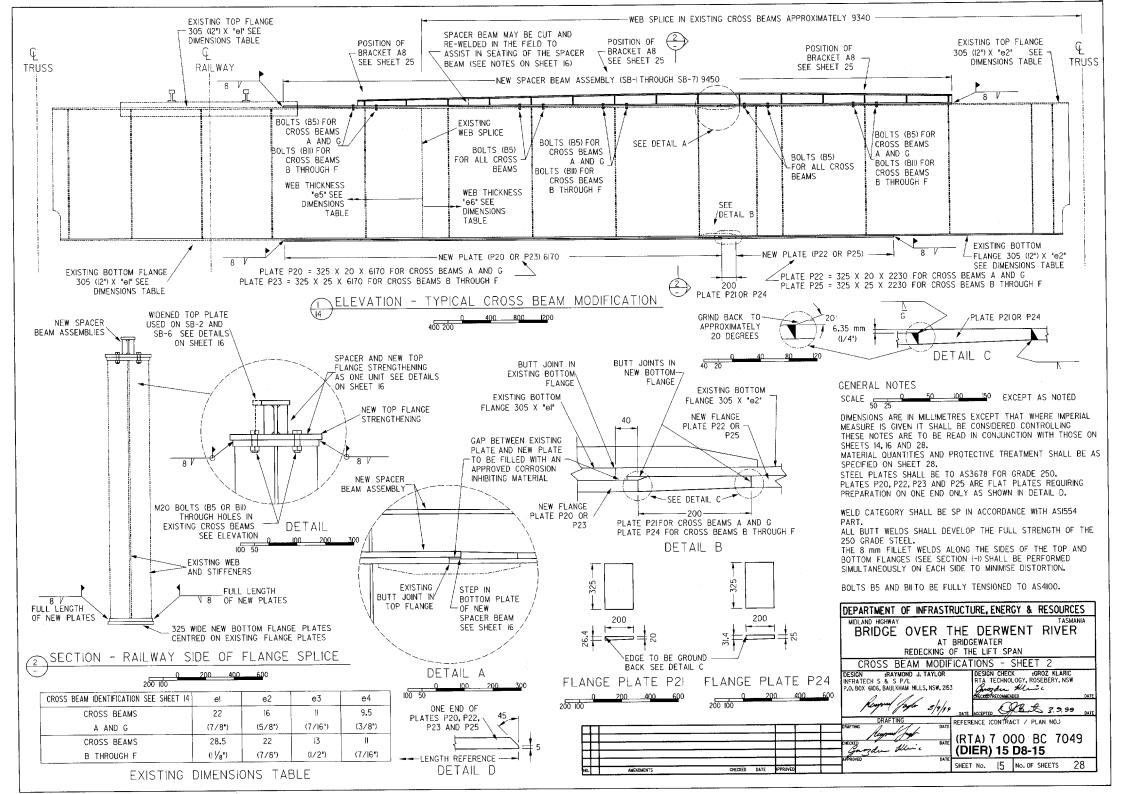


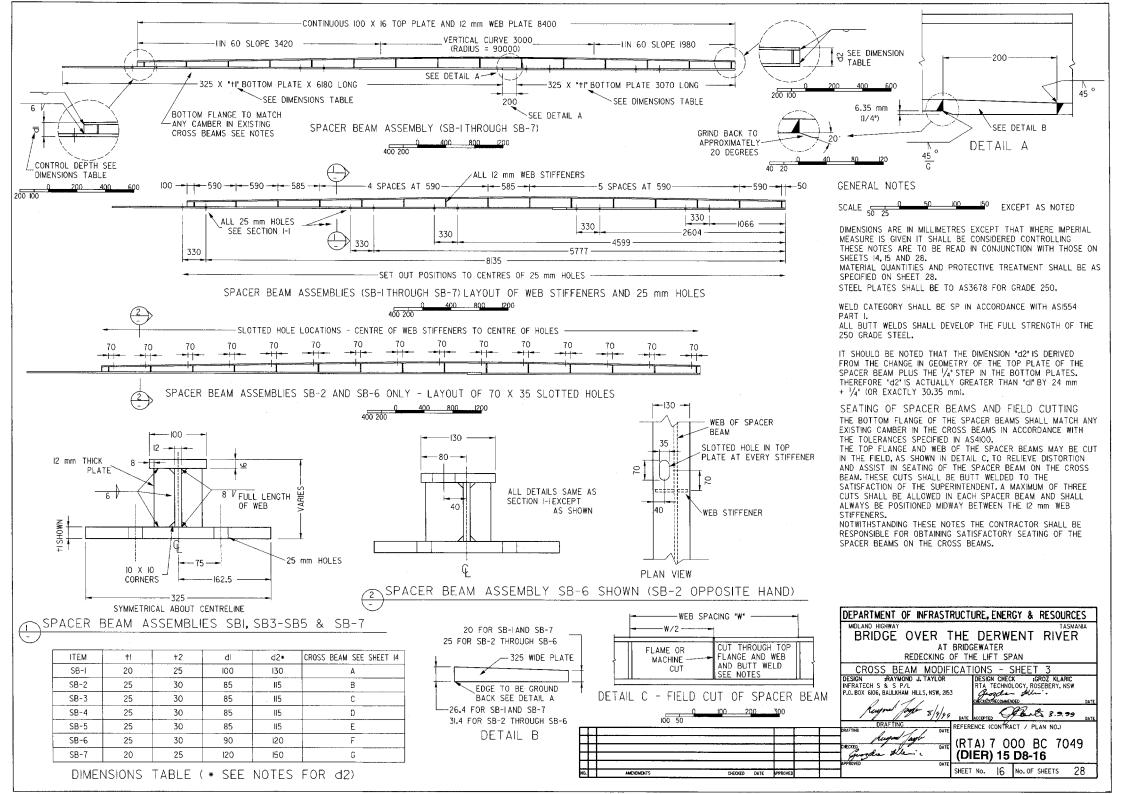


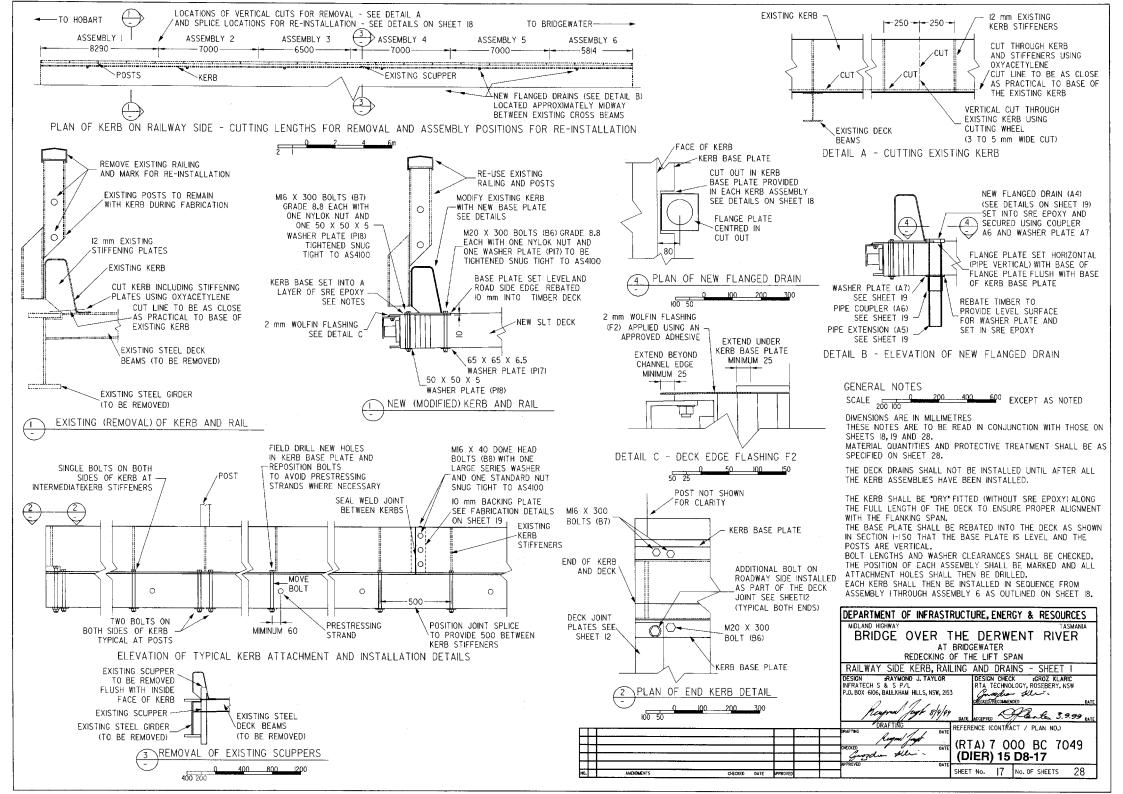


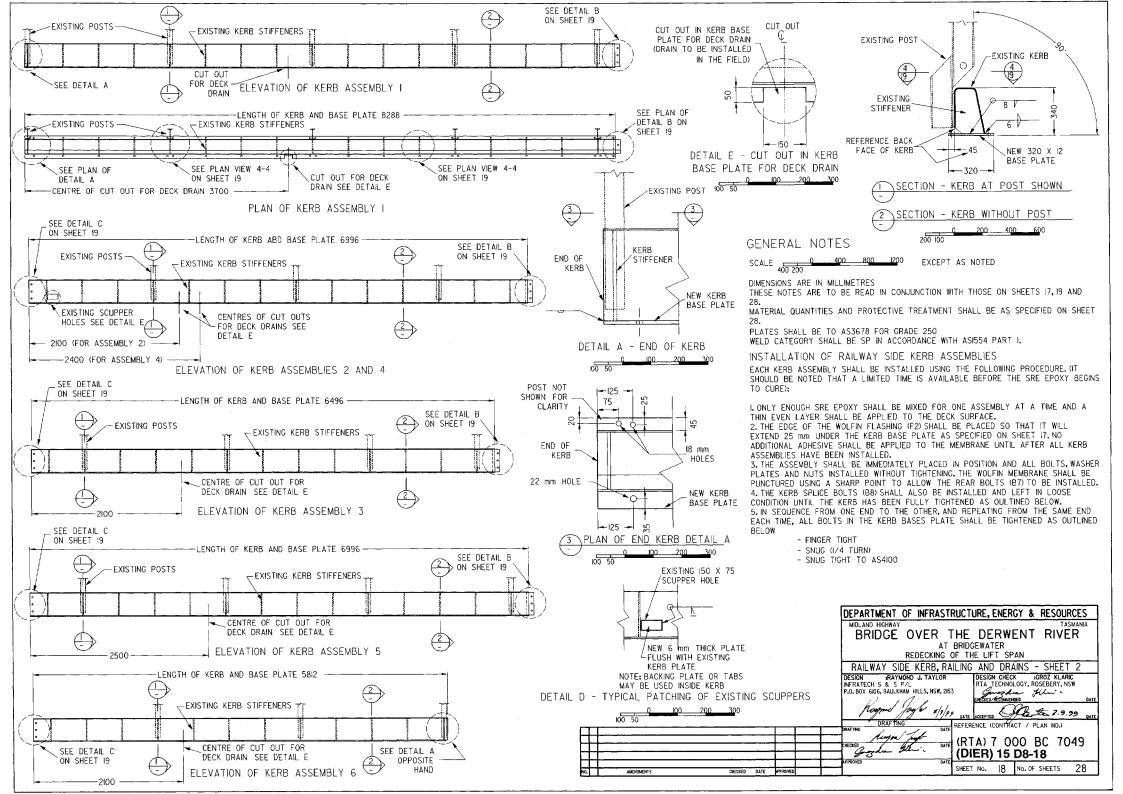


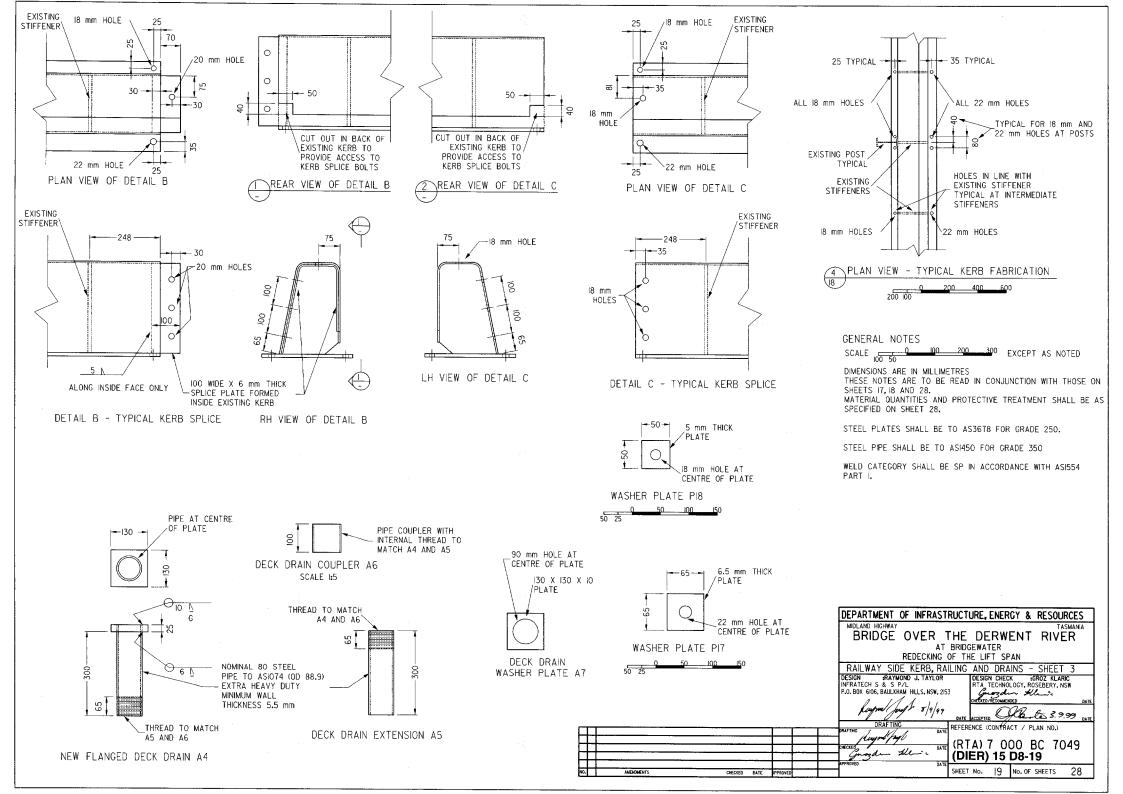


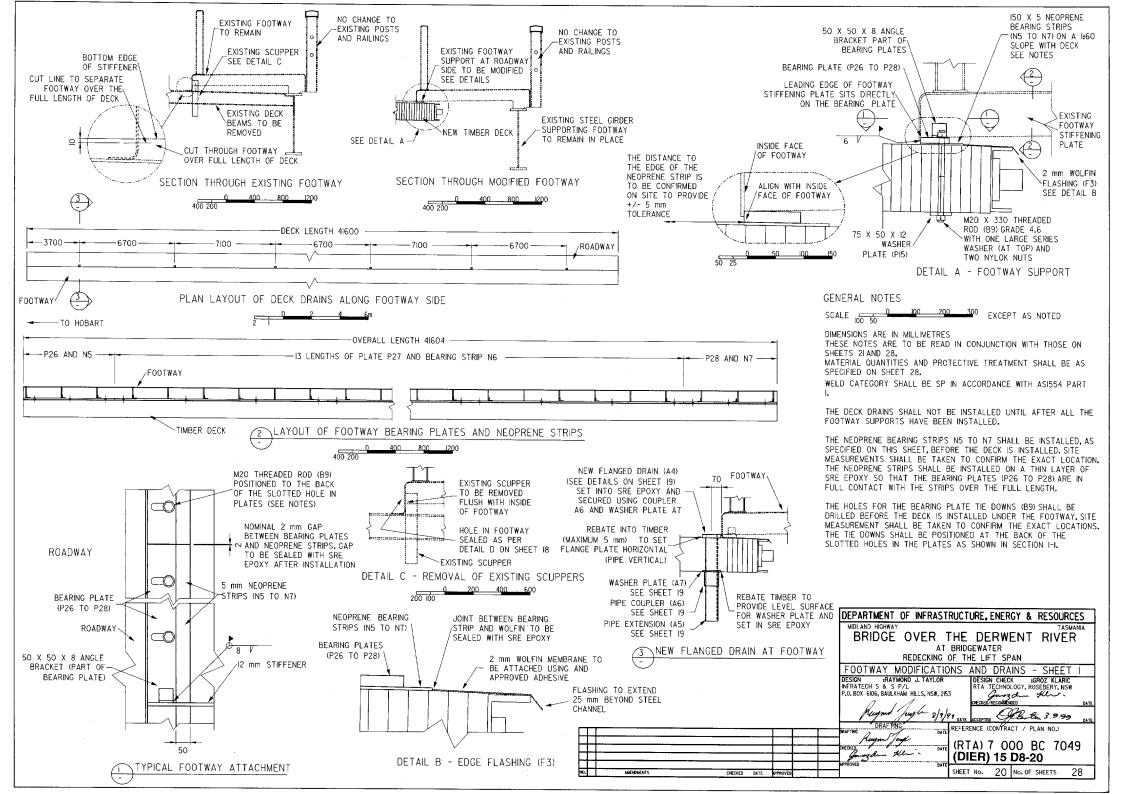


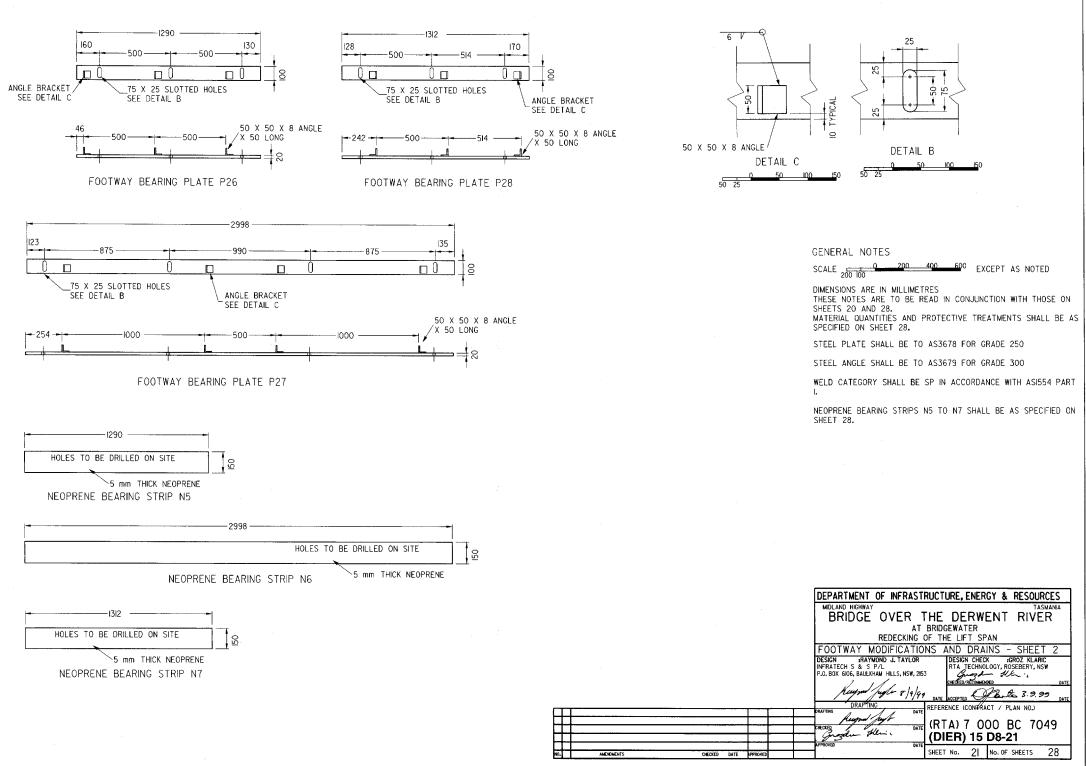


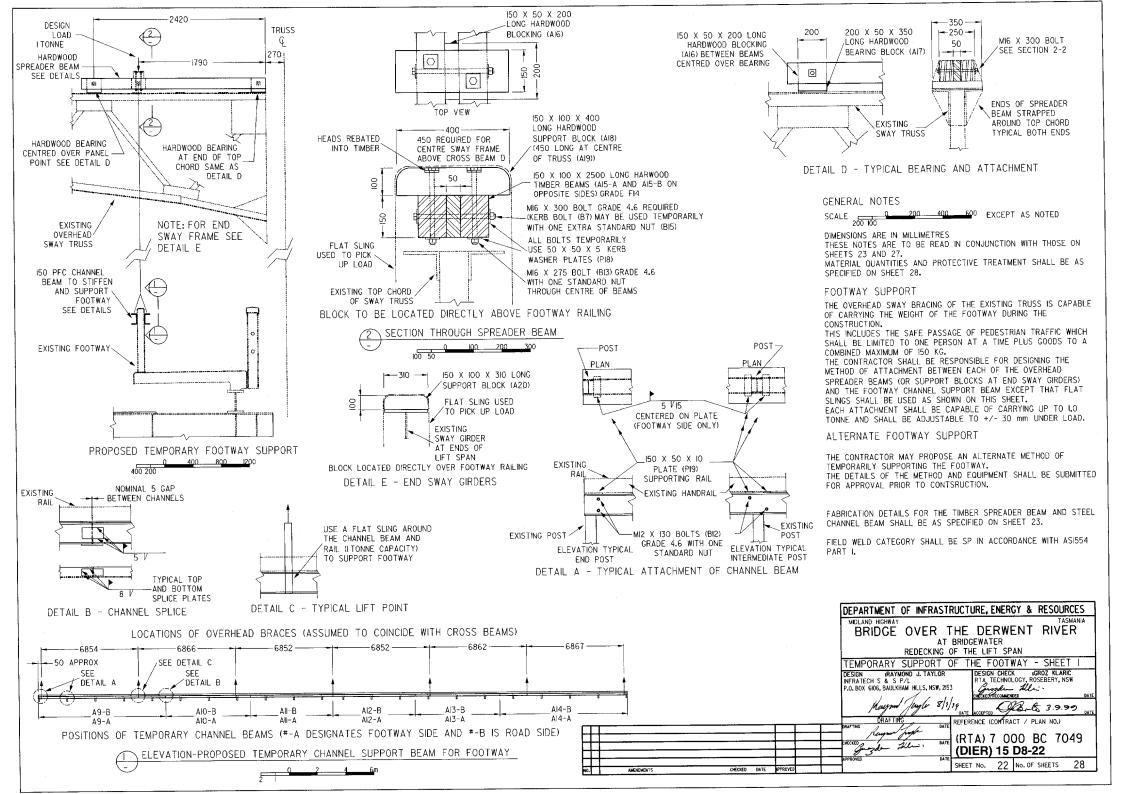


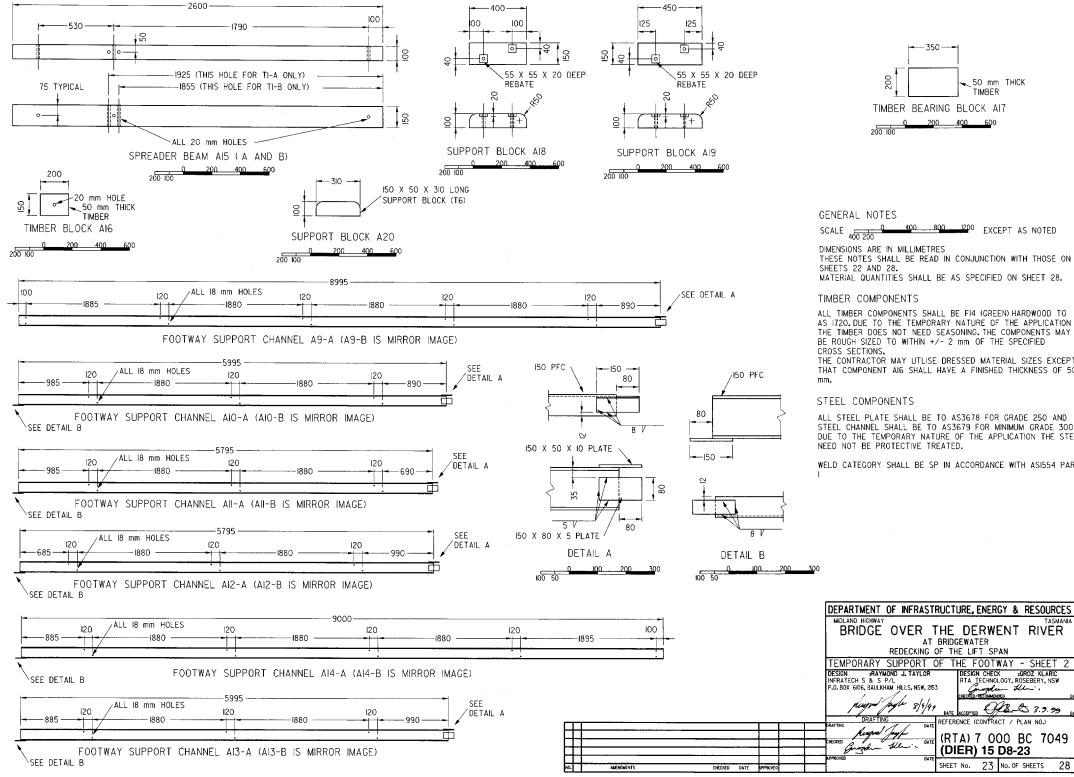












-350 50 mm THICK TIMBER TIMBER BEARING BLOCK AI7

200 EXCEPT AS NOTED

DIMENSIONS ARE IN MILLIMETRES THESE NOTES SHALL BE READ IN CONJUNCTION WITH THOSE ON

MATERIAL QUANTITIES SHALL BE AS SPECIFIED ON SHEET 28.

ALL TIMBER COMPONENTS SHALL BE FI4 (GREEN) HARDWOOD TO AS 1720. DUE TO THE TEMPORARY NATURE OF THE APPLICATION THE TIMBER DOES NOT NEED SEASONING. THE COMPONENTS MAY BE ROUGH SIZED TO WITHIN +/- 2 mm OF THE SPECIFIED THE CONTRACTOR MAY UTLISE DRESSED MATERIAL SIZES EXCEPT THAT COMPONENT AIG SHALL HAVE A FINISHED THICKNESS OF 50

ALL STEEL PLATE SHALL BE TO AS3678 FOR GRADE 250 AND STEEL CHANNEL SHALL BE TO AS3679 FOR MINIMUM GRADE 300. DUE TO THE TEMPORARY NATURE OF THE APPLICATION THE STEEL NEED NOT BE PROTECTIVE TREATED.

WELD CATEGORY SHALL BE SP IN ACCORDANCE WITH ASI554 PART

DESIGN CHECK

REFERENCE (CONTRACT / PLAN NO.)

(DIER) 15 D8-23

DATE ACCEPTE

SHEET No.

RTA TECHNOLOGY, ROSEBERY, NSW

(RTA) 7 000 BC 7049

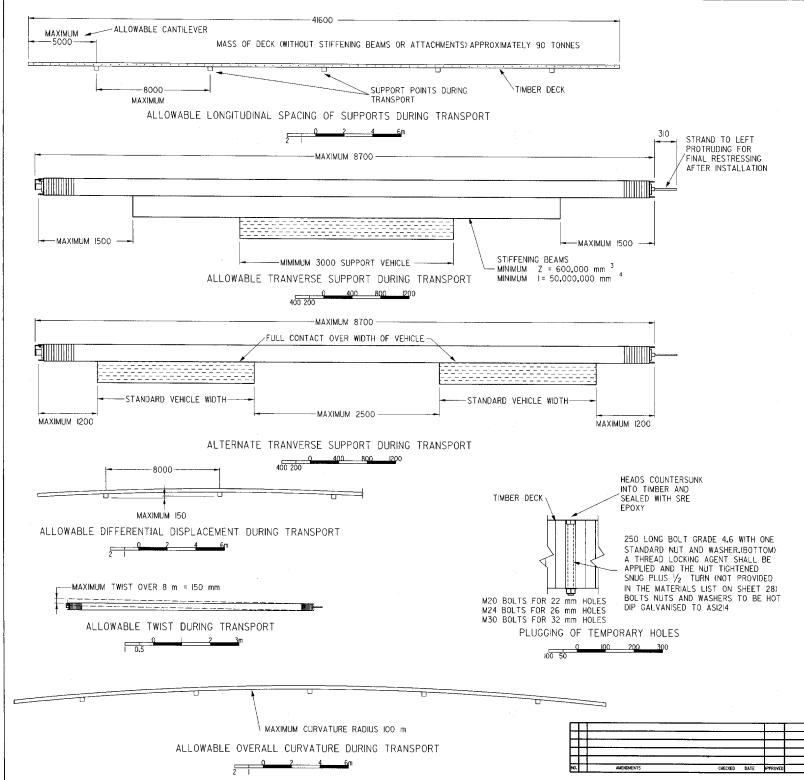
23 NO. OF SHEETS

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GROZ KLARIC



GENERAL NOTES

SCALES AS SHOWN DIMENSIONS ARE IN MILLIMETRES THESE NOTES ARE TO BE READ IN CONJUNCTION WITH THOSE ON SHEETS 25 THROUGH 28. THE TEMPORARY MATERIALS SHOWN ON THIS SHEET ARE NOT PROVIDED IN THE MATERIALS LIST ON SHEET 28.

THE CONTRACTOR SHALL BE RESPONSIBLE FOR DESIGNING THE METHOD OF LOADING, TRANSPORT AND UNLOADING FOR THE NEW TIMBER DECK FROM THE ASSEMBLY AREA TO THE FLANKING SPAN READY FOR LAUNCHING.

NOTWITHSTANDING THE DETAILS PROVIDED ON SHEETS 24 THROUGH 27 THE CONTRACTOR SHALL ASSESS THE LAUNCHING AND INSTALLATION METHOD TO ENSURE THEY ARE ACCEPTABLE FOR HIS PURPOSES. THE DETAILS OF THE METHOD AND EQUIPMENT SHALL BE SUBMITTED FOR APPROVAL.

DECK SUPPORT DURING TRANSPORT

DURING LOADING, TRANSPORT AND UNLOADING THE DECK SHALL BE SUPPPORTED ALONG ITS LENGTH AT INTERVALS OF NOT MORE THAN 8 m WITH END CANTILEVERS OF NOT MORE THAN 5 m.

EXCEPT AS NOTED BELOW, EACH OF THESE SUPPORTS SHALL BE CONTINUOUS OVER THE WIDTH OF THE DECK EXCEPT THAT THE EDGE OF THE DECK SHALL NOT CANTILEVER MORE THAN 1.5 m. WHERE A STEEL BEAM IS USED, COMBINED WITH A SUPPORT VEHICLE WIDTH OF 3 m, THE RECOMMENDED MINIMUM SECTION PROPERTIES OF THE BEAM SHALL BE AS SPECIFIED ON THIS SHEET. A SINGLE SUPPORT VEHICLE WIDTH OF LESS THAN 3 m IS NOT RECOMMENDED IN ORDER TO MAINTAIN STABILITY.

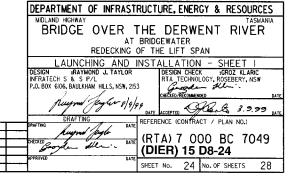
WHERE TWO VEHICLES (SIDE BY SIDE) ARE USED THE TRANSVERSE SUPPORTS MAY BE PROVIDED IN TWO LENGTHS AS SHOWN ON THIS SHEET. THE DECK NEED NOT BE TRANSVERSLEY STIFFENED.

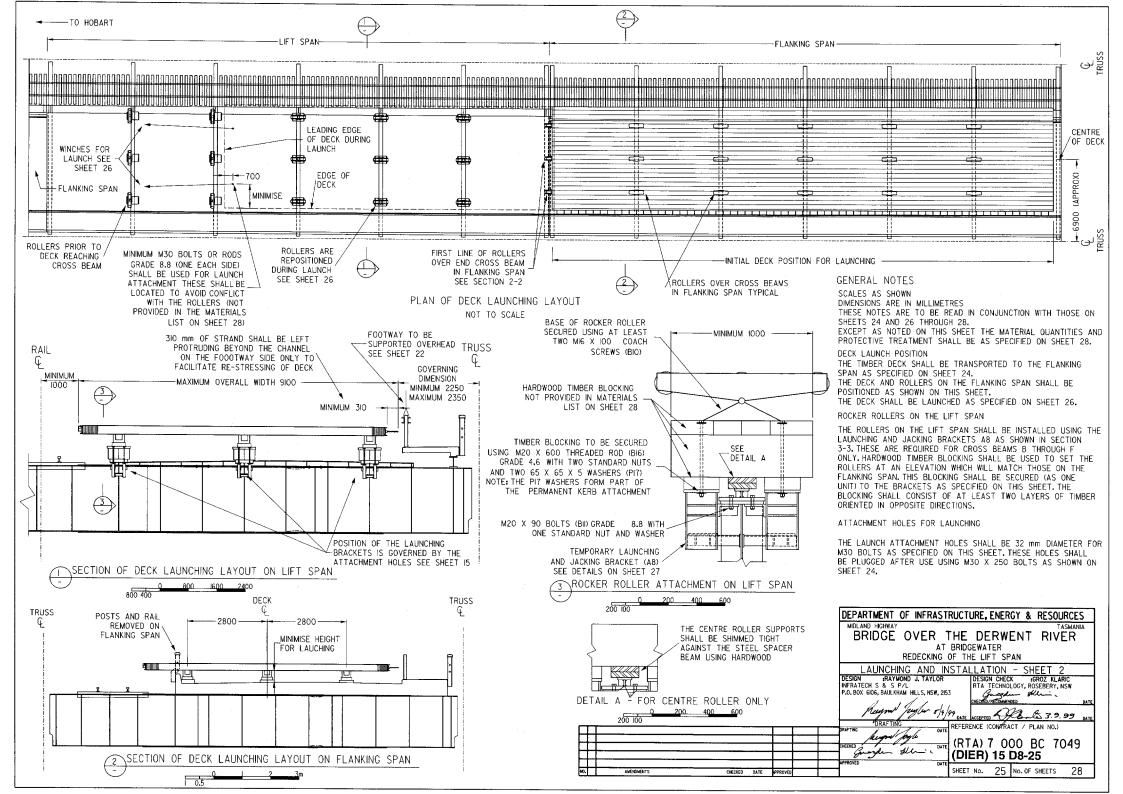
ADDITIONAL TEMPORARY DECK ATTACHMENTS FOR LIFTING

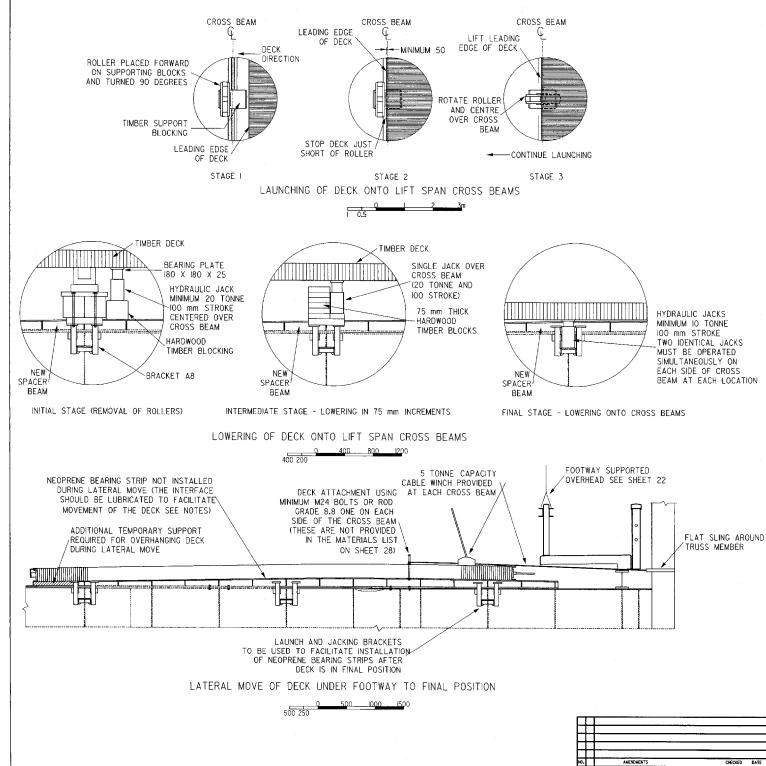
ATTACHMENTS FOR LIFTING DEVICES MAY BE INSTALLED BY DRILLING HOLES OF NOT MORE THAN 22 mm DIAMETER THROUGH THE TIMBER DECK. THESE HOLES SHALL NOT BE CLOSER THAN 100 mm TO ANY PRESTRESSING STRAND AND SHALL BE PLUGGED AFTER USE WITH AN M20 X 240 BOLT AS SHOWN ON THIS SHEET. THE LOCATION OF THESE HOLES SHALL NOT CONFLICT WITH PERMANENT ATTACHMENTS OR SUPPORTS.

ALLOWABLE DEFORMATIONS DURING TRANSPORT

THE NEW TIMBER DECK IS STRONG AND FLEXIBLE AND DOES NOT NEED TO BE TRANPORTED IN A LEVEL PLANE. DURING LOADING, TRANSPORT AND UNLOADING THE DECK CAN SUSTAIN DIFFERENTIAL AND TORSIONAL DEFORMATIONS WITHIN THE LIMITS SPECIFIED ON THIS SHEET.







GENERAL NOTES

SCALES AS SHOWN DIMENSIONS ARE IN MILLIMETRES

THESE NOTES ARE TO BE READ IN CONJUNCTION WITH THOSE ON SHEETS 23, 24, 27 AND 28

EXCEPT FOR THE LAUNCH AND JACKING BRACKET (A8) NONE OF THE TEMPORARY MATERIALS OR EQUIPMENT ARE PROVIDED IN THE MATERIALS LIST ON SHEET 28.

WINCHES FOR LAUNCHING

TWO WINCHES (5 TONNE CAPACITY) OR EQUIVALENT SHALL BE USED TO PULL THE DECK ONTO THE LIFT SPAN.

ATTACHMENT OF THE WINCHES TO THE DECK SHALL BE AS SPECIFIED ON SHEET 25.

THE PROPOSED METHOD AND EQUIPMENT DETAILS SHALL BE SUBMITTED FOR APPROVAL BEFORE THE BRIDGE IS CLOSED TO TRAFFIC.

ALLIGNMENT AND CLEARANCES DURING LAUNCH

ALL ROLLERS ON THE FLANKING SPAN SHALL BE PROPERLY ALIGNED TO ENSURE THAT THE DECK RUNS PARALLEL TO THE BRIDGE. CLEARANCES AND ALIGNMENT SHALL BE CHECKED AFTER THE FIRST 3 m OF LAUNCH AND SUBSEQUENTLY AFTER THE LEADING EDGE OF THE DECK

REACHES EACH CROSS BEAM. IF NECESSARY THE ROLLERS MAY BE ROTATED SLIGHTLY TO ASSIST IN

RE-ALIGNING THE DECK. THE ALIGNMENT OF THE DECK SHALL BE CLOSELY CHECKED AT THE END

OF THE LAUNCH.

POSITIONING ROLLERS AT CROSS BEAMS DURING LAUNCH

AT EACH CROSS BEAM THE LEADING EDGE OF THE DECK SHALL PASS AT LEAST 50 mm BEYOND THE CENTRE LINE OF THE CROSS BEAM. THE LEADING EDGE OF THE DECK SHALL THEN BE LIFTED SLIGHTLY TO ALLOW THE REPOSITIONING OF THE ROLLERS AS SHOWN ON THIS SHEET. THE LAUNCH CAN THEN CONTINUE TO THE NEXT CROSS BEAM.

LOWERING DECK ONTO CROSS BEAMS

THE LOWERING OF THE DECK SHALL BE PERFORMED IN STAGES AS SHOWN IN THE DIAGRAMS OF THIS SHEET.

EACH STAGE SHALL BE PERFORMED SIMULTANEOUSLY AT EACH OF THE THREE JACKING LOCATIONS ON A CROSS BEAM.

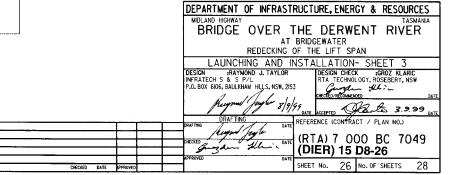
THE DECK MAY BE LOWERED AT ALL CROSS BEAMS SIMULTANEOUSLY OR AT ONE CROSS BEAM AT A TIME.REGARDLESS OF THE METHOD CHOSEN THE DIFFERENTIAL DISPLACEMENT OR DEFORMATION OF THE DECK SHALL NOT EXCEED THE LIMITS SPECIFIED ON SHEET 24.

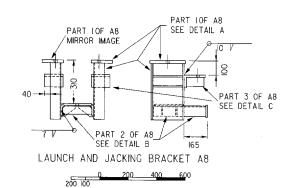
LATERAL MOVE OF DECK TO FINAL POSITION

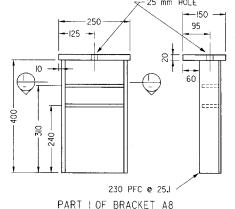
THE LATERAL MOVE OF THE DECK TO ITS FINAL POSTION UNDER THE FOOTWAY SHALL BE PERFORMED AS DETAILED IN THE DIAGRAM ON THIS SHEET.

THE NEOPRENE BEARING STRIPS (N2) SHALL NOT BE INSTALLED UNTIL AFTER THE MOVE IS COMPLETED. THE INTERFACE BETWEEN THE DECK AND THE CROSS BEAM SHOULD BE LUBRICATED. A THIN STRIP OF OILED TIMBER OR PLYWOOD (CONTINUOUS UNDER THE DECK) IS RECOMMENDED. STOPS SHOULD BE FIXED TO THE TOPS OF THE CROSS BEAMS UNDER THE FOOTWAY TO PREVENT THE DECK FROM MOVING PAST THE DESIRED LOCATION. LOOSE SPACERS SHOULD BE USED BETWEEN THE ENDS OF THE DECK AND THE FLANKING SPANS TO MAINTAIN THE DESIRED GAP AT THE DECK JOINTS.

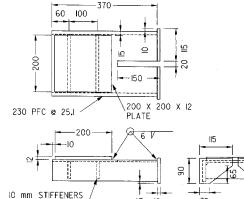
THE TEMPORARY HOLES FOR THE M24 BOLTS SHALL BE PLUGGED AFTER USE WITH M24 X 250 BOLTS AS SHOWN ON SHEET 24.





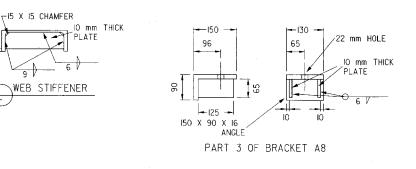


9



35 5.10 SEE SECTION I-I

PART 2 OF BRACKET A8



GENERAL NOTES

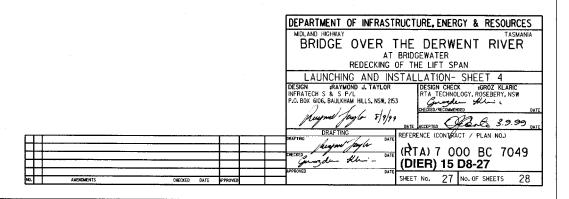
SCALE 300 EXCEPT AS NOTED

DIMENSIONS ARE IN MILLIMETRES THESE NOTES ARE TO BE READ IN CONJUNCTION WITH THOSE ON SHEETS 24 TO 26 AND 28.

MATERIALS QUANTITIES SHALL BE AS SPECIFIED ON SHEET 28

ALL STEEL PLATE SHALL BE TO AS3678 FOR GRADE 250 AND STEEL CHANNEL SHALL BE TO ASII63 FOR MINIMUM GRADE 300. DUE TO THE TEMPORARY NATURE OF THE APPLICATION THE STEEL NEED NOT BE PROTECTIVE TREATED.

WELD CATEGORY SHALL BE SP IN ACCORDANCE WITH ASI554 PART I.



😴 25 mm HOLE

ITEM	DESCRIPTION		SHEET	FABRIC	QUANT	EXTRA	TOTAL
			REF	SHEET	REQ'D	UNITS SUGG	QUANT
PI	150 X 150 X 25 ANCHORAGE PLATES		- 3	4	138	0	138
P2	90 mm DIAMETER X 40 WASHER PLATES	-	10 &11	1	210	2	212
P3	100 X 50 X 16 WASHER PLATE		10 &11	1	210	2	212
P4	TIE DOWN CLIP PLATE		0		156	0	156
P6	TIE DOWN CLIP PLATE		- 10		12	0	13
P7	TIE DOWN WASHER PLATE			н 	28	0	12
P8	TIE DOWN WASHER PLATE		Ĩ	H	20	Ó	2
P9	100 X 50 X 1535 JOINT PLATE		12	13		Ő	ī
PIO	100 X 50 X 1535 JOINT PLATE		12	13	2	0	2
PII PI2	100 X 50 X 1485 JOINT PLATE		12		4	0	4
PI3	100 X 50 X 1535 JOINT PLATE		12	13	~	0	
PI4	100 X 50 X 1660 JOINT PLATE		12	13	~ <u>_</u>	ŏ	
PI5	75 X 50 X 12 WASHER PLATE		12,20	13	120	Ĭ	121
PI6	45 X 45 X 12 WASHER PLATE		2	13	40		41
P17 P18	65 X 65 X 6.5 WASHER PLATE (SEE NOTE) 50 X 50 X 5 WASHER PLATE (SEE NOTE)		7	19	4	2	116
P19	150 X 50 X 10 TEMPORARY SUPPORT PLATE	F	22	19 N/A	42	2	44
P20	325 X 20 X 6170 BOTTOM FLANGE PLATE		15	15	2	0	2
P2I	TAPERED BOTTOM FLANGE PLATE		15	15		Ō	2
P22	325 X 20 X 3070 BOTTOM FLANGE PLATE		15	15	2	0	2
P23	325 X 25 X 6170 BOTTOM FLANGE PLATE		15	15	5	0	5
P24 P25	TAPERED BOTTOM FLANGE PLATE 325 X 25 X 3070 BOTTOM FLANGE PLATE		15	15	5	0	5
P26	100 X 20 X 1290 BEARING PLATE		15 20	15 21	5	0	5
P27	100 X 20 X 2998 BEARING PLATE		20	21	13	Ö	13
P28	100 X 20 X 1312 BEARING PLATE		20	21	Ĩ	Ö	1
Al	150 X 90 X 8 PROTECTION ANGLE		3	4	7	0	7
A2	150 X 90 X 8 PROTECTION ANGLE		3	4		Ó	1
A3 A4	ISO X 90 X 8 PROTECTION ANGLE		3	4	1	0	12
A4 A5	DECK DRAIN EXTENSION PIPE		17,20	19	12 12	0	12
A6	DECK DRAIN COUPLER	-	17,20	19	12	0	12
A7	DECK DRAIN WASHER PLATE		17,20	19	12	0	12
<u>A8</u>	TEMPORARY LAUNCH & JACKING BRACKET		25	27	30	0	30
A9-A	150 X 75 PFC TEMPORARY SUPPORT BEAM		22	23		0	1
A9-B AIO-A	150 X 75 PFC TEMPORARY SUPPORT BEAM 150 X 75 PFC TEMPORARY SUPPORT BEAM		22	23		0	
AIO-B	150 X 75 PFC TEMPORARY SUPPORT BEAM 150 X 75 PFC TEMPORARY SUPPORT BEAM		22	23		0	1
All-A	150 X 75 PFC TEMPORARY SUPPORT BEAM	-	22	23		0	
All-B	150 X 75 PFC TEMPORARY SUPPORT BEAM		22	23	1	0	1
AI2-A	150 X 75 PFC TEMPORARY SUPPORT BEAM		22	23	1	0	1
AI2-B	150 X 75 PFC TEMPORARY SUPPORT BEAM		22	23	<u> </u>	0	1
AI3-A AI3-B	150 X 75 PFC TEMPORARY SUPPORT BEAM 150 X 75 PFC TEMPORARY SUPPORT BEAM		22	23 23	<u>_</u>	0	
AI4-A	150 X 75 PFC TEMPORARY SUPPORT BEAM		22	23	1	0	
AI4-B	150 X 75 PFC TEMPORARY SUPPORT BEAM		22	23		Ő	
AIS-A	150 X 100 X 2600 TEMPORARY TIMBER BEA		22	23	5	Ö	5
AI5-B	150 X 100 X 2600 TEMPORARY TIMBER BEA		22	23	5	0	5
A16 A17	150 X 50 X 200 TEMPORARY TIMBER BLOCK 200 X 50 X 350 TEMPORARY TIMBER BEAR		22 22	23	15	0	15
AIS	150 X 100 X 400 TEMPORARY TIMBER SUPPORT BLO	ING ING	22	23 23	4	0	10
AI9	150 X 100 X 450 TEMPORARY TIMBER SUPPORT BLO	CK	22	23	1	0	1
A20	150 X 100 X 310 TEMPORARY TIMBER SUPPORT BLOC	ж	22	23	2	Ő	2
CI	230 X 75 X 4795 PFC ANCHORAGE CHANNE	L	3	4	7	0	7
<u>C2</u>	230 X 75 X 4275 PFC ANCHORAGE CHANNEL		3	4		0	<u> </u>
C3 C4	230 X 75 X 495 PFC ANCHORAGE CHANNEL 230 X 75 X 3680 PFC ANCHORAGE CHANNE		3	4	8	0	8
<u> </u>	230 X 75 X 4275 PFC ANCHORAGE CHANNE		3	4		0	
C6	230 X 75 X 3680 PFC ANCHORAGE CHANNE		3	4	1	0	r
SB-I	FABRICATED STEEL SPACER BEAM		15	16	1	0	
SB-2	FABRICATED STEEL SPACER BEAM		15	16		0	
SB-3 SB-4	FABRICATED STEEL SPACER BEAM		15 15	16		0	<u>-</u>
5B-5	FABRICATED STEEL SPACER BEAM	-+	15	16 16	1	0	
SB-6	FABRICATED STEEL SPACER BEAM		15	16		0	1
<u>SB-7</u>	FABRICATED STEEL SPACER BEAM		15	16		0	1
VI	15.2 mm PRESTRESSING STRAND X 10000		3	-	69		70
V2 V3	THREADED ANCHORAGE BARREL FOR 15.2 STRA	AND	3		138 138	2	140
V4	25 mm X 400 PVC SLEEVE		3		138	4	142
V5	THREADED NYLON PROTECTIVE CAP		3	-	138	2	40
Ni	100 X 50 X 5 NEOPRENE WASHER		10,1	11	210	4	214
N2	100 X 15 X 8400 NEOPRENE STRIP BEARING		10,1		5	0	5
N3	MINIMUM LENGTHS 1500 130 X 15 X 8400 NEOPRENE STRIP BEARING			-	_		L ~
	MINIMUM LENGTHS 1500		10, 1	-	2	0	2
N4	40 mm DIAMETER X 3 mm NEOPRENE WASHER		12	-	102	8	10
N5	150 X 5 X 1290 NEOPRENE STRIP BEARING		20	21		0	
N6	150 X 5 X 2998 NEOPRENE STRIP BEARING		20	21	13	0	13
<u>N7</u> Fl	150 X 5 X 1312 NEOPRENE STRIP BEARING 300 X 2 mm THICK X 9000 WOLFIN FLASH	INC +	20 12	21	2	0	
F2	180 X 2 mm THICK X 42000 WOLFIN FLASHING		17	-	<u> </u>	0	2
F3	250 X 2 mm THICK X 42000 WOLFIN FLASHING	G	20	-		0	
GREASE	KPXT GREASE (SEE NOTES)		3		400	LITRES	
EPOXY	SRE BITUMEN EPOXY (FINISHED VOLUME)		MULTIPLE		130	LITRES	
						L	L
SHEET REF						G FABRI	
QUANT REC		IRA UN	ITS SUGG	SUGGE	STED E	KTRA UN	ITS
TOTAL QUANT		T GR			AL GRA		D
LARGE WAS		LOK 1	WASH NUT	NYLOK	NIT	S WASHE	<u>'</u> 11
							-

NOTES ON MATERIALS ALL BOLTS, THREADED ROD AND ASSOCIATED NUTS SHALL BE TO ASIIIFOR GRADE 4.6 OR ASI252 FOR GRADE 8.8 AS NOTED IN THE TABLE. ALL BOLTS, COACH SCREWS AND ASSOCIATED NUTS AND WASHERS. (EXCEPT AS NOTED BELOW) SHALL BE HOT DIP GALVANISED TO ASI2I4. ITEMS BIO, BI2, BI3, BI5 AND BI6 SHALL NOT BE PROTECTIVE TREATED, ALL STEEL PLATES AND SECTIONS SHALL BE TO AS3678 AND AS3679 COINCIDENT WITH THE PERMANENT CROSS BEAM SUPPORTS AS WELL RESPECTIVELY FOR THE GRADES SPECIFIED ON THE (FABRICATION) SHEETS REFERENCED IN THE TABLE. ALL STEEL PLATES AND SECTIONS (EXCEPT AS NOTED BELOW) SHALL BE HOT DIP GALVANISED TO ASI650. ALL EDGES TO BE PROTECTIVE TREATED SHALL BE ROUNDED TO A RADIUS OF 1.5 mm. ALL STEEL PLATES AND SECTIONS FOR TEMPORARY USE SPECIFIED ON LEAST 100 mm. SHEETS 22 THROUGH TO 27 SHALL NOT BE PROTECTIVE TREATED. PRESTRESSING STRAND SHALL BE 7 WIRE STRESS RELIEVED. HIGH TENSILE STEEL, SUPER GRADE, LOW RELAXATION TO ASI3I WITH ANCHORAGES TO ASI314, STRANDS SHALL BE GREASED AND SHEATHED BY THE MANUFACTURER AND THE MAXIMUM OUTSIDE DIAMETER OF THE SHEATH SHALL BE 19 mm. THE PRESTRESSING PROTECTION SYSTEM SPECIFIED ON SHEET 3. USING ITEMS V3 THROUGH V6 HAS BEEN DEVELOPED BY VSL PRESTRESSING AUSTRALIA P/L IN CONJUNCTION WITH THE ROADS AND LAMINATE REMAINS VERTICAL AND PROPERLY ALIGNED. TRAFFIC AUTHORITY (NSW) AND THE CONSULTANT. THIS SYSTEM HAS BEEN DEVELOPED SPECIFICALLY FOR USE IN STRESS LAMINATED TIMBER DECKS AND IS AVAILABLE FROM VSL PRESTRESSING P/L. THE DETAILS OF ALTERNATE PRESTRESSING AND PROTECTION SYSTEMS SHALL BE SUBMITTED FOR APPROVAL PRIOR TO CONSTRUCTION. SRE EPOXY SHALL BE SEMIRIGID EPOXY RESIN JOINT SEALER "SRE/R" MANUFACTURED BY CTI. TIMBER DECK LAMINATES SHALL BE AS SPECIFIED ON SHEETS 5 THROUGH 9. THE GREASE FOR INJECTION INTO THE VOIDS AROUND THE SHEATHED STRANDS, AS SPECIFIED ON SHEETS 3, SHALL BE CASTROL APXT OR FOUIVALENT. THE WOLFIN FLASHING SHALL BE 2 mm THICK AND ATTACHED TO THE DECK USING AN APPROVED COMPATIBLE ADHESIVE. NEOPRENE STRIP BEARINGS AND WASHERS NITO N3 AND N5 TO N7 SHALL BE IN ACCORDANCE WITH RTA QA SPECIFICATIONS B280 "UNREINFORCED ELASTOMERIC BEARING PADS AND STRIPS" AS PROVIDED IN THE CONTRACT DOCUMENTS. NEOPRENE WASHERS N4 MAY BE CUT FROM STANDARD NEOPRENE STRIP OR SHEET WHICH IS DESIGNATED AS SUITABLE FOR PETROL AND OIL APPLICATIONS. GENERAL NOTES THESE NOTES SHALL BE READ IN CONJUNCTION WITH THOSE ON ALL SHEETS AS WELL AS THE FOLLOWING ROADS AND TRAFFIC AUTHORITY (NSW) SPECIFICATIONS WHICH ARE CONTAINED IN THE CONTRACT DOCUMENTS: RTA FORM 2382 'TIMBER FOR BRIDGES, STRESS LAMINATED TIMBER DECKS, SUPPLY AND HANDLING' (JUNE 1995) RTA SPECIAL FORM 238I CONSTRUCTION OF STRESS LAMINATED TIMBER BRIDGE DECKS" (MARCH 12, 1999) RTA SPECIAL FORM 2115 'STRESSING OF STRESS LAMINATED TIMBER

DECK ASSEMBLY AREA

THE STRESS LAMINATED TIMBER DECK SHALL BE ASSEMBLED AND STRESSED TOGETHER OFF THE ROADWAY ON THE NORTH SIDE OF THE BRIDGE, THE SITE SHALL BE DESIGNATED BY THE DEPARTMENT OF INFRASTRUCTURE, ENERGY AND RESOURCES. THE ASSEMBLY BED SHALL BE DESIGNED TO SUPPORT 1.5 TIMES THE WEIGHT OF THE NEW TIMBER DECK (1.5 X 90 TONNES) IN ORDER TO ALLOW FOR THE NECESSARY MEN AND EQUIPMENT FOR ASSEMBLY AND STRESSING. THE ASSEMBLY BED SHALL HAVE SUPPORTS (CONTINUOUS ACROSS THE WIDTH OF THE DECK) WHICH ARE AS INTERMEDIATE SUPPORTS MIDWAY BETWEEN THESE, EACH OF THESE SUPPORTS SHOULD BE AT LEAST IO m LONG TO ALLOW FOR THE ADDITIONAL WIDTH OF THE LOOSE ASSEMBLY OF LAMINATES BEFORE STRESSING, EACH SUPPORT SHALL HAVE A SMOOTH TIMBER BEARING STRIP OR A SMOOTH STEEL BEARING WITH A WIDTH OF AT

CONSTRUCTION OF TIMBER DECK EXCEPT AS NOTED IN THE DRAWINGS AND THESE NOTES THE CONSTRUCTION OF THE DECK SHALL BE IN ACCORDANCE WITH RTA SPECIAL FORM 2381 (MARCH 12, 1999). I. THE DECK SHALL BE ASSEMBLED IN DECK SETS AS SPECIFIED FOR THE SELECTED OPTION FROM SHEETS 5 TO 8. 2. ALL LAMINATES SHALL BE NAILED AS OUTLINED IN RTA SPECIAL FORM 238I AND CARE SHALL BE TAKEN TO ENSURE THAT EACH 3. IT IS RECOMMENDED THE TOP SURFACE OF THE DECK BE MARKED FOR THE LOCATIONS OF THE FOLLOWING ITEMS AND NAILING BE OMITTED TO FACILITATE DRILLING FOR THOSE ITEMS:

- TIE DOWNS AT CROSS BEAMS (SHEET IO)
- KERB BOLTS (SHEET 17)
- DECK JOINTS BOLTS (SHEET 12)
- FOOTWAY SUPPORT BOLTS (SHEET 20)
- DECK DRAINS (SHEETS 18 AND 20)

4. THE ASSEMBLY OF THE DECK SHALL COMMENCE FROM THE RAILWAY SIDE AND THE STRANDS SHALL NOT BE INSTALLED UNTIL THE DECK IS FULLY ASSEMBLED. 5. THE GREASE INJECTION HOLES AS SPECIFIED IN RTA SPECIAL

FORM 2115 SHALL BE DRILLED IN EVERY 32ND LAMINATE RUN (1120 SPACING) ALONG EACH STRAND AS WELL AS IN THE OUTSIDE LAMINATE AS SHOWN ON SHEETS 5 TO 8. 6. THE PRESTRESSING STRANDS, PROTECTION SYSTEM AND ANCHORAGES SYSTEM SHALL BE INSTALLED AS SHOWN ON SHEET 3. 7. STRESSING OF THE DECK SHALL BE IN ACCORDANCE WITH RTA SPECIAL FORM 205 AND THE STRESSING NOTES ON THIS SHEET. 8. GREASING OF THE VOIDS USING THE HOLES SPECIFIED IN 5 ABOVE SHALL BE PERFORMED IMMEDIATELY AFTER THE STRESSING OF THE DECK IS COMPLETED AND THE HOLES SHALL BE PLUGGED IMMEDIATELY AS SPECIFIED ON SHEETS 5 TO 8 TO PREVENT

MOISTURE FROM ENTERING THE DECK. 9. SITE MEASUREMENTS SHALL BE TAKEN TO CONFIRM THE LOCATION OF THE RAILWAY SIDE KERB AND FOOTWAY SUPPORT BEARING. IO. REBATING FOR THE RAILWAY SIDE KERB SHALL BE PERFORMED AS SPECIFIED ON SHEET 17, BUT NO HOLES SHALL DRILLED. IL THE FOOTWAY SIDE NEOPRENE BEARINGS (N5 TO N7) SHALL BE FITTED AS SPECIFIED ON SHEET 20, THE HOLES FOR THE RODS (B9) SHALL BE DRILLED USING THE BEARING PLATES AS TEMPLATES. 12. NO ADDITIONAL DRILLING OR REBATING SHALL BE PERFORMED UNTIL THE DECK HAS BEEN LAUNCHED INTO PLACE.

CHECKED DATE

NPPROVE

STRESSING OF DECK

1. EXCEPT AS OUTLINED BELOW STRESSING SHALL BE PERFORMED IN ACCORDANCE WITH RTA SPECIAL FORM 215. 2. STRESSING SHALL ONLY BE PERFORMED UNDER THE DIRECTION OF THE DESIGN ENGINEER OR HIS DELEGATE. 3. A MAXIMUM NUMBER OF STRANDS SHALL BE STRESSED SIMULTANEOUSLY SUCH THAT THE FULL LENGTH OF THE DECK IS STRESSED DURING THE INITIAL STAGES. 4. UNLESS APPROVED OTHERWISE AT LEAST 10 JACKS SHALL BE USED AND THEY SHALL BE EVENLY DISTRIBUTED ALONG THE FULL LENGTH OF THE DECK. 5. THE GEOMETRY OF THE DECK SHALL BE CHECKED AS SPECIFIED IN RTA SPECIAL FORM 2115 OR ADDITIONALLY AS DIRECTED BY THE SITE ENGINEER. 6. THE OVERALL WIDTH SHALL BE CHECKED FOR CONFORMANCE WITH THE REQUIREMENTS ON SHEET 3 AFTER THE INITIAL STRESSING HAS BEEN COMPLETED. THE MEASUREMENT SHOULD ALLOW FOR ANOTHER 50 mm OF DECK COMPRESSION TO COMPLETE THE RE-STRESSING REQUIREMENTS SPECIFIED IN RTA SPECIAL FORM 205.

STRESSING NOTES

THE FOLLOWING SHALL BE OBSERVED FOR THE 15.2 mm PRESTRESSING STRANDS (FORCE PER STRAND):

. MINIMUM ULTIMATE STRENGTH = 250 KN 2. MAXIMUM PERMISSIBLE (DESIGN) JACKING FORCE = 210 KN 3. DESIGN FORCE AFTER TRANSFER = 175 KN MINIMUM STRAND FORCE = 100 KN

THE MINIMUM STRAND FORCE IS APPLICABLE FOR FUTURE LONG TERM MAINTENANCE. THE DECK SHALL BE RE-STRESSED WHEN THE RESIDUAL TENDON FORCES FALL TO THIS LEVEL.

PREPARATION AND INSTALLATION OF THE DECK

THE PROCEDURE FOR REMOVAL OF THE OLD DECKING. INSTALLATION OF SPACER BEAMS AND CROSS BEAM STRENGTHENING SHALL BE DESIGNED TO MINIMISE THE OVERALL ROAD CLOSURE PERIOD THE CONTRACTOR SHALL SUBMIT THE DETAILS OF THE PROPOSED METHOD AND EQUIPMENT, INCLUDING PROPOSED ROAD CLOSURE REQUIREMENTS, WITH THE TENDER SUBMISSION.

THE ROAD CLOSURE PERIOD AND QUALITY ASSURANCE. PROCEDURE FOR WELDING OF THE CROSS BEAMS SHALL FORM PART OF THE TENDER ASSESSMENT PROCESS. NOTWITHSTANDING THESE PROCEDURES A MAXIMUM 48 HOUR CLOSURE TO TRAIN TRAFFIC SHALL APPLY. THE NEW DECK WILL CONFLICT WITH THE RAILWAY CLEARANCES DURING TRANSPORT, LAUNCH AND INSTALLATION. THE INSTALLATION INCLUDING THE LATERAL MOVE UNDER THE FOOTWAY, IS TO BE COMPLETED WITHIN THE 48 HOUR WINDOW SPECIFIED ABOVE.

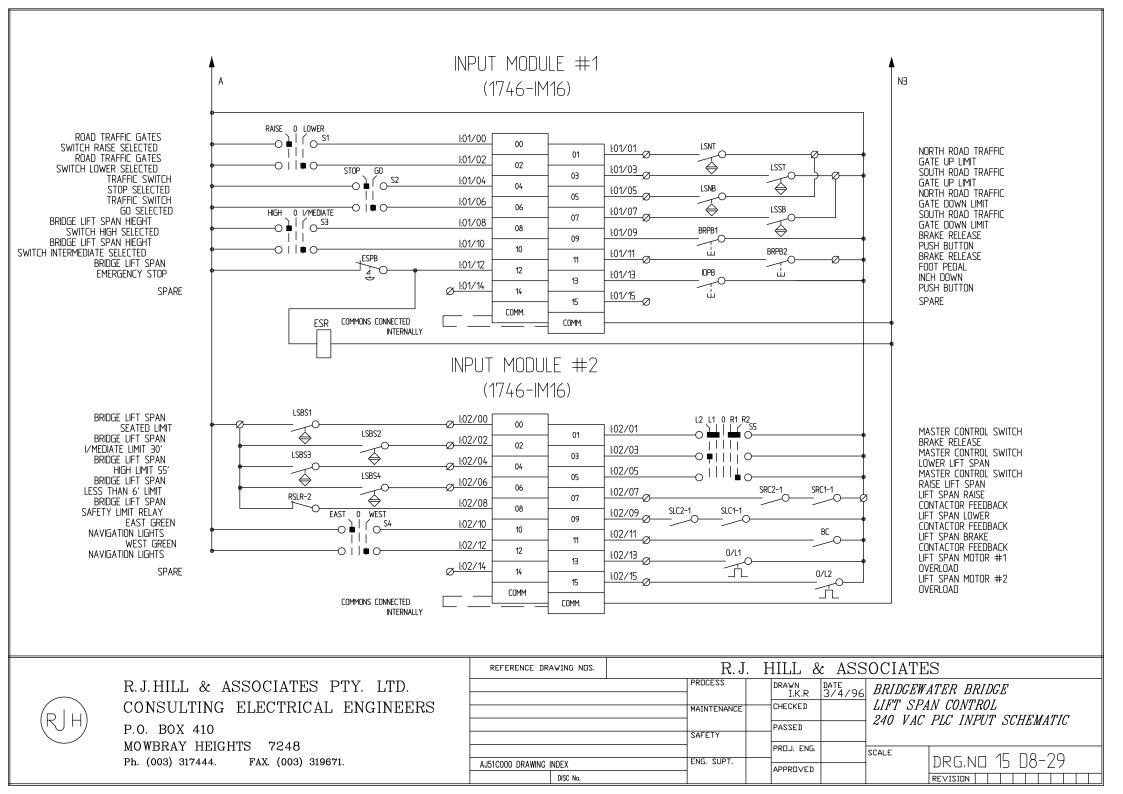
ADDITIONAL NOTES ON CROSS BEAM WELDING

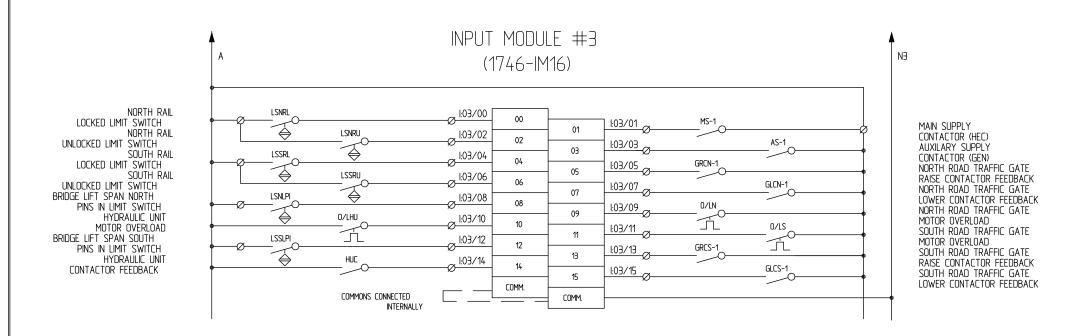
PRIORITY SHALL BE GIVEN TO INSTALLING AND BOLTING THE SPACER BEAMS AND LAUNCHING BRACKETS AS SPECIFIED ON SHEET IS TO FACILITATE LAUNCHING OF THE DECK. WELDING OF THE CROSS BEAMS AND BOTTOM FLANGE STRENGTHENING MAY BE PERFORMED DURING LAUNCHING AND INSTALLATION WITH THE FOLLOWING EXCEPTIONS. I NO SPACER BEAM OR BOTTOM FLANGE PLATE SHALL BE PARTIALLY WELDED WHEN THE DECK IS CANTILEVERED OVER THAT CROSS BEAM. 2. NO SPACER BEAM OR BOTTOM FLANGE PLATE SHALL BE PARTIALLY WELDED DURING THE PASSAGE OF TRAINS. 3. ALL WELDING SHALL BE COMPLETED BEFORE THE BRIDGE

IS RE-OPENED TO ROAD TRAFFIC.

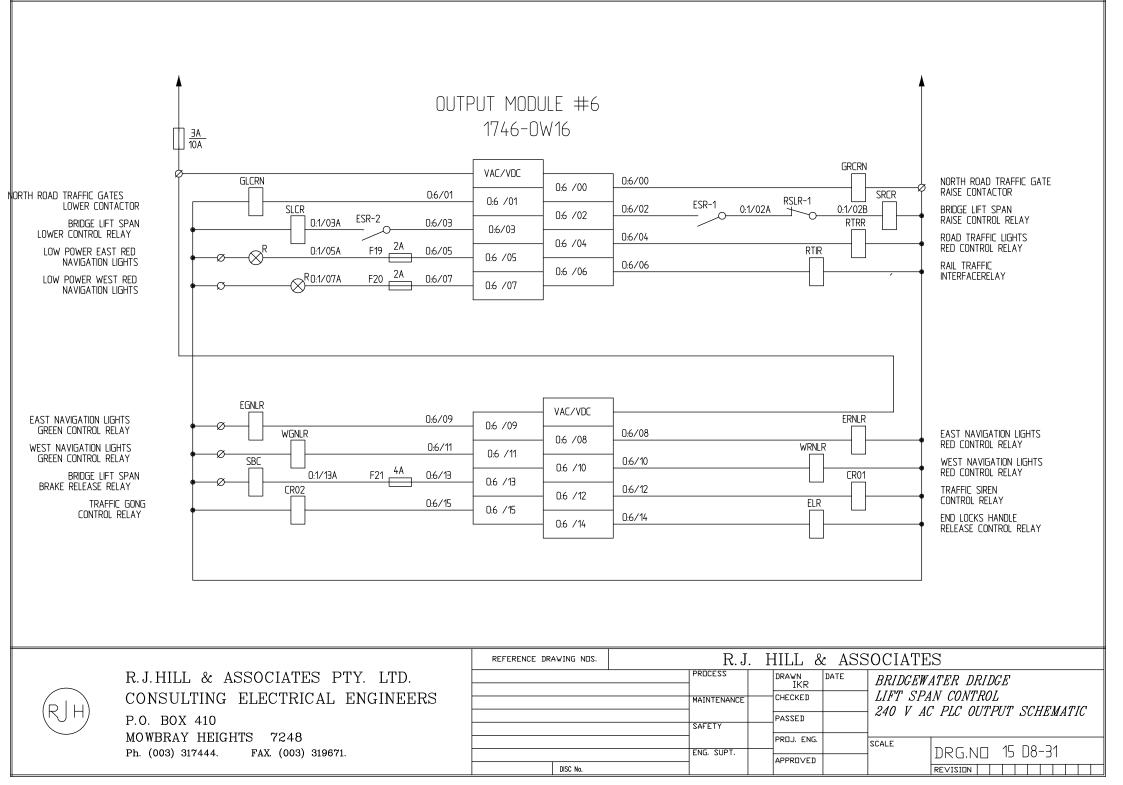
DEPARTMENT OF INFRAST	RUCTURE, ENERGY & RESOURCES
MIDLAND HIGHWAY	TASMANIA
BRIDGE OVER	THE DERWENT RIVER
	BRIDGEWATER
REDECKING	OF THE LIFT SPAN
	S AND CONSTRUCTION NOTES
DESIGN #RAYMOND J. TAYLOR INFRATECH S & S P/L P.O. BOX 6106, BAULKHAM HILLS, NSW, 215	DESIGN CHECK :GROZ KLARIC RTA TECHNOLOGY, ROSEBERY, NSW 53
Ruyne Juyle 8/9/	44 DATE ACCEPTED DATA 3.9.99 DAT
DRAFTING DRAFTING DATE	REFERENCE (CONTRACT / PLAN NO.)
CHECKED DATE	
APPROVED DATE	(DIER) 15 D8-28
1	SHEET No. 28 NO. OF SHEETS 28

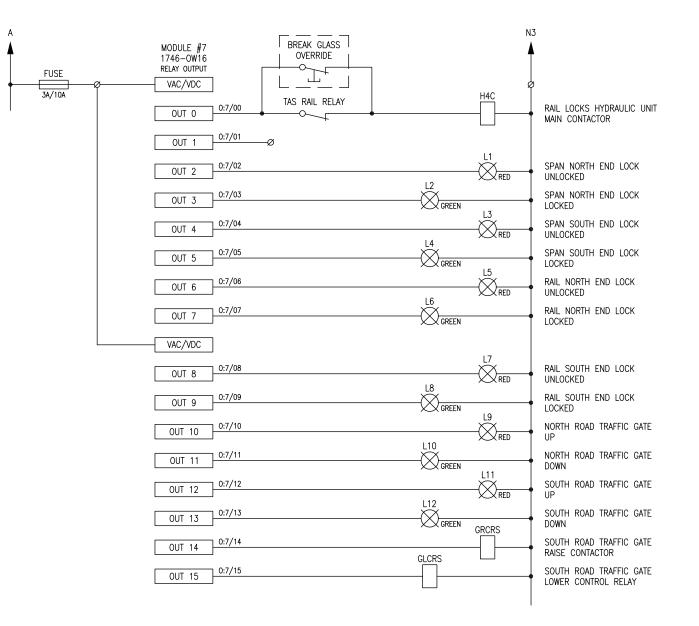
ITEM	DESCRIPTION	MAT	SHEET		* OF NI					EXTRA	TOTA
		GRADE	REFER	UNITS	STAND	LOCK	STAND	LARGE	NYLOK	UNITS	QUANT
			#	REQ'D	NUT	NUT	WASH	₩ASH	NUT	SUGG	UNITS
BI	MIO X 65 COACH SCREW	4.6	3	176						6	182
BI	M24 X 520 THREADED ROD	4.6	5	16						1	16
B2	MI6 NYLOK NUTS ONLY	4.6	3	52	-					0	52
B3	M20 X 350 THREADED ROD	8.8	10-11	210	2		2			2	212
84	M20 X 320 HEX HEAD BOLT	8.8	12	102	1	1				2	142
B5 *	M20 X 75 HEX HEAD BOLT	8.8	15	80	-	1				0	80
B6	M20 X 300 HEX HEAD BOLT	8.8	17	114						0	114
B7	MI6 X 300 HEX HEAD BOLT	8.8	17	14					1	1	115
B8	MI6 X 40 DOME HEAD BOLT	8.8	17	20	1			1		0	20
B9	M20 X 330 THREADED ROD	4.6	20	58				1	2	1	59
B10	MI6 X 100 COACH SCREW	4.6	25	30						2	32
B∥.●●	M20 X 90 HEX HEAD BOLT	8.8	15	60	1		- 1			1	61
BI2	MI2 X 130 HEX HEAD BOLT	4.6	22	44	1					1	45
BI3	MI6 X 275 HEX HEAD BOLT	4.6	22	10						0	10
BI4	MI2 X 75 COACH SCREW	4.6	5-8	552						8	560
BI5	M20 STANDARD NUT ONLY	4.6	22	15						0	15
BI6	M20 X 600 THREADED ROD	4.6	25	60	2					0	60
		50 mn 75 mr									



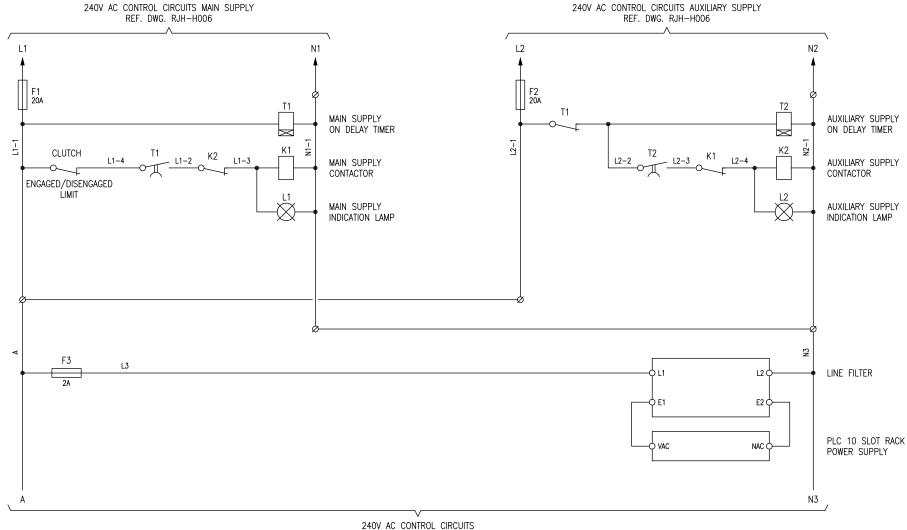


		REFERENCE DRA	WING NOS.	R. J.	. HI	LL &	: ASS	OCIATE	ES
\frown	R.J.HILL & ASSOCIATES PTY. LTD.		·	PROCESS	DR	awn I.K.R	date 3/4/96		WATER BRIDGE
	CONSULTING ELECTRICAL ENGINEERS			MAINTENANCE	СНЕ	ECKED			AN CONTROL S PLC INPUT SCHEMATIC
$J \overline{J}$	P.O. BOX 410			SAFETY	PAS	SSED		240 VAC	FLC INFUT SCHEMAITC
	MOWBRAY HEIGHTS 7248				PRI	DJ. ENG.		SCALE	
	Ph. (003) 317444. FAX. (003) 319671.	AJ51C000 DRAWING IN	ENG. SUPT.	APf	PROVED			DRG.ND 15 D8-30	



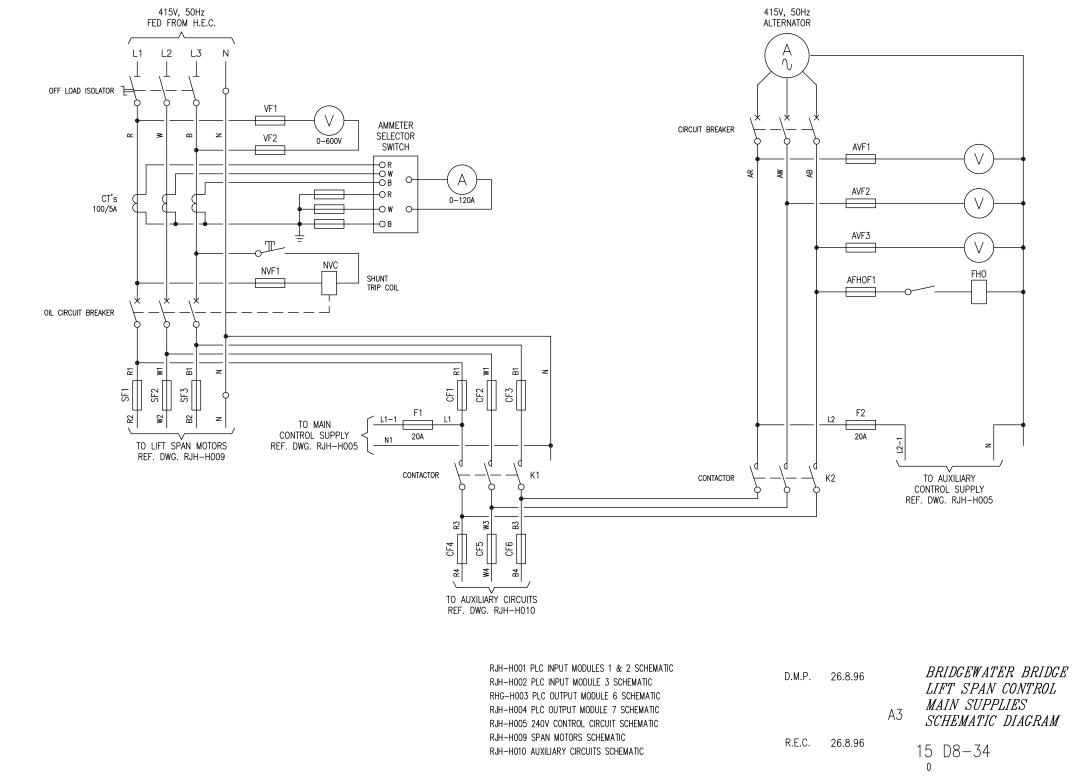


RJH-H001 PLC INPUT MODULES 1 & 2 SCHEMATIC RJH-H002 PLC INPUT MODULE 3 SCHEMATIC RJH-H003 OUTPUT MODULE 6 SCHEMATIC RJH-H005 240V CONTROL CIRCUIT SCHEMATIC	D.M.P.	26.8.96	۸ 7	BRIDGWATER BRIDGE LIFT SPAN CONTROL 240V PLC OUTPUT MODULE #7
RJH-H006 MAIN SUPPLIES SCHEMATIC			AJ	SCHEMATIC DIAGRAM
RJH-H007 240V AC CONTROLS SCHEMATIC RJH-H008 240V AC CONTROLS SCHEMATIC	R.E.C.	26.8.96	1	5 D8-32
			·	0

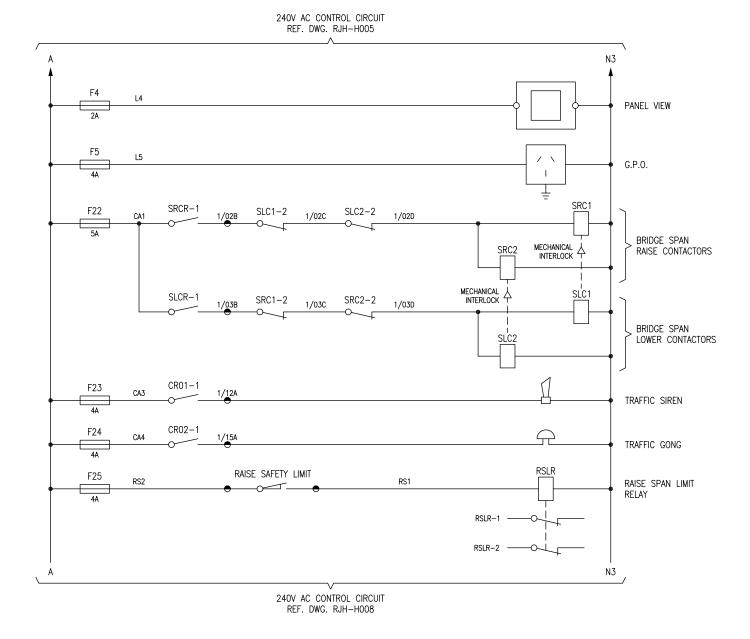


REF. DWG. RJH-H007

RJH-H001 PLC INPUT MODULES 1 & 2 SCHEMATIC RJH-H002 PLC INPUT MODULE 3 SCHEMATIC RJH-H003 PLC OUTPUT MODULE 6 SCHEMATIC RJH-H004 PLC OUTPUT MODULE 7 SCHEMATIC	D.M.P.	27.8.96	A3	BRIDGEWATER BRIDGE LIFT SPAN CONTROL 240V AC CONTROL CIRCUITS		
RJH-H006 MAIN SUPPLIES SCHEMATIC			AJ	SCHEMATIC DIAGRAM		
RJH-H007 240V AC CONTROL CIRCUIT SCHEMATIC	REC	27.8.96				
RJH-H008 240V AC CONTROL CIRCUIT SCHEMATIC	N.E.O.	27.0.50		15 D8-33		
				0		

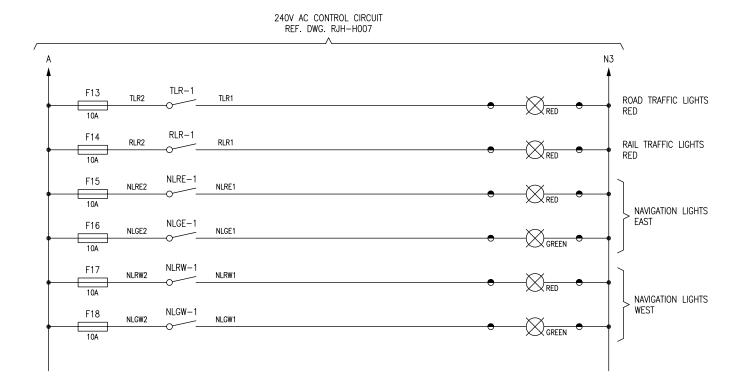


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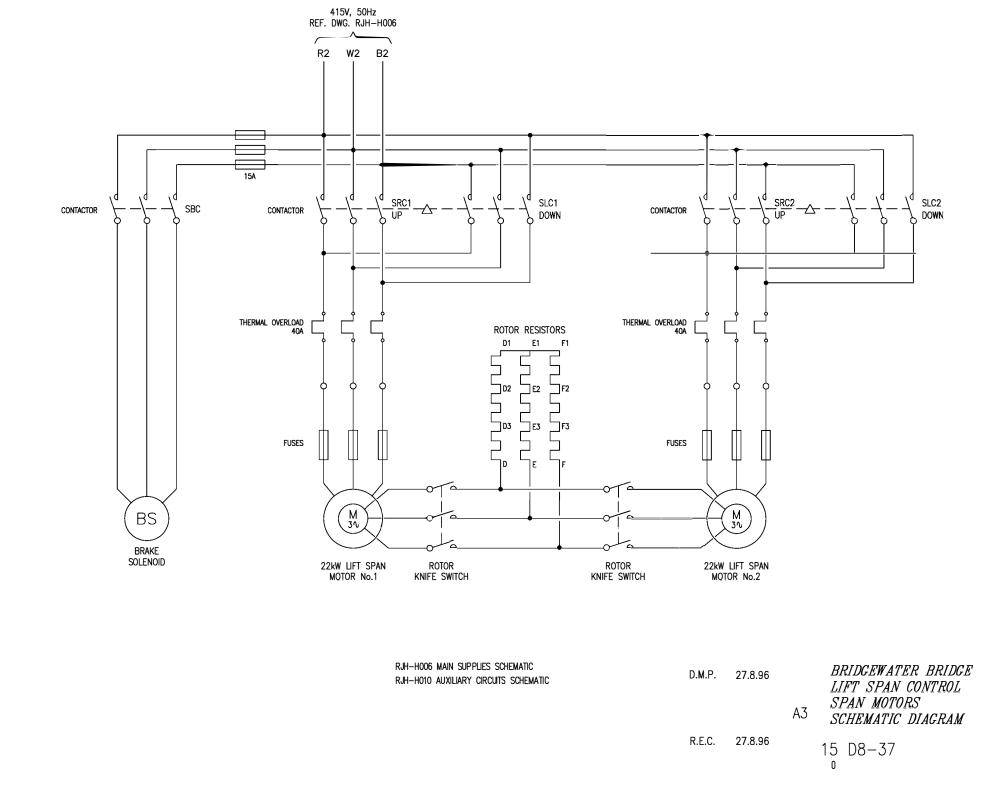


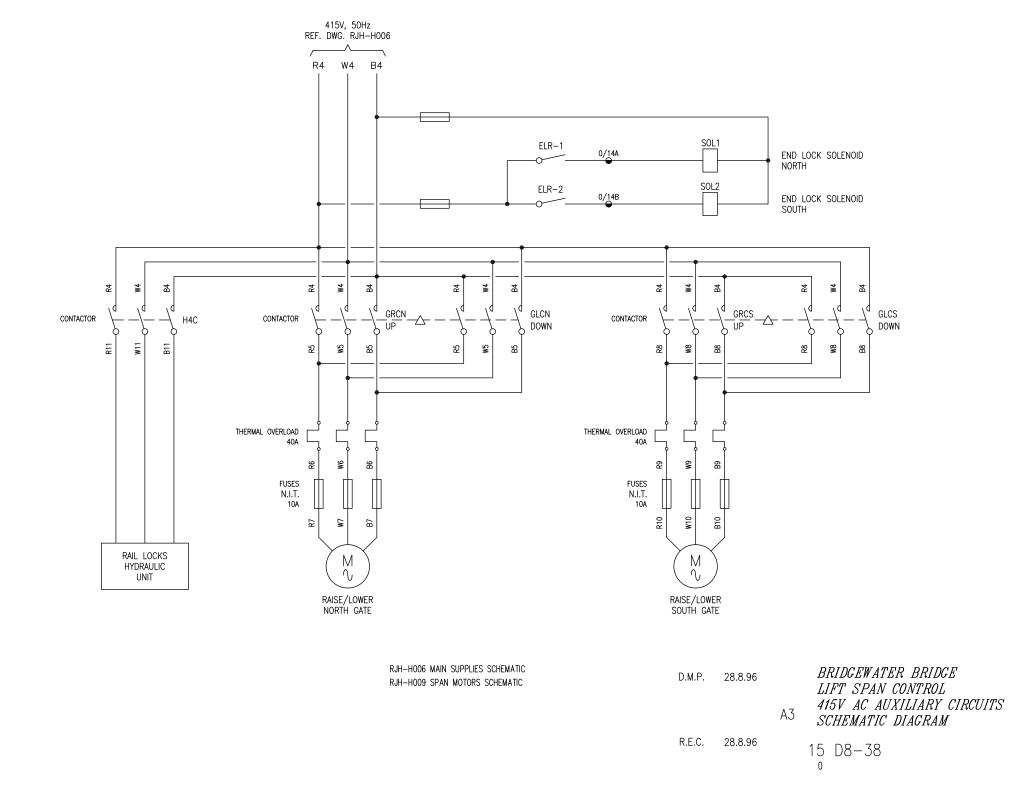
RJH-H001 PLC INPUT MODULES 1 & 2 SCHEMATIC BRIDGEWATER BRIDGE D.M.P. 27.8.96 RJH-H002 PLC INPUT MODULE 3 SCHEMATIC LIFT SPAN CONTROL RJH-H003 PLC OUTPUT MODULE 6 SCHEMATIC 240V AC CONTROL CIRCUIT RJH-H004 PLC OUTPUT MODULE 7 SCHEMATIC Α3 SCHEMATIC DIAGRAM RJH-H005 240V AC CONTROL CIRCUIT SCHEMATIC RJH-H006 MAIN SUPPLIES SCHEMATIC R.E.C. 27.8.96 15 D8-35 RJH-H008 240V AC CONTROL CIRCUIT SCHEMATIC

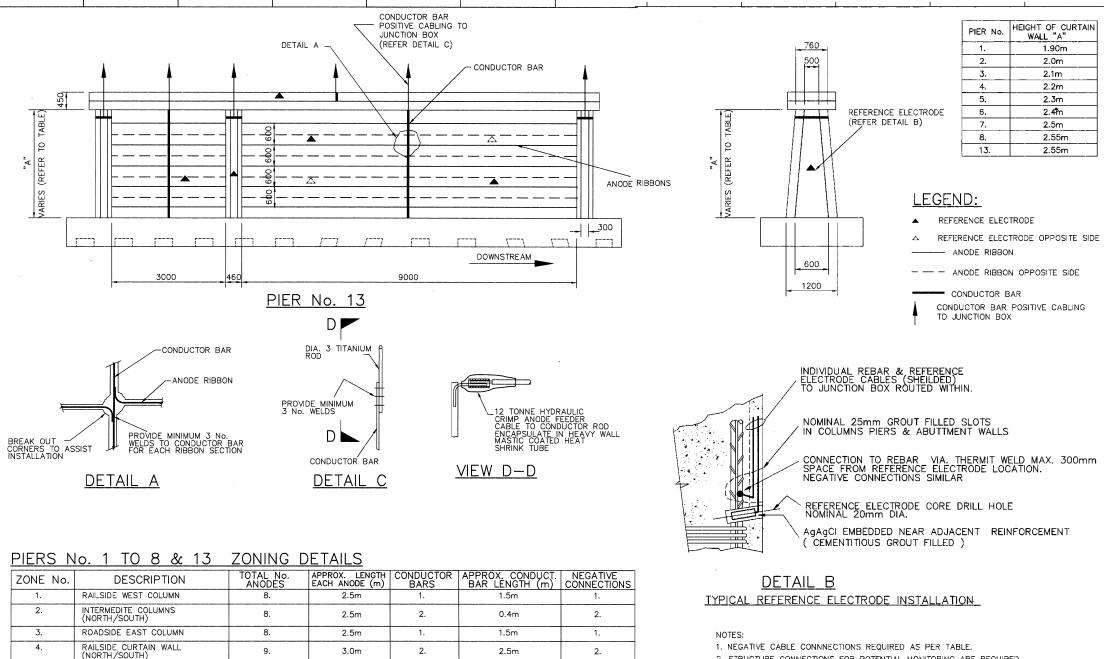
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RJH-H001 PLC INPUT MODULES 1 & 2 SCHEMATIC RJH-H002 PLC INPUT MODULE 3 SCHEMATIC RJH-H003 PLC OUTPUT MODULE 6 SCHEMATIC RJH-H004 PLC OUTPUT MODULE 7 SCHEMATIC RJH-H005 240V AC CONTROL CIRCUIT SCHEMATIC	D.M.P.	27.8.96	A3	BRIDGEWATER BRIDGE LIFT SPAN CONTROL 240V AC CONTROL CIRCUIT SCHEMATIC DIAGRAM
RJH-H006 MAIN SUPPLIES SCHEMATIC RJH-H007 240V AC CONTROL CIRCUIT SCHEMATIC	R.E.C.	27.8.96		15 D8-36







- 2. STRUCTURE CONNECTIONS FOR POTENTIAL MONITORING ARE REQUIRED
- ADJACENT TO EACH REFERNCE CELL INSTALLATION.
- 3. MAXIMUM ANODE RIBBON SPACING ON CURTAIN WALL TO BE 600mm.
- 4. ANODE AND REFERENCE ELECTRODE POSITIONS ARE NOMINAL ONLY. ACTUAL POSITIONS ARE TO BE DETERMINED BY SITE ENGINEER DURING CONSTRUCTION.

5. REFERENCE ELECTRODES REQUIRED ON BOTH UPSTREAM NOTE: ABOVE DETAILS RELATE TO PIER 13 (OTHER PIERS ARE SIMILAR) AND DOWNSTREAM COLUMNS EVISION CUERT DEPARTMENT OF TRANSPORT TASMANIA ACCIPTED FOR DOT CATHODIC PROTECTION & ASSOCIATED WORKS DERWENT RIVER BRIDGE AT BRIDGEWATER DIER WILSON WALTON INTERNATIONAL DRAWN 26-05-98 MELBOURNE CHECKED CONTRACT No 720 0 A.C.N. 054 016 303 MATERIAL DISCLOSED IN THIS DOCUMENT IS CONDENTIAL PROPRIETARY INFORMATION AND SHOULD NOT BE COFIED OR REPRODUCED IN ANY FORM OR GVEN TO CHECKED A. 1 CHECKED SCALE A PROJ. A N.T.S. CLIENT SIGNED 15 D8-39 TYPICAL ARRANGEMENT FOR PIERS 1 TO 8 & 13 TRE-----____ NO. BY DATE CHK'D APPR. REVISION DRAWING NO REFERENCE DRAWINGS NY OTHER PERSON WITHOUT WRITTEN DATE-

4.

2.

2.5m

0.3m

5.

6.

ROADSIDE CURTAIN WALL

(NORTH/SOUTH)

PIER CAP

9.

4.

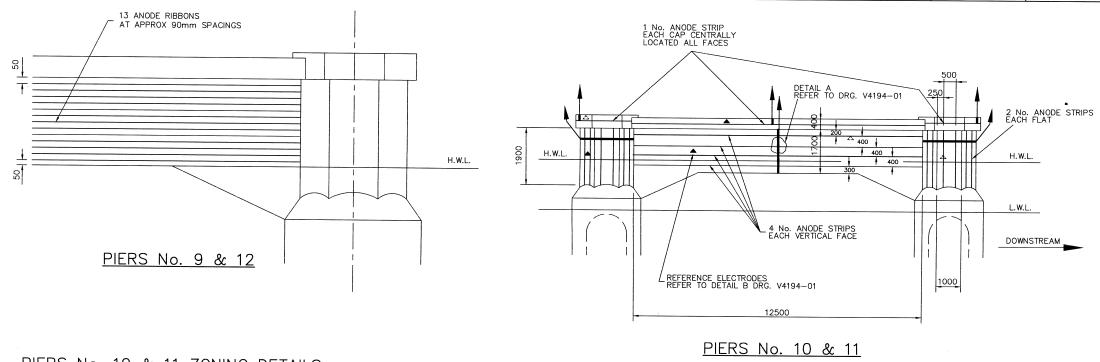
10.0m

2x15m

2x1.5m

2.

2.



PIERS No. 10 & 11 ZONING DETAILS

ZONE No.	DESCRIPTION	TOTAL No. ANODE STRIPS	APPROX. LENGTH EACH ANODE (m)	CONDUCTOR	APPROX. CONDUCT. BAR LENGTH (m)	NEGATIVE CONNECTIONS
1.	RAILSIDE OCTAGONAL CAP	1.	7.3m	1.	0.3m	1.
2.	ROADSIDE OCTAGONAL CAP	1.	7.3m	1.	0.3m	1.
3.	RAILSIDE OCTAGON	14.	2.0m	1.	7.5m	2.
4.	ROADSIDE OCTAGON	14.	2.0m	1.	7.5m	2.
5.	SOUTHSIDE VERTICAL CROSSBEAM FACE	4.	12.5m	1.	2.1m	2.
6.	NORTHSIDE VERTICAL CROSSBEAM FACE	4.	12.5m	1.	2.1m	2.
7.	CROSSBEAM CAP	2.	12.5m	2.	0.3m	2.

LEGEND:

- REFERENCE ELECTRODE
- △ REFERENCE ELECTRODE OPPOSITE SIDE
- ANODE RIBBON
- CONDUCTOR BAR
- CONDUCTOR BAR POSITIVE CABLING TO JUNCTION BOX

9 512

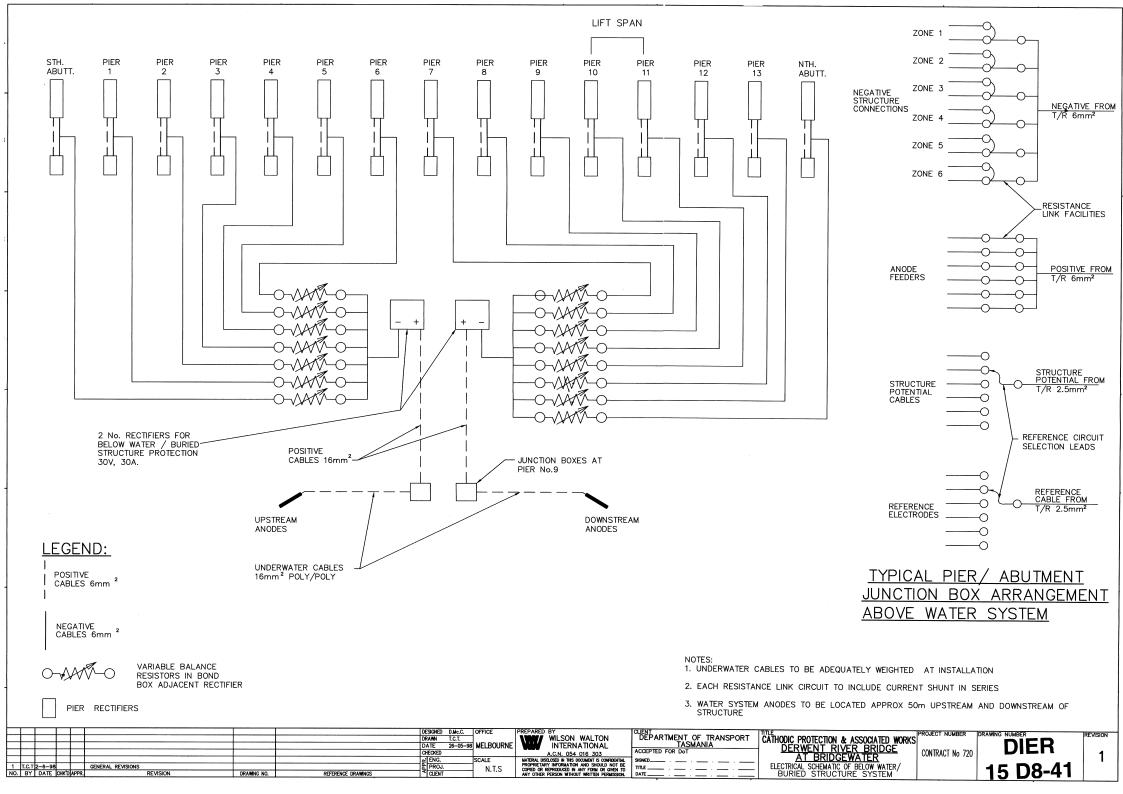
PIERS No. 10 & 11 ZONING DETAILS

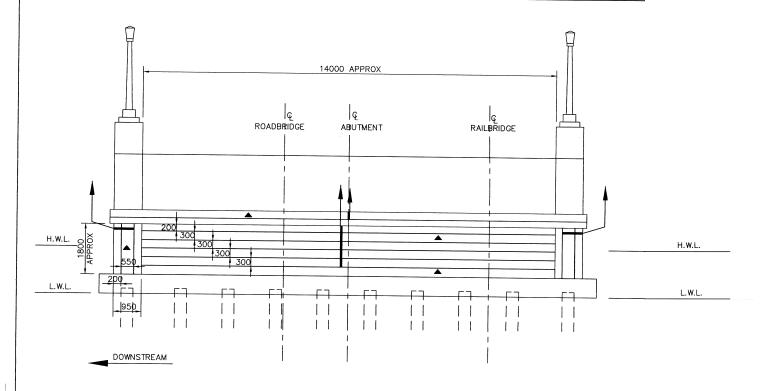
ZONE No.	DESCRIPTION	TOTAL No. ANODE STRIPS	APPROX. LENGTH EACH ANODE (m)	CONDUCTOR BARS	APPROX. CONDUCT. BAR LENGTH (m)	NEGATIVE CONNECTIONS
1.	RAILSIDE OCTAGONAL CAP	1.	7.3m	1.	0.3m	2.
2.	ROADSIDE OCTAGONAL CAP	1.	7.3m	1.	0.3m	2.
3.	RAILSIDE OCTAGON	14.	2.0m	1.	7.5m	2.
4.	ROADSIDE OCTAGON	14.	2.0m	1.	7.5m	2.
5.	SOUTHSIDE VERTICAL CROSSBEAM FACE	13.	12.5m	1.	2.1m	2.
6.	NORTHSIDE VERTICAL CROSSBEAM FACE	13.	12.5m	1.	2.1m	2.
Ζ.	CROSSBEAM CAP	2.	12.5m	2.	0.3m	2.

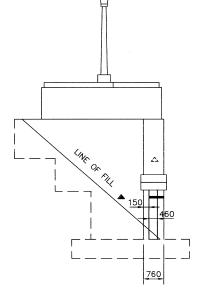
NOTES:

- 1. 2 No. NEGATIVE CABLE CONNNECTIONS FOR EACH ZONE REQUIRED.
- STRUCTURE CONNECTIONS FOR POTENTIAL MONITORING ARE REQUIRED ADJACENT TO EACH REFERNCE CELL INSTALLATION.
- ANODE AND REFERENCE ELECTRODE POSITIONS ARE NOMINAL ONLY. ACTUAL POSITIONS ARE TO BE DETERMINED BY SITE ENGINEER DURING CONSTRUCTION.
- 4. CONDUCTOR BAR FOR EACH OCTAGON AND OCTAGON CAP ARE SEPARATE.
- 5. FOR PIERS No. 9 & 12 ALL DETAILS ARE AS PER PIERS 10 & 11 EXCEPT ADDITIONAL ANODE RIBBONS ON VERTICAL CROSS BEAM FACES AS SHOWN.

							DRAWN T.C.T. DATE 26-05-98 CHECKED	MELBOURNE	INTERNATIONAL A.C.N. 054 016 303 MATERIAL DISCLOSED IN THIS DOCUMENT IS CONFIDENTIAL PROPRIETARY INFORMATION AND SHOULD NOT BE	CLENT DEPARTMENT OF TRANSPORT TASMANIA ACCEPTED FOR DOT SOURD	CATHODIC PROTECTION & ASSOCIATED WORKS DERWENT RIVER BRIDGE AT BRIDGEWATER	CONTRACT NO 720	
NO. BY	DATE	HK'D APP	R.	REVISION	DRAWING NO.	REFERENCE DRAWINGS		N.T.S.		_ III CE		15 D8-40	







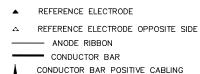
SOUTH ABUTMENT ZONING DETAILS

ZONE No.	DESCRIPTION	TOTAL No. OF ANODES	APPROX. EACH ANODE LENGTH (m)	CONDUCTOR BARS	APPROX. CONDUCT. BAR LENGTH (m)	NEGATIVE CONNECTIONS
1.	EAST COLUMN	4.	1.8m	1.	1.3m	1.
2.	WEST COLUMN	4.	1.8m	1.	1.3m	1.
3.	CURTAIN WALL	5.	14.0m	1.	1.6m	2.
4.	WALL CAP	1.	16.0m	1.	0.3m	2.
		-	1			

NORTH ABUTMENT ZONING DETAILS

ZONE No.	DESCRIPTION	TOTAL No. ANODE STRIPS	APPROX. EACH ANODE LENGTH (m)	CONDUCTOR BARS	APPROX. CONDUCT. BAR LENGTH (m)	NEGATIVE CONNECTIONS
1.	EAST COLUMN	4.	2.5m	1.	1.3m	1.
2.	WEST COLUMN	4.	2.5m	1.	1.3m	1.
3.	CURTAIN WALL	7.	14.0m	1.	2.3m	2.
4.	WALL CAP	1.	16.0m	1.	0.3m	2.

LEGEND:

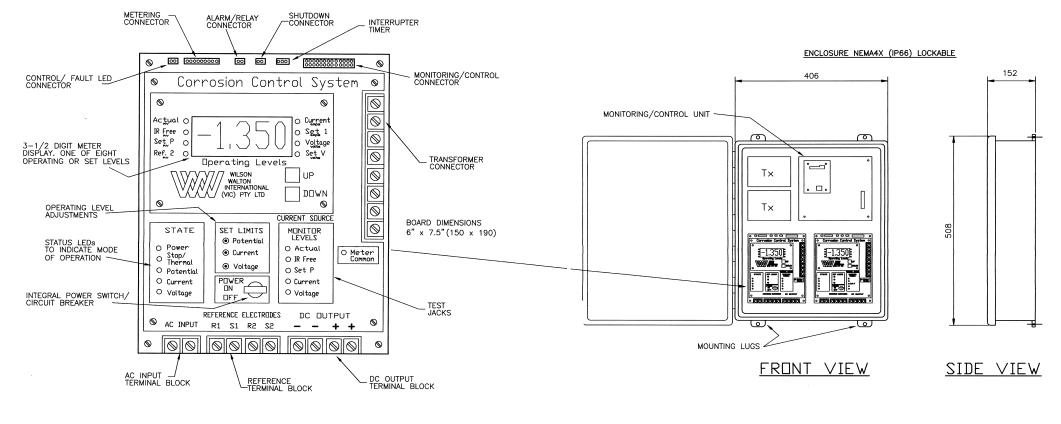


TO JUNCTION BOX

NOTES:

- 1. 2 No. NEGATIVE CABLE CONNNECTIONS REQUIRED FOR CURTAIN WALL AND WALL CAP.
- 2. STRUCTURE CONNECTIONS FOR POTENTIAL MONITORING ARE REQUIRED ADJACENT TO EACH REFERNCE CELL INSTALLATION.
- 3. ANODE AND REFERENCE ELECTRODE POSITIONS ARE NOMINAL ONLY. ACTUAL POSITIONS ARE TO BE DETERMINED BY SITE ENGINEER DURING CONSTRUCTION.
- 4. NORTH ABUTMENT SIMILAR BUT REQUIRES ADDITIONAL ANODE STRIPS PER ZONING DETAILS
- 5. AREAS NOT COVERED BY RIBBON ANODES PROTECTED BY BELOW WATER/ BURIED PROTECTION SYSTEM.

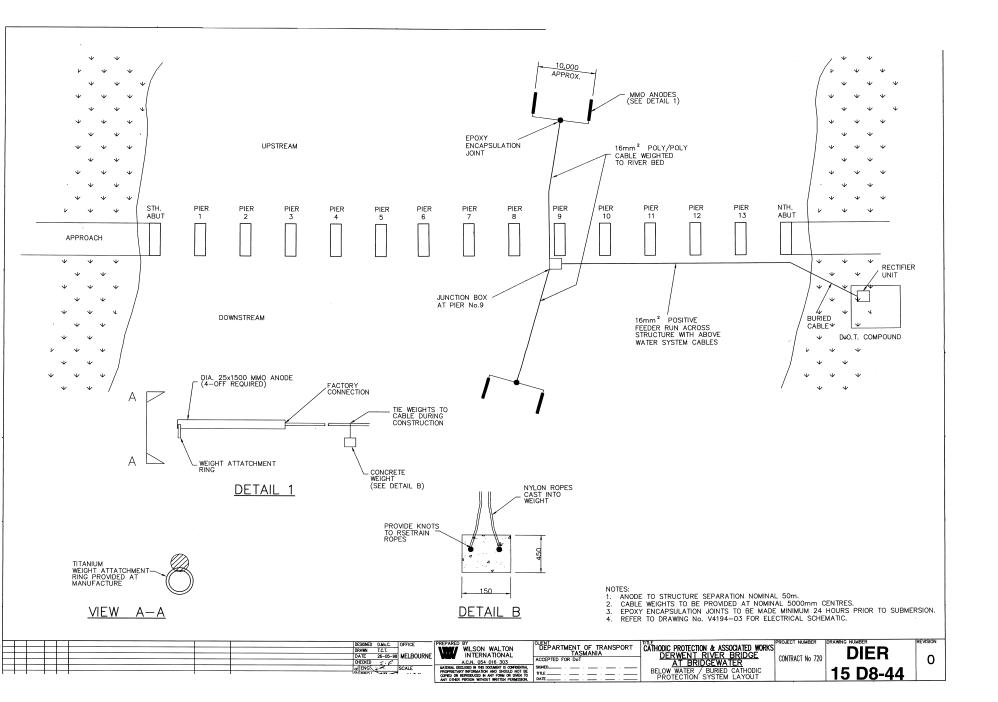
	DESIGNED [D.Mc.C.	OFFICE	PREPARED BY	CLIENT	INDE	PROJECT NUMBER	DRAWING NUMBER	REVISION
	DRAWN 1	T.C.T.	1	WILSON WALTON	DEPARTMENT OF TRANSPORT	CATHODIC PROTECTION & ASSOCIATED WORKS	THOSE OF HOMELIN		
	DATE 2	26-05-98	MELBOURNE	E INTERNATIONAL	TASMANIA	DERWENT RIVER BRIDGE			
	CHECKED	56		A.C.N. 054 016 303	ACCEPTED FOR DoT	DERWENT NIVER DINDOL	CONTRACT No 720		
	CHENG.	a ·	SCALE	WATERIAL DISCLOSED IN THIS DOCUMENT IS CONFIDENTIAL	SIGNED	AT BRIDGEWATER			
	IFIPROJ.	m	NTC	PROPRIETARY INFORMATION AND SHOULD NOT BE	775	GENERAL ARRANGEMENT FOR		15 D8-42	
NO. BY DATE CHK'D APPR. REVISION DRAWING NO. REFERENCE DRAWINGS			N.I.S	COPIED OR REPRODUCED IN ANY FORM OR GIVEN TO ANY OTHER PERSON WITHOUT WRITTEN PERMISSION.	DATE	ABUTMENTS			
				ANT OTHER PERSON WITHOUT WITTEN PERMISSION.		//BellinEirite			



PHASED CURRENT SOURCE RECTIFIER (TYPE PCS2)

A.C. INPUT- 240V AC 1PH. 50Hz D.C. OUTPUT- 0-24V 0-2 AMPS

					DESIGNED		OFFICE	PREPARED		CLIENT	TITLE	PROJECT NUMBER	DRAWING NUMBER	REVISION
					DRAWN	T.C.T.	1		WILSON WALTON	DEPARTMENT OF TRANSPORT	CATHODIC PROTECTION & ASSOCIATED WORKS		DIED	
					DATE	26-05-98	MELBOURN	IE NIN	INTERNATIONAL	TASMANIA	DERWENT RIVER BRIDGE		DIER	-
					CHECKED	エード	7		A.C.N. 054 016 303	ACCEPTED FOR DoT		CONTRACT No 720		
					ENG.	sa	SCALE	MATERIAL D	ISCLOSED IN THIS DOCUMENT IS CONFIDENTIAL	SIGNED	AT BRIDGEWATER			
					음 PROJ.	m l	N.T.S	PROPRIETA	REPRODUCED IN ANY FORM OR GIVEN TO	nn£	TYPICAL TRANSFORMER		15 D8-13	
NO. BY	DATE CHK'D APPR.	REVISION	DRAWING NO.	REFERENCE DRAWINGS	< CLIENT		1 1.1.5	ANY OTHER	R PERSON WITHOUT WRITTEN PERMISSION.	DATE	RECTIFIERS DETAILS		10 00-43	
								6						



Department of Main Roads, Tasmania

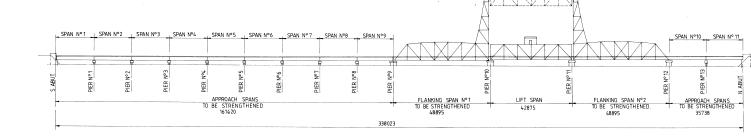
Derwent River Bridge at Bridgewater – Strengthening

Drawings

Maunsell & Partners Pty Ltd Consulting Engineers & Planners

COVER & TO BE WELDED TO UNDERSDE OF TOP & BORTOM FLANGES OF PLATE GIRDER Nº 1,2 & 3, (REFER TO DRG Nº 1503/15) COUTER & GIRDER CINNER & GIRDER H WL. RL 0.691 H WL. RL 0.691	ADDITIONAL INCLINED BEARING STIFFENER HWL RL COVER PLATES TO TOP & BOTTOM HWL RL CFT-FT-FT-LWL RL	GENERAL NOTES STRUCTURAL STEEL. 1 ALL STRENGTHENING STEEL TO BE GRADE 250L0. 2 ALL TEMPORARY WORKS STEEL TO BE GRADE 250. WELDING 1 ALL WELDING TO BE S.P. CATEGORY IN ACCORDANCE WITH AS1554. PART 1 2 ALL FULCTORES FOR FULLET WELDS TO BE F48XX. 3 ALL FULL PRETRATION BUTT WELDS TO BE F48XX. 4 ALL FULL STRENGTH OF 250LD STEEL. 4 ALL FULLET WELDS TO E 6 mm UNO.
APPROACH SPAN — TYPICAL CROSS SECTION	NOTE BRACING OMITTED FOR CLARITY.	
	ι.	Maunsell BRAWING IN. 17687-1001
D REFERENCE DRAWINGS SCALES ICADIO DESIGN DRAWING D T44 DESIGN DRAWING DESIGN DRAWING D PREPARED FILPY LLL' PREPARED FILPY LLL' PREPARED D OPERATION OPERATION DRAWING DRAWING D OPERATION OPERATION DREPARED FILPY LLL' D OPERATION OPERATION DREVISED DREVISED DATE AMENDMENTS APPROVED SUPERVISED PREFACE	CONTRACT NUMBER MIDLAND HIGHWAY BRIDGEWATER RECOMMENSION PUL/Like/Arei 4/4/67 Mension Enderer Beroges Assetshut Decctor	DEPARTMENT OF MAIN ROADS, TASMANIA DERWENT RIVER BRIDGE EXTENT OF STRENGTHENING FOR TYPICAL APPROACH SPAN

17982



	DRAWING LIST
DRG. Nº.	TITLE
15D3/14	EXTENT OF STRENGTHENING FOR TYPICAL APPROACH SPAN
1503/15	APPROACH SPAN STRENGTHENING - DETAILS
15D3/16	APPROACH SPAN UNLOADING FRAME



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- Additional inclined bearing Stiffener Boths Ends of 12 Girder N°2 Only (Refer to DRG.N° 1503/15)

(TF)

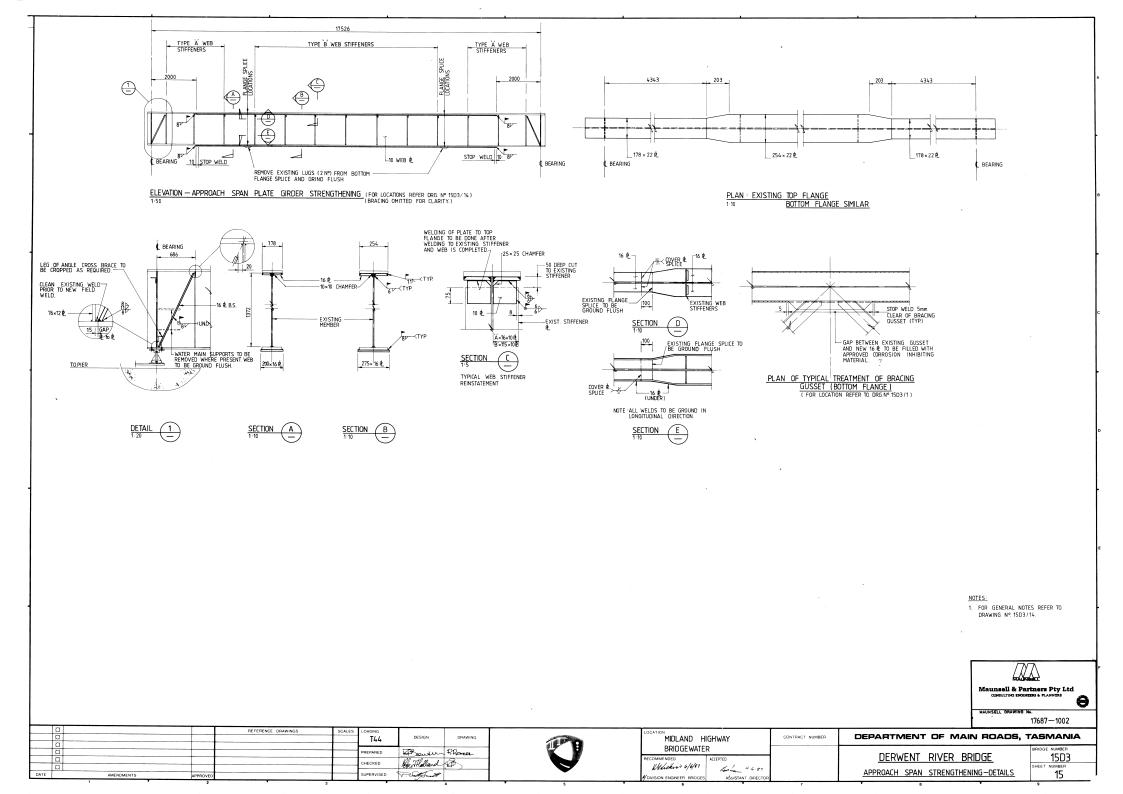
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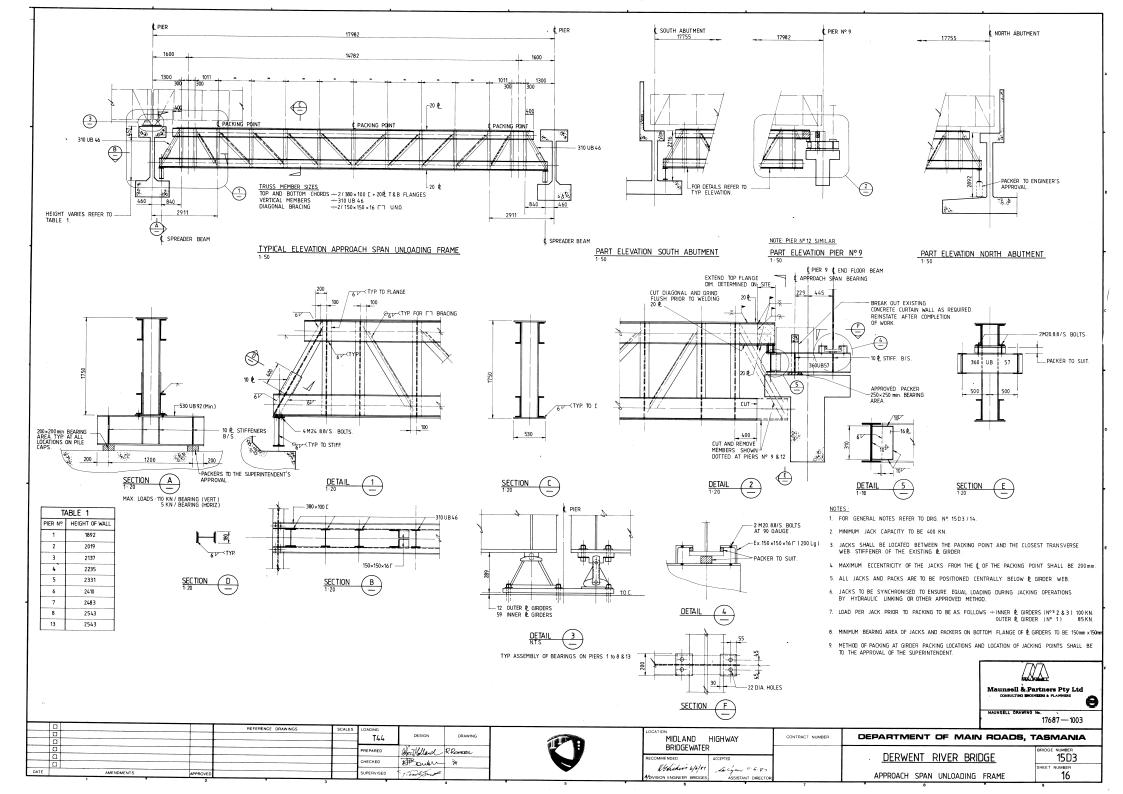
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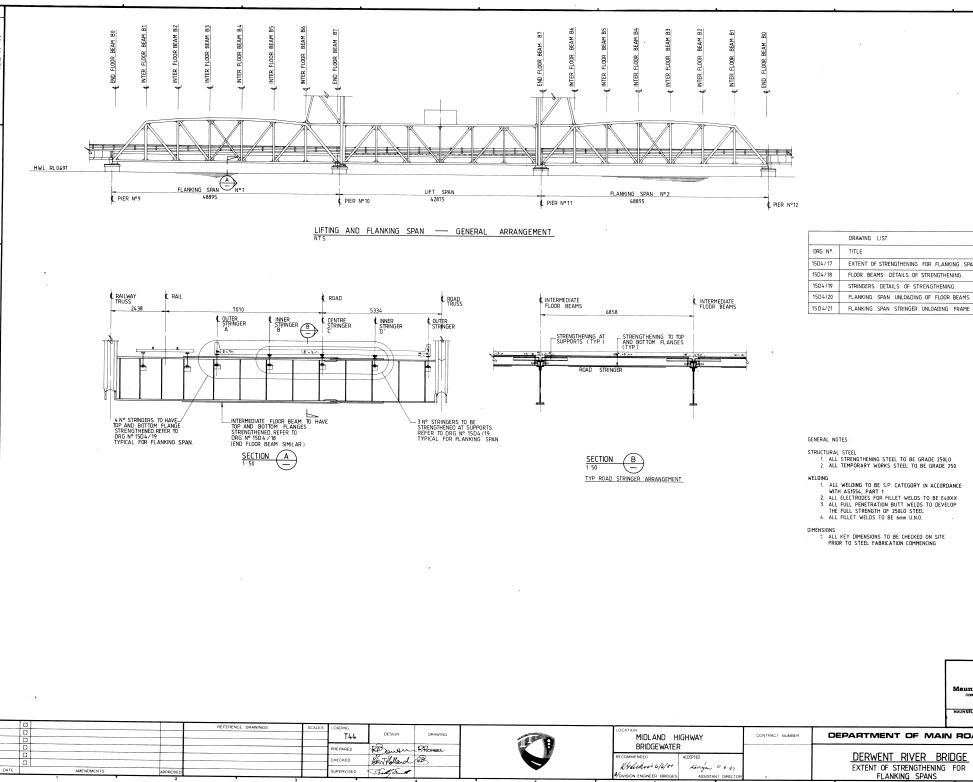
ROAD

A

RAIL





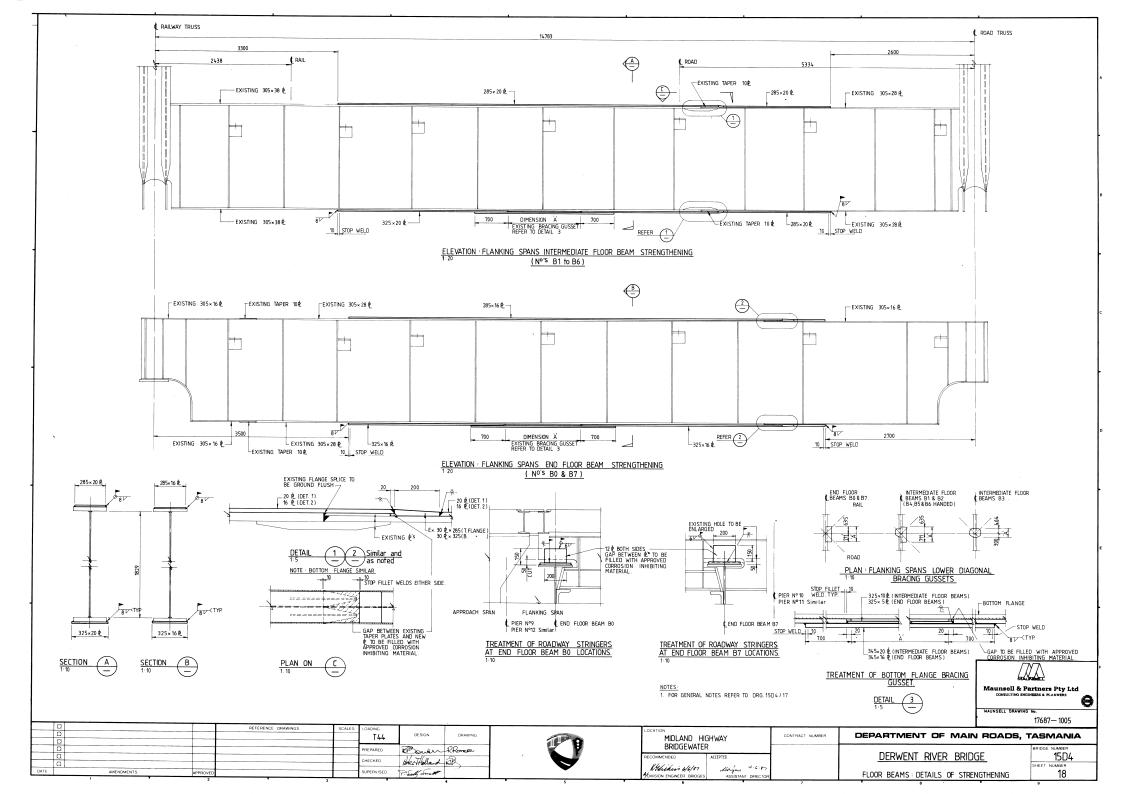


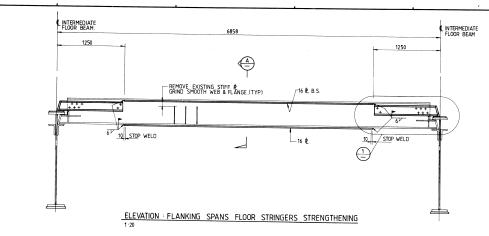
EXTENT OF STRENGTHENING FOR FLANKING SPANS. FLOOR BEAMS: DETAILS OF STRENGTHENING. STRINGERS DETAILS OF STRENGTHENING. FLANKING SPAN UNLOADING OF FLOOR BEAMS.

1. ALL STRENGTHENING STEEL TO BE GRADE 250L0 2. ALL TEMPORARY WORKS STEEL TO BE GRADE 250

Maunsell & Partners Pty Ltd consulting engineers & planners	θ
MAUNSELL DRAWING No. 17687-1004	

	GHWAY	CONTRACT NUMBER	DEPARTMENT OF MAIN ROADS,	TASMANIA
BRIDGEWATEF	2			BRIDGE NUMBER
RECOMMENDED	ACCEPTED		DERWENT RIVER BRIDGE	15D4
Kydickins 6/6/87	lariyan 4.6.87		EXTENT OF STRENGTHENING FOR	SHEET NUMBER
DIVISION ENGINEER BRIDGES	ASSISTANT DIRECTOR	•	FLANKING SPANS	17
6		7	8	9





SECTION

1:5

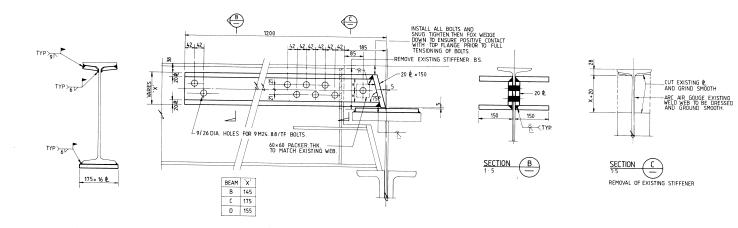
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STRENGTHENING FOR STRINGERS A.B.C & D. REFER DRG.Nº 15D 4 / 17 DETAIL

1.5

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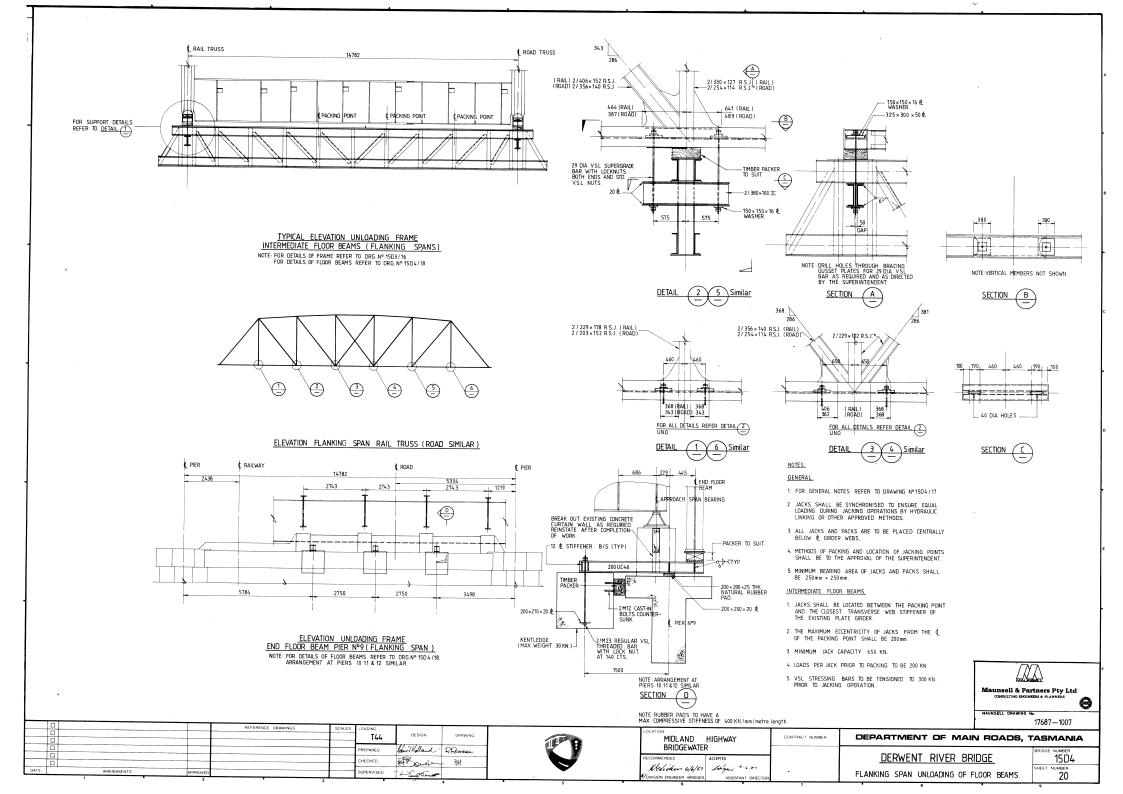
STRENGTHENING FOR STRINGERS B,C & D APPLIES AT ALL INTERMEDIATE FLOOR BEAM LOCATIONS. REFER TO DRG. Nº 15D4 / 17

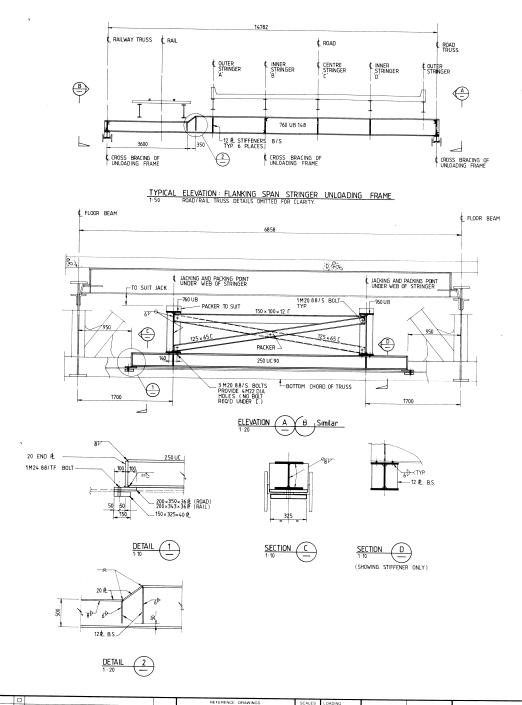


NOTES: 1. FOR GENERAL NOTES REFER TO DRAWING Nº 15D4/17

 ALL CONTACT SURFACES TO BE FASTENED WITH FRICTION GRIP BOLTS TO BE PREPARED AS DETAILED IN THE SPECIFICATION.

											Maunsell & Partners Pty Ltd CONSULTING ENGINEER'S & PLANNERS
	1	REFERENCE DRAWINGS	SCALES	LOADING	T						MAUNSELL DRAWING No. 17687—1006
			JUNCES	T44	DESIGN	DRAWING			CONTRACT NUMBER	DEPARTMENT OF MAIN	I ROADS, TASMANIA
				PREPARED	Reverthalland	RRaneer 1973	BRIDGEWAT RECOMMENDED	ACCEPTED	-	DERWENT RIVER BRI	
AMENDMENTS	APPROVED	3		SUPERVISED	PSelfort	4	S Neuron 6/6/1		R	STRINGERS DETAILS OF STREN	IGTHENING 19





Э.	JACKS SHALL BE SYNCHRONISED TO ENSURE EQUAL LOADING DURING JACKING OPERATIONS BY HYDRAULIC LINKING OR OTHER APPROVED METHOD.
4.	LOAD PER JACK PRIOR TO PACKING SHALL BE AS FOLLOWS.

NOTES

- STRINGER (A 25 KN. STRINGER (A - 25 KN. STRINGER B,C & D - 43 KN.
- AND LOCATIONS OF JACKING POINTS SHALL BE TO THE APPROVAL OF THE SUPERINTENDENT.

1. FOR GENERAL NOTES REFER TO DRAWING Nº 15D4/17.

2. MINIMUM JACK CAPACITY SHALL BE 100 KN.

- ONLY ONE STRINGER TO BE SUPPORTED ON UNLOADING FRAME AT ANY TIME.
- MINIMUM BEARING AREA OF JACKS AND PACKS ON BOTTOM FLANGE FLANGE OF STRINGER 150 mm × 150 mm.

Maunsell & Partners Pty Ltd

			CONSULTING ENGINEERS & PLANNESS MAUNSELL DRAWING No. 17687 – 1008
	25 SCALES LOADING T44 DESIGN DRAWING	LOCATION HIGHWAY CONTRACT NUMBER	DEPARTMENT OF MAIN ROADS, TASMANIA
	PREPARED POWIN RROKEN OHECKED (BRC/THOULD RD		DERWENT RIVER BRIDGE 15D4
DATE AMENDMENTS APPROVED	SUPERVISED FSchfmat	Northing Willer dw. Jac "14/87. VOMISION ENGINEER BRIDGES ASSISTANT DRECTOR	FLANKING SPAN STRINGER UNLOADING FRAME 21

APPENDIX 6 - POINT CLOUD SURVEY, SAMPLE VIEWS

Bridgewater Crossing – Archival Record [Revision 02, 18th August 2021] https://purcellukcom.sharepoint.com/sites/AsiaPacific/Shared Documents/Projects/240780/30 Reports, Specifications & Schedules/Archival Record/00 Report/Bridgewater Crossing Archival Record 20210818.docx

PURCELL



Sample View 01 – Overview Bridgewater Bridge, looking south.



Sample View 02 – Overview Bridgewater Bridge, west elevation.



Sample View 03 – Aerial perspective of Bridgewater Bridge.

Bridgewater Crossing – Archival Record [Revision 02, 18th August 2021] https://purcellukcom.sharepoint.com/sites/AsiaPacific/Shared Documents/Projects/240780/30 Reports, Specifications & Schedules/Archival Record/00 Report/Bridgewater Crossing Archival Record 20210818.docx

PURCELL



Sample View 04 – Overview Bridgewater Bridge, east elevation.



Sample View 05 – Perspective view of Bridgewater Bridge, looking north.



Sample View 06 - Bridgewater Bridge viewed from causeway to the north.

Bridgewater Crossing – Archival Record [Revision 02, 18th August 2021] https://purcellukcom.sharepoint.com/sites/AsiaPacific/Shared Documents/Projects/240780/30 Reports, Specifications & Schedules/Archival Record/00 Report/Bridgewater Crossing Archival Record 20210818.docx